Surface Water Study as part of the Integrated Waste Management Licence for the Codisposal Facility at Kusile Coal Fired Power Station

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Surface Water Study as part of the Integrated Waste Management Licence for the Ash Co-Disposal Facility at Kusile Coal Fired Power Station

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Disclaimer

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List of Abbreviations

AD Ash Dump

ADDD Ash Co Disposal Facility Dirty Dam

ADDF Ash Co Disposal Facility

BMP Best Management Practice(s)

BPG Best Practice Guideline(s)

D Duration

DWA Department of Water Affairs

E Spatial extent

EAD Emergency Ash Dump

EIA Environmental Impact Assessment
EMP Environmental Management Plan

FGD Flue Gas Desulphurisation

GA General Authorisation

GN Government Notice

MAP Mean Annual Precipitation

MAR Mean annual Runoff

Ns Not stated

KPS Kusile Power Station

P Probability

PCD Pollution Control Dam

P&G Provisional and General

R Reversibility

RDF Recommended Design Flood

RMF Regional Maximum Flood

RWQO Resource Water Quality Objectives

S Severity / magnitude

SCS Soil Conservation Services

SDD Station Dirty Dam

SDDST Station Dirty Dam Settling Tanks

SED Safety Evaluation Flood

SS Suspended Solids

Stds Standards

SWMP Stormwater Management Plan

TDS Total Dissolved Salts

WMA Water Management Area

1 Introduction and Scope of Work

SRK Consulting was appointed by Iliso Consulting to undertake a surface water specialist study for incorporation into the application for an Integrated Waste Management Licence for the construction of the facility which includes an Ash/gypsum Co-Disposal Facility, the Ash Co-Disposal Dirty Water Dam (ADDD), the Station Dirty Water Dam (SDD) and the station dirty dam settling tanks (SDD ST).

Considering the information already available and in view of the above the scope of work has been defined as summarised below:

- a. Describe all the surface water impacts and then propose mitigation measures as normally required for and EIA/EMP This will be done for the construction, operational, decommissioning and closure phases;
- b. A Storm Water Management Plan (SWMP) as prescribed by the Best Practice Guideline G1: Storm Water Management by DWAF, 2006. All recommendations to be in line with Regulation 704 of the NWA, 1998 and to include the following:
 - Catchment characteristics i.e. catchment boundaries (clean and dirty water), rainfall, water bodies (pans, dams, etc.), slope and drainage directions;
 - Determine the impact of all water retention infrastructure (dirty water dams associated with the ash co-disposal facility) on the Mean Annual Runoff (MAR) by simulating the life of the development over the affected streams;
 - Determine the storm water flows and volumes (1:50 & 1:100 year recurrence intervals) for both the dirty and clean water areas together with the infrastructure engineer. For storm water containment purposes the volumes for longer storm durations (24 hours) should also be determined;
 - **Flood lines** on all river sections that might be affected by or is in close proximity to Power Plant activities (100m).

1.1 Background

Kusile Coal-Fired Power Station is currently under construction with an anticipated output 4 800 MW, which covers approximately 2 500 ha of land on the Farm Hartebeesfontein 537 JR and the Farm Klipfontein 566 JR. in the Witbank area. Application was previously made for an environmental authorisation for a water treatment works, a wastewater treatment works, access roads, railway line, water supply pipelines, a coal stockyard, an ash disposal facility, a coal and ash conveyor system and water storage facilities. A positive environmental authorisation was received in June 2007.

This June 2007 EA was appealed and a revised EA was issued in March 2008 under the ECA. In terms of this EA, Eskom can construct the power station and operate ash disposal systems. The EA also states that Kusile Power Station will have Flue Gas Desulphurisation (FGD) technology to minimize particulate and SO2 emissions. As a result of FGD technology, gypsum shall be produced as a by-product during operation of the power station. At the time of the EIA, Eskom's intention was to dispose of ash only. Although the possibility of gypsum being generated through the FGD process and the commercial value related to it was discussed in the final EIA Report, the disposal of gypsum on the ash dump was not included. The co-disposal of gypsum with ash is therefore not authorised.

Since gypsum is considered to be a hazardous waste (classified as a medium hazardous waste), a Waste Management Licence (WML) must be applied for, to co dispose ash and gypsum as a listed activity 9, Category B of GN718 and the construction of the facility (Ash/gypsum co-disposal facility, the Ash Co-

disposal facility Dirty Water Dam (ADDD), the Station Dirty Water Dam (SDD) and the station dirty dam settling tanks (SDD ST)) will trigger activity 11, Category B of GN 718. In addition to the hazardous waste that will be disposed of at Kusile, general waste including rock spoils (the concrete rock spoil and K3 spoils) produced during construction will also be temporarily stored on site.

1.2 Location and Context of Kusile Power Station

The Kusile Power Station is situated approximately 10 km north of the Kendal Power Station, and west to north-west of the New Largo Coal Field.

The construction of the Kusile Power Station is on approximately 2,500 ha on the Farms Hartbeestfontein 537 JR and Klipfontein 566 JR.

The largest town within a 30 km radius of the site is Witbank. The smaller town of Bronkhorstspruit lies approximately 20 km North West of the site.

The power station falls within the jurisdiction of the Delmas District Municipality.

A locality map is provided below in Figure 1.1.



Figure 1-1: Locality of Kusile Power Station

1.3 Structure of Report

The aim of this document is to provide a risk assessment for the Kusile Power station Ash/Gypsum codisposal facility, the Ash Co-disposal Facility Dirty Water Dam (ADDD), the Station Dirty Water Dam (SDD) and the station dirty dam settling tanks (SDD ST). In line with this, the plan is divided into five main sections, with each section providing guidance and information on particular aspects of the SWMP. The three main sections contained in this study are:

- Legislative Framework & Regulatory Requirements;
- Status Quo Assessment of Existing Control Measures;
- Risk Assessment Methodology and Predicted Risk Assessments.

1.4 Methodology

The methodology implemented to develop the Surface Water Study consists of a number of different stages. These stages include the following:

- Collection of data: In order to inform the study on the risk assessments at the Kusile Power Plant, data and information related to the Kusile Power Plant was collected from various sources. This data was used to develop the necessary spatial representations (maps) and database to support the Surface Water Study, as well as to determine new control measures and proposed upgrade of existing controls;
- Assessment of relevant standards and guidelines: During this stage relevant Eskom and related South African standards/legislation were investigated (these are listed in Table 1-2 below) in order to determine the requirements related to stormwater management and pollution control at the Kusile Power Station;
- Site Visit and Status Quo Investigation: A site visit was undertaken by members of the
 project team on 11 September 2013. The aim of this visit was to investigate the current building
 status of infrastructure at the Kusile Power Station and to ascertain the floodline levels which
 could influence the compilation of the risk assessments. Where required, data and information
 such as measurements related to the capacity of infrastructure was obtained from relevant
 collected data;
- **Determination of required control measures:** Having defined legal requirements as well as the current status quo of the existing system enabled the team to identify required additional control measures as well as remediation opportunities for existing control measures.

1.5 Legislative Framework & Regulatory Guidelines

When assessing the existing status quo of a power station building project, relevant standards and regulations need to be used for benchmarking the current control structures and the operation at the power station. The relevant legislation and guidelines that were reviewed are summarised in Table 1-2 below.

Table 1-1: Summary of Legislative Requirements and Regulatory Guidelines relevant to stormwater and pollution control

Act / Regulation	Relevance and Requirement
National Environmental Management Act, 1998 (Act No. 107 of 1998)	On water management aspects
Regulations on Dam Safety published in terms of the National Water Act (Act no 36 of 1998): Dam Safety Standards	Minimum dam spillway requirements regarding spillway capacity: Recommended Design Flood (RDD): 1:100 year routed peak

Act / Regulation	Relevance and Requirement
	flow; Recommended Safety Evaluation Flood (SED): Regional Maximum Flood (RMF)
National Environmental Management : Waste Act (Act 59 of 2009)	Licensing of waste management activity
(GN) 704 dated 4 June 1999 Regulations published in terms of the National Water Act, 1998 (Act No. 36 of 1998):	Regulating the following: Separation of "clean" and "dirty" water on a site. Stormwater control structures to handle at least a 1:100 year storm event. Containment of "dirty" water run-off up to 1:50 year storm event with 0.8 m freeboard or a 1:200 year runoff volume with no freeboard. Prevention of erosion Structures to be outside a 1:100 year flood line and/or 100 m from the river, whichever is the greatest.
Department of Water Affairs Best Practice Guideline G1- Stormwater Management Plan & A4 – Pollution Control Dams 2006	Best practice guidelines for water resource protection in the South African mining industry (Stormwater Management (Department of Water Affairs and Forestry, 2006) and Pollution Control Dams (Department of Water Affairs and Forestry, 2008))

The following approach and standards have been used for compiling the Surface Water Study:

- Clean and dirty water systems to be kept separate and be designed, constructed, maintained and operated such that these systems do not spill into each other more than once in 50 years;
- Measures to be taken to protect water resources.
 - All dirty water or substances which cause or are likely to cause pollution of a water resource through natural surface flow to be contained;
 - Pollution control dams to have a surge storage capacity (minimum required storage capacity at onset of storm event) equal to the 1:50 year runoff volume due to a 24hour storm event plus 0.8 m freeboard;
 - All pollution control dams are to be lined with an impervious liner excepting where there is a natural clayey area that prevents polluted water from seeping into the ground water;
 - Dam spillways to handle at least the 1:100 year routed peak flow;
 - All diversions and canals to handle at least a 1:100 year storm event with no freeboard;
 - All control structures to be located outside the 1:100 year floodline and/or 100 m from the river – whichever is the greatest; and
- Clean temporary stormwater holding ponds to be decanted over a maximum period of 30 days after the storm event. d

2 Study Objectives and Work Program

2.1 Study objectives

The main objectives of the study are:

Predict risk assessments based on the information collected.

2.2 Project team

The following team undertook work for the study:

M Braune Pr. Eng (Reviewer)

M. Hinsch: Principal Water Quality / Resources Specialist

J. Mathole : HydrologistM. Stols: GIS Specialist

R. Sobey: Environmental Scientist

3 Data Collection and Reviewed Documents

An important aspect of this study is to obtain all relevant information on previous and current studies undertaken for KPS, as well as compliance requirements enforced by the DWA. The documentation reviewed and spatial data obtained from the power station, and their relevance is summarised in Table 3-1 below.

Table 3-1: Summary of reviewed documents and digital data

Data List					
Name	Description	Source			
Wetlands Method Statement – Kusile PS Combustion Waste Terrace (Knight Piesolt, 2013)	Wetlands method statement for the construction of the combustion Waste Terrace	Knight Piesold Consulting			
Aquatic Ecological Assessment (Ecosun, Report E 457/06/B)	Wetland and Ecological Impact Assessment	Ecosun Consulting			
Ash Dump and Ash Dump Dirty Dam Design Report (Panel B Consortium_ PBCJV TO#31, 2010)	Kusile Power Station Ash Dump Terrace Layer Works Design	Gibb, SSI and Knight Piesold Consulting			
Ash Dump Report	Proposed Amended Layout and Construction Sequence for the Ash Dump	Gibb, SSI and Knight Piesold Consulting			
Emergency Ash Dump Layer Works Design Report and Drawings (Panel B Consortium joint Venture PBC JV#19, 2008)	Emergency Ash Dump Layer Works Design Report and Drawings	Gibb, SSI and Knight Piesold Consulting			
Station Dirty Dam Design Report (Panel B Consultants joint Venture PBC JV-TO #31, 2010)	Kusile Power Station Dirty Dam Design Report	Gibb, SSI and Knight Piesold Consulting			
Final Kusile EMP	EMP approved in March 2008	Gibb, SSI and Knight Piesold Consulting			
Ash Dump Embankment Culvert (Panel B Consultants joint Venture	Construction of the Ash Dump Embankment	Gibb, SSI and Knight Piesold Consulting			

Data List					
Name	Source				
WMS 5452/110/014 (Rev 1), 2010)	Culvert				
Ground and Surface water monitoring report September 2013	Ground and Surface water monitoring report September 2013	Zitholele Consulting			
	Spatial Data				
Phase 1 and 2		Shape Files for Kusile Layout Plan showing separate phases			
Site Layout		Shape Files for Kusile Layout Plan			

4 Status Quo Assessment of Stormwater and Pollution Control System

It is important to obtain an understanding of the existing stormwater system during construction as well as the pollution control system of the Power Station and its operation. Relevant details are given in this section.

4.1.1 Zero liquid effluent discharge

Eskom's Kusile Power Station has implemented integrated water conservation into the organisations planning to ensure that appropriate technologies will be implemented to ensure the optimisation of the water. In order to ensure that water management is optimised Eskom has implemented a zero liquid effluent discharge philosophy at the Kusile Power Station, which will also apply to the Ash Co-disposal Facility (ADDF). This means that liquid effluents will not be discharged from the waste site, Dirty Water Dams or the Ash Dam (AD) site into the environment, but will rather be recycled and reused. An example of the recycling that is employed is that Kusile Power Station will employ a three step process at its wastewater treatment plant of 1) Pre-treatment, 2) Evaporation/Concentration, and 3) Crystallisation to treat this wastewater. This will produce a clean water stream that can be reused, which allows the power station to reduce its raw water intake by up to 3%.

4.1.2 Minimising seepage losses

The engineering of the Ash Co-disposal facility and its associated infrastructure lining for all dirty water is designed to reduce seepage losses and reduce risks on the receiving water environment.

4.1.3 Segregation of clean and dirty water systems

In accordance with the principles of Regulation 704 of the Water Act, clean storm water will be diverted around the footprint area of Ash Co-disposal facility and is to be released into the natural environment, whilst impacted storm water within the footprint area of Ash Co-disposal facility will be contained and reutilised through the ADDD and SDD.

4.2 Field Measurements and Existing Stormwater Drainage System

All the information gained for this study was received from a field study, the data received from the various sources and from SRK's own desktop study. SRK also developed and its own GIS files to properly ascertain the floodline levels and hydrological modelling.

4.3 Existing Pollution Control System

The existing pollution control system consisting mainly of the Dirty Dams are not yet in operation.

4.4 Catchment Delineation and Classification

The study area lies approximately 35km east south east of Witbank, situated in the Olifants River Catchment (Quaternary Catchment B20F). The catchments are divided into various main catchments as well as sub-catchments. The catchment size and boundaries have been determined from existing contour information and taking into account existing control systems that reroute flows in various directions. Table 4-1 below contains the details of the Quaternary Catchment B20F.

Table 4-1: Table showing the mean annual precipitation, run-off and potential evaporation per quaternary catchment (WR2005 Study_WRC).

Quaternary Catchment	Catchment Surface Area km ²	Mean Annual Rainfall (MAP) in mm	Mean Annual Run-off (MAR) in mm	MAR as % of MAP
B20F	504	661	16.7	2.5

The catchments in the Kusile Power Station Area were then classified in terms of the land use as well as condition in terms of level of pollutants. This was based on the Best Practice Guideline G1. A summary of the catchment land-use classification is given in Table 4-2 below. The relevant sections to the ash dam, is shown in bold.

Table 4-2: Catchment Land-use Classification an abstract from Department of Water Affairs and Forestry Guideline (Department of Water Affairs and Forestry, 2006)

Classification	Area	Comment		
		Regional geology of agricultural practices may contaminate runoff.		
	Residue deposits	Includes coal discard, slurry facilities, slime dams, waste rock dumps and sand dumps.		
Moderately dirty Unrehabilitated areas Dissolved and		Dissolved and suspended contaminants.		
Haul roads		Dissolved and suspended contaminants.		
	Pollution control dams	Depends on contents of dam.		
Dirty	Residue deposits	Includes coal discard, slurry facilities, slime dams, waste rock dumps and sand dumps.		
	Unrehabilitated areas	Dissolved and suspended contaminants.		
	Haul roads	Dissolved and suspended contaminants.		
	Pollution control dams	Depends on contents of dam.		

4.5 Hydrological Modelling

In order to determine flood peaks and runoff volumes from the above defined catchments and subcatchments a hydrological model needed to be set up. Visual SCS and Rational methods were used to determine the Peak flows for floodline determination and rational method flood peaks were adopted for the ash co-disposal facility dirty water and clean water catchments as better correlation was observed between this method and the peak flows used for the designing of the dirty water and clean water channels. The model makes use of the following main input parameters:

- i. Storm rainfall;
- ii. Soil conditions;
- iii. Catchment shape, slope and size; and
- iv. Urbanisation, vegetation and land use.

Relevant input parameters have been calculated from the determined information and are described below.

4.5.1 Rainfall Assessment

Rainfall for the model was based on IDF (intensity-duration-frequency) curves derived for this study area by J C Smithers and R E Schulze. The estimated design rainfall depths for durations ranging from 15 minutes to 7 days and for return periods ranging from 2 to 200 years for the Kusile study area were calculated.

The 24-hour design rainfall for various return periods is given in Table 4-3 below:

Table 4-3: Design Rainfall (24 hr.)

Return Period	1:2 Year	1:5 Year	1:10 Year	1:20 Year	1:50 Year	1:100 Year
Rainfall depth (mm)	59	81	99	119	143	165

4.5.2 Catchment Details

The catchment details and land-use classification for the natural watercourse (Including diversion canal) as abstracted for the Kusile Power Plant are now summarised in Table 4-4 below. Figure 4-3: shows the locality of catchments and detailed delineation descriptions.

Table 4-4: Summary of storm water delineated catchments and classification thereof

Catchment Name	Classification	Individual Area (km²)	Cumulative Area (km²)
KLF	Clean	9.20	60.38
KLFS1	Clean	2.26	49.51
KLFS2	Dirty	9.77	34.86
KLFS3	Dirty	6.54	21.23
KLFS1T	Moderately Dirty	1.67	1.67
KLFS2T1	Dirty	4.05	12.84
KLFS2T2a	Dirty	3.40	3.40
KLFS2T2b	Dirty	0.54	4.0
KLFS2T2c	Dirty	0.54	6.0
KLFS2T2d	Dirty	0.86	9.66
KLFS2T2e	Dirty	1.59	1.59
KLFS2T2f	Dirty	2.8	2.80
HLF	Clean	14.63	14.63
Wilge1T1	Clean	4.75	28.95
Wilge1T2	Clean	7.28	17.50
Wilge1T3	Moderately Dirty	6.40	6.40
Wilge1T1T	Clean	6.70	6.70
Wilge1T2T	Clean	3.82	3.82

The following can be observed from the table above:

- i. More than half of sub-catchments are classified as dirty. This is mainly due to the construction of the dirty water dams, ash co-disposal facility and the haul roads.
 - The areas surrounding the KPS are generally clean.

- A quarry is situated to the north east corner of the power station.
- The ash co-disposal facility will be built to the south of the power station, which contributes to the dirtying of a few of the catchment areas.
- All the areas in direct contact with the power plant were also classified as dirty
- ii. Only two catchments were classified as moderately dirty.
 - The moderately dirty catchment areas have a haul road which will be used to transport coal.
- iii. The defined clean sub-catchments consist of the following areas:
 - Natural vegetation and farm land lies mostly to the south, west and north of the power station.
 - To the south east lies farmland with what appears to be a clean dam on the border of the catchment area.

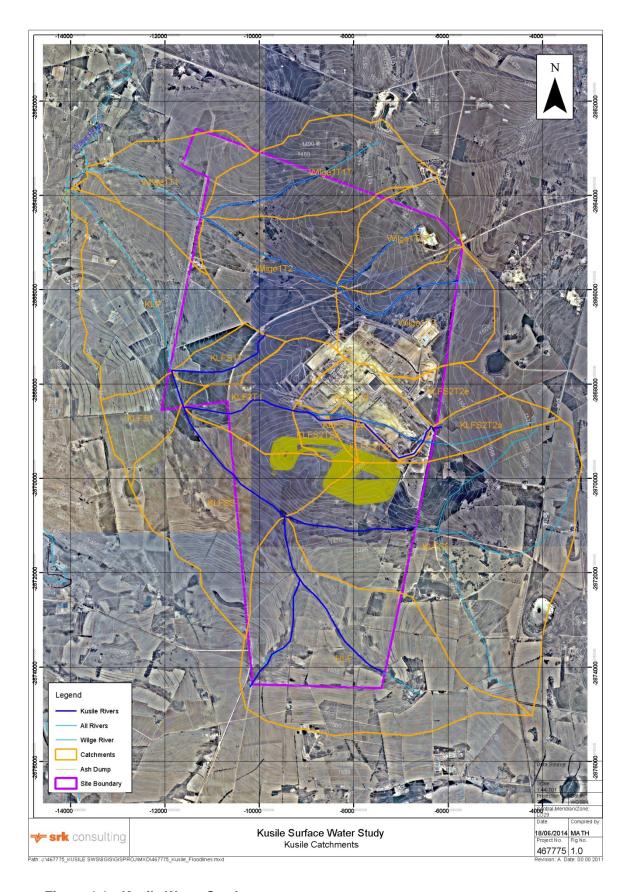


Figure 4-1: Kusile Water Catchments

4.5.3 Hydrological Model Details and Parameters

The hydrological model could now be compiled based on the catchment and input parameters derived in the above sections for both the existing drainage system as well as the possible future drainage system. The drainage systems are defined as follows:

- i. At present the area is under construction and basic storm water features are in place to separate the dirty and clean water.
- ii. The ash co-disposal facility embankment culvert has been constructed to direct water from a stream underneath the ash co-disposal facility to avoid contamination.
- iii. Excavated clean water drains have been constructed around the ash disposal facility with culverts and culvert discharge trenches which lead to silt retention dams.
 - a. The 1:100 yr./ 24 hr. clean stormwater runoff will be kept separate from the dirty water runoff from the co-disposal facility site.
 - b. Runoff from fully rehabilitated areas will be managed as clean water and discharged to the streams on either side of co-disposal facility after passing through a series of retention/settling dams located around the ash co-disposal facility perimeter. These facilities will be monitored on an ongoing basis to test the water quality before discharging to the natural streams.
 - c. The runoff from the incremental clean water catchments outside of the active footprint, flowing towards the active co-disposal facility will be intercepted with temporary cut-off drains. These drains will divert the flow around the ash co-disposal facility footprint, into the clean water system after passing through retention/settling dams.
- iv. Within the ash co-disposal facility disposal facility temporary artificial channels to be constructed on the exposed ash surfaces to lead stormwater down the faces to the dirty water collection channels in a controlled manner thereby preventing erosion and pooling of water.
- v. Dirty water concrete channels have been constructed within the ash co- disposal facility to channel away dirty stormwater and water used for the irrigation of the ash to the ADDD.
- vi. The ADDD has been built to handle the capacity of a one in 50 year, 24 hr storm event.
- vii. The Emergency Ash Dam (EAD) will consist of a concrete lined area of approximately 1.4 ha, sloped to fall with a concrete trapezoidal drain on two adjacent sides and a concrete rectangular channel drain on the other two sides that joins the trapezoidal drain.
- viii. The Station Dirty Dam (SDD) receives all the dirty water from the power plant. Gravity pipelines flowing from the Coal Stockyard Settling Tanks (CSY ST) and the Station Dirty Dams Settling Tanks (SDD ST) will also flow to the SDD using the down gradient of the slopes running North West of the power station.
- ix. The SDD is designed to contain all of the dirty water runoff from the Kusile Power Station for the 1:50 year, 24 hour duration storm event.
- x. The SDD ST can handle the dirty water runoff from its inflow sources for the 1:50 year, peak instantaneous storm event including an emergency spillway to accommodate larger events.

Figure 4-2 below shows the various existing and planned infrastructure mentioned above.

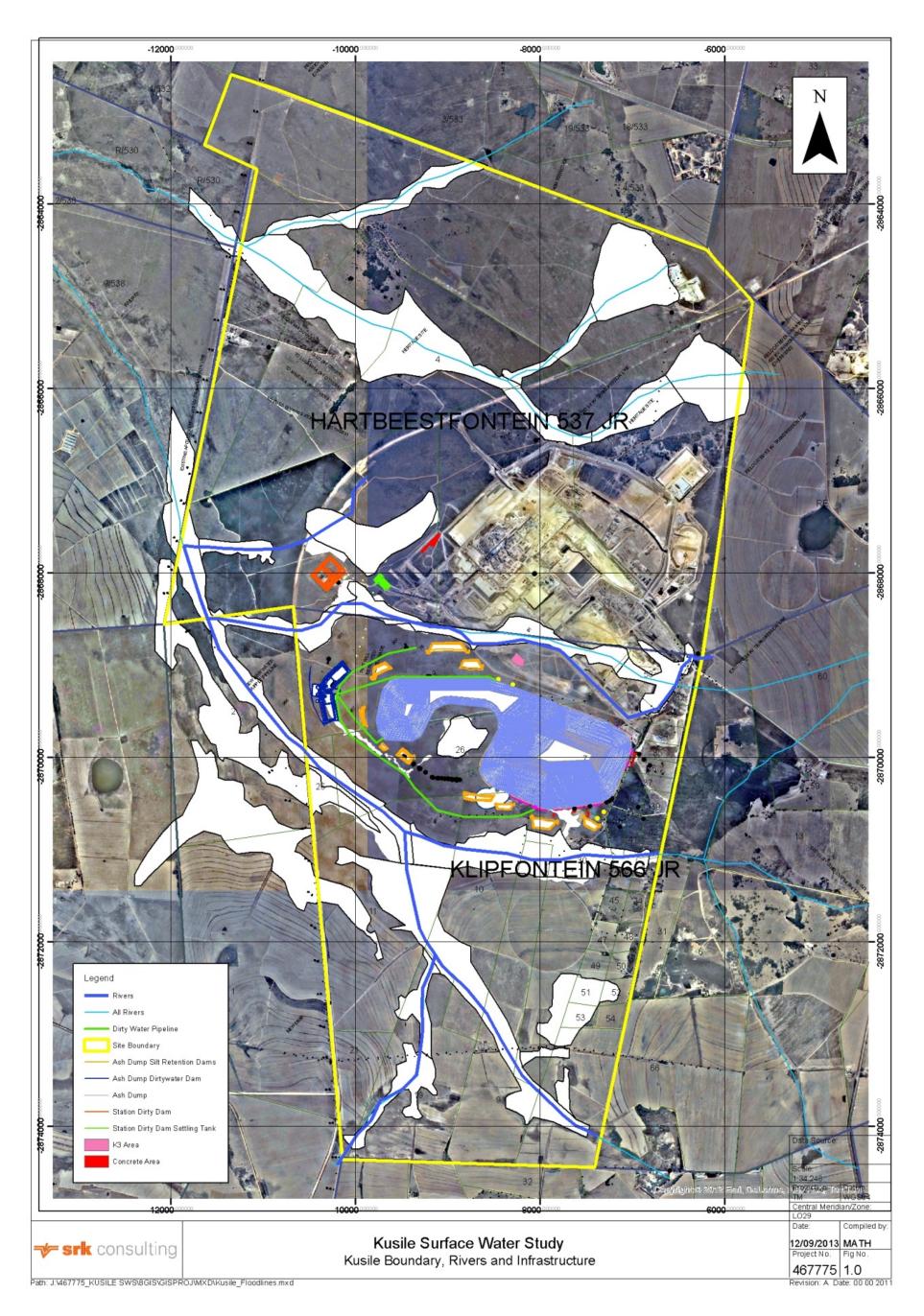


Figure 4-2: Kusile Site Boundary and Infrastructure

4.6 Assessment of current drainage system

The current drainage system is still in its infancy as the power plant is not operation as yet. Storm water diversion culverts and berms are operational around the construction of the various dirty water dams and the ash disposal facility and are compliant at this point as per the site visit conducted on the 11 of September 2013.

4.6.1 The Ash Co-disposal Facility Clean and Dirty Water Systems

The dirty and clean water collection system for the Ash Co-disposal facility were designed by Panel B Consultants Joint Venture (Panel B Consortium joint Venture PBC JV#19, 2008) The Ash Co-disposal facility clean water system was designed to handle a 1:100 year/ 24 hour storm event and the Ash Co-disposal facility dirty water was designed for a 1:50 year/24 hour duration storm.

SRK determined the Ash Co-disposal facility dirty catchment areas that will contribute the dirty water runoff and determined the peak flows that will be generated from these dirty water catchments. The dirty water canal running around the ash co-disposal facility that will collect the ash co-disposal facility dirty water were sized based on the calculated 1:50 year and 1:100 year peak flows, a minimum of 1:200 canal slope, A 2.5m base with a manning value of 0.018.

The **Table 4-5** below shows the dirty water canal sizes around the ash co-disposal facility that can handle the generated peak flows:

Catchment Name	Area km2	Length m	1:50 Year Peak Flow	1:100 Year Peak Flow	1:50 Year Flow Depth	1:50 Year Flow Velocity	1:100 Year Flow Depth	1:100 Year Flow Velocity
AD1	0.21	355.75	3.47	4.42	0.53	2.15	0.61	2.31
AD2	0.08	181.90	2.13	2.71	0.4	1.84	0.46	1.98
AD3	0.19	303.21	3.77	5.50	0.56	2.2	0.7	2.47
AD4	0.27	635.45	3.54	5.20	0.54	2.16	0.67	2.43
AD5	0.19	424.42	2.97	3.78	0.49	2.04	0.56	2.2
AD6	0.42	636.45	5.50	7.01	0.7	2.47	0.8	2.65
AD7	0.16	440.55	2.47	3.63	0.44	1.93	0.52	2.12
AD8	0.19	324.97	3.25	4.77	0.51	2.1	0.64	2.37
AD9	0.13	428.34	2.02	2.97	0.39	1.8	0.49	2.04
AD10	0.07	176.17	1.93	2.84	0.38	1.78	0.47	2.01
AD11	0.07	335.62	1.18	1.74	0.28	1.51	0.35	1.72
AD12	0.11	377.74	1.78	2.62	0.36	1.73	0.45	1.96

Table 4-5 Dirty Water Canal Sizes to accommodate the generated peak flows

A system of clean water drain will be developed to collect clean water from undeveloped area of the power station and divert the clean water from the ash co-disposal facility towards the natural watercourse. The clean water undeveloped catchment areas were determined and peak flows generated using Rational method to determine the clean water channel sizes. The channels were sized based on the calculated 1:50 year and 1:100 year peak flows, a minimum of 1:200 channel slope, a 2.5m base with a manning value of 0.018.

The details of the clean water channel sizes are given in Table 4-6 below

1.95

2.05

1:100 1:100 1:100 1:50 Year 1:50 Year 1:50 Year Catchment Area Length Year Year Year **Peak** Flow Flow Name km² Peak Flow Flow m **Flow** Depth Velocity **Flow** Depth Velocity CW1 623.62 2.04 3.00 0.17 0.39 1.81 0.49 2.05

2.87

Table 4-6: Clean water Cannel Sizes

863.26

CW2

0.17

A series of clean water drains around the perimeter of the ash co-disposal facility were also designed by Panel B Consultants Joint Venture for the purpose of receiving clean storm water run-off from rehabilitated surfaces of the ash co-disposal facility. The clean water drains will discharge the clean water from the rehabilitated ash co-disposal facility to the silt retention dams before discharging to the natural stream.

0.38

1.78

0.48

The Ash co-disposal facility clean- and dirty water areas are indicated in Figure 4-3

4.6.2 The Ash Co-disposal Facility Dirty Dam Co-disposal facility

The ash co-disposal facility dirty dam was designed for a 1:50 year/ 8 day storm (Detail Design Report 5452-90-011 Rev7 by Panel B Consortium joint Venture PBC JV#19, 2008). Dirty water from the ash co-disposal facility will be collected into the dirty water canal running along the perimeter of the ash co-disposal facility. The dirty water in the canal will be transported into the ash co-disposal facility dirty dam via a system of dirty water drain pipes. The ash co-disposal facility dirty dam has a design total storage capacity of 227, 410 m3. This storage will accommodate the ash co-disposal facility dirty water, Make-up water, dust suppression water and irrigation water. The 1:150 year and 1:100 year dirty water volumes for each of the dirty water sub-catchments were determined and are given in the Table 4-8 below:

Table 4-7: Dirty Water Catchments Volumes

Catchment Name	1:50 Year Volume (10³ m³)	1:100 Year Volume (10 ³ m ³)
AD1	9.0	11.3
AD2	3.3	4.2
AD3	5.8	8.4
AD4	5.4	8.0
AD5	6.4	8.0
AD6	14.3	18.1
AD7	3.8	5.5
AD8	8.5	12.4
AD9	3.1	4.5
AD10	4.1	6.1
AD11	3.0	4.5
AD12	3.8	5.5
CW1	4.3	6.3
CW2	5.9	8.6
Total	70.5	96.6

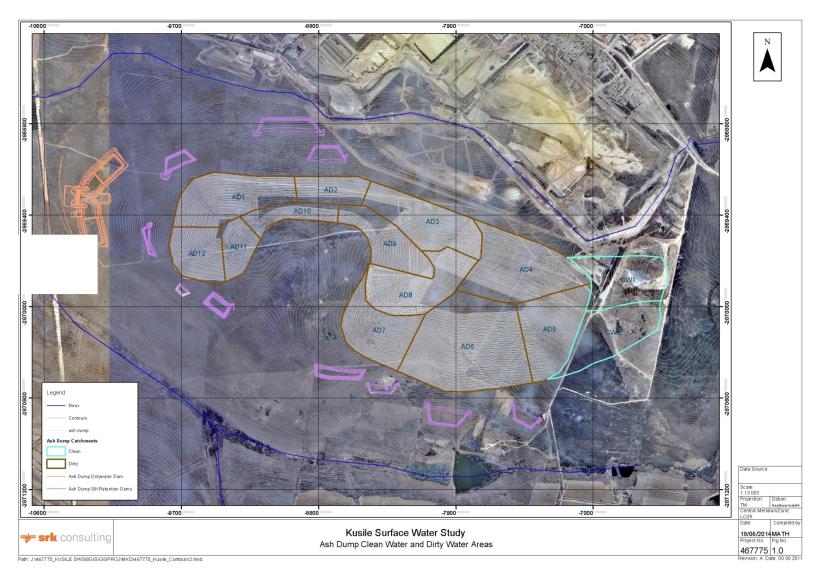


Figure 4-3: Ash Co-disposal Facility Clean Water and Dirty Water Catchments

4.7 Assessment of Current Pollution Control Dams

In addition to assessing the existing drainage system, the current dirty dams also need to be assessed .These too are in the construction phase as can be seen in Figure 4-4 below.



Figure 4-4: Construction progress on the Station Dirty Dam as of 11 September 2013

This assessment is needed though in terms of GN 704 storage facility requirements. A need therefore exists to define the future storage capacity of the holding facilities as well as the expected operating level and stormwater runoff entering the dam. The following approach has been adopted:

 Determination of the initial storage capacity based on information from (Panel B Consortium_ PBCJV TO#31, 2010) Table 4-8 shows the various waste dirty dams and their storage capacity.

Table 4-8: Summary of the quantity of waste to be received once the dirty dams are operational.

Waste Site	Size of facility for a waste management activity	The quantity of waste to be received once operational	Type of Facility
Ash/Gypsum co-disposal facility	The footprint of the ash/gypsum co-disposal facility is approximately 250 ha	The total waste storage for the Ash/gypsum disposal facility will be 84 423 000 m3.	Ash is classified as non- hazardous waste and gypsum is classified as a moderate hazardous waste therefore, the mixture is classified as a moderate hazardous waste. The co-disposal of ash and gypsum will

Waste Site	Size of facility for a waste management activity	The quantity of waste to be received once operational	Type of Facility
			require a class H: h (LB+) waste disposal facility.
Ash Co-disposal Facility Dirty Water Dam	The ADDD will be approximately 7.01 ha.	The total waste storage volume of the ADDD will be 227 410 m3.	The dirty water collection channels from the Ash/gypsum co-disposal facility will be routed to the ADDD. The ADDD is therefore classified as a hazardous waste disposal facility.
Station Dirty Water Dam	The footprint of the SDD is approximately 5.615 ha.	The design storage capacity of each dam with the sloping floors is 181 890 m3.	The Station Dirty water Dam is classified as a hazardous waste facility.
Station Dirty Dam Settling Tank	The footprint of the Station Dirty Dam Settling Tank is approximately 0.8 ha.	The waste storage volume of the Station Dirty Dam Settling Tank will be 7 975 m3.	The Station Dirty water Dam Settling Tank is classified as a hazardous waste facility.
Rock Stockpile Areas	The footprint of the Concrete Spoil stockpile will be approximately 9.6 ha and the K3 stockpile will be approximately 4.84 ha.	The total waste storage volume of the concrete spoil stockpile and K3 stockpile will be approximately 229 500 m3 and 750 000 m3 respectively	The rock stockpile is classified as General Waste. It will primarily consist of silty soils and degradable rock not suitable for use as general backfill.

In addition to the above the required minimum "surge" volumes are applicable to the following dirty dams given below. The surge volume is defined as the spare storage capacity of the dam needed at any point in time to contain the 24-hour runoff volume from the dam catchment due to a 1:50 year storm event. Relevant details on the above are given in this section

- i. The ADDD has been built to handle the capacity of a one in 50 year, 8 day storm event.
- ii. The SDD ST can handle the dirty water runoff from its inflow sources for the 1:50 year, peak instantaneous storm event including an emergency spillway to accommodate larger events.

4.8 Natural Water Courses and Floodlines

The Kusile Power Plant river catchments all drain into the Wilge River. The Klipfonteinspruit and its tributaries have a total catchment area of 60.4 km² The upstream part of the tributary of Klipfonteinspruit that originally ran through the coal stock yard was diverted into a channel that runs on the south eastern and south western side of the coal stock yard and joins the natural river on the western side of the coal stockyard. Floodlines were determined for the Klipfonteinspruit and its tributaries including the diverted channel and the Floodline report and drawings are given as an addendum in Appendix A.

Conclusions from the Floodline report is in

5 Floodline Determination and Results

The 1:50 and 1:100-year floodlines were determined based on the HECRAS model and peak flow rates as given in the report in Appendix A: Floodline Study.

Details and certified floodlines are shown on drawing 467775/001 in the same report

From the floodline study, the following was observed:

- The existing development and infrastructure is not affected by the 1:50 year and 1:100 year floodlines. Nm
- The diverted channel running on the south eastern and south western sides of the coal stock yard can handle the 1:50 year and 1:100 year flood events.

The floodlines are shown in Figure 5-1 below.

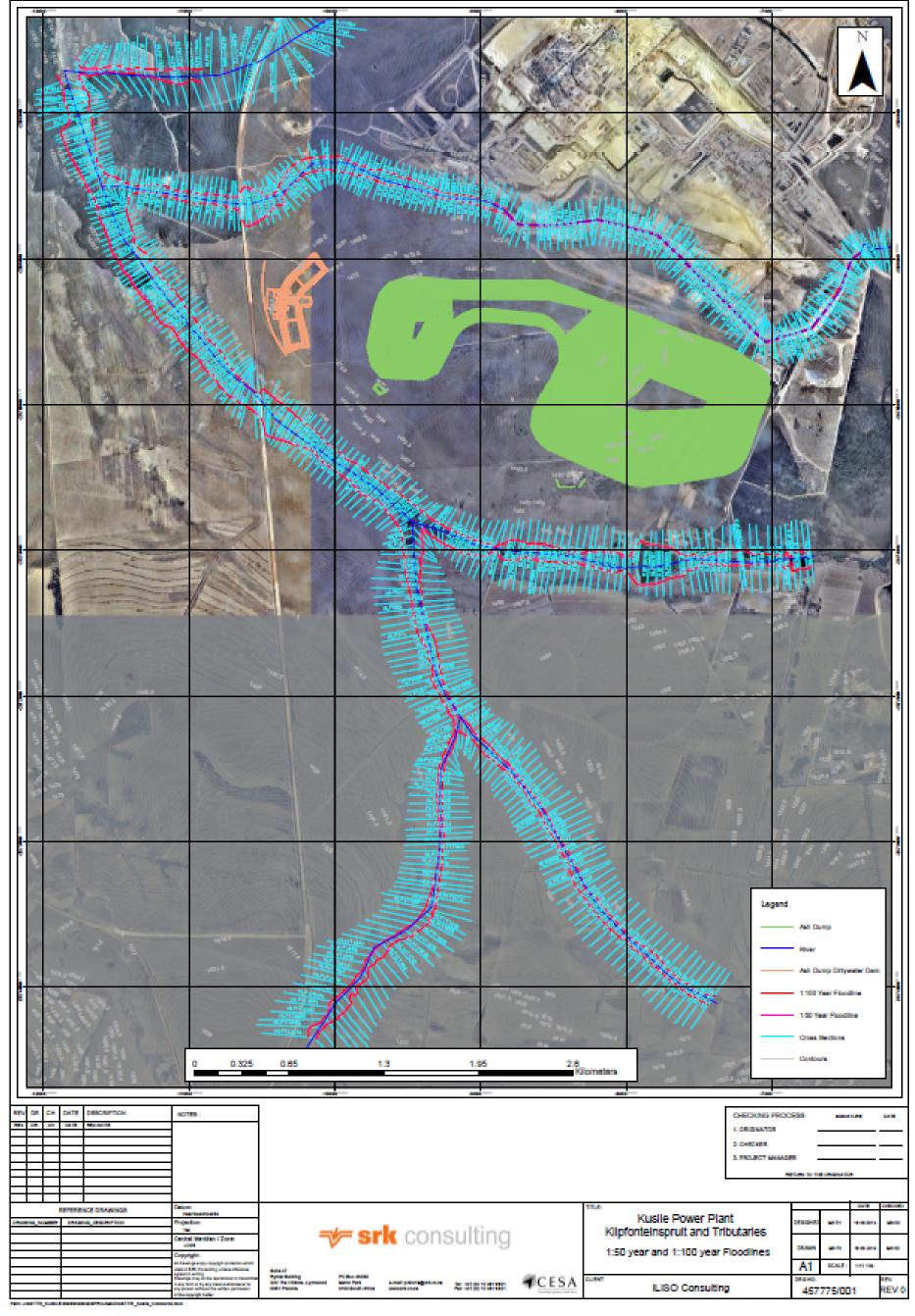


Figure 5-1: Kusile power Plant Klipfonteinspruit and Tributaries 1:50 and 1:100 year Floodlines

6 Water Quality Overview

6.1 Water Users downstream from Kusile Power Station

The land use downstream from Kusile and surrounding the power station is dominated by maize, grazed fields, coal mines and power stations. Water bodies are the only land use regarded as sensitive. The most sensitive user here is however the domestic use. The various applicable water user requirements are shown in Table 6-1. Available water quality results is evaluated against the target value for the most sensitive user for that specific parameter

Table 6-1 Various Water Quality Standards, General Limits and Guidelines for different water users

Variables	General limit, Guide	eral limit, Guidelines and Standards						
	GA	GA Stds Guidelines						
(mg/l unless otherwise specified)	General Limit values for up to 2000m³/d	Lifetime SANS241: 2011 consumption	Domestic use (sulfate from WHO Guideline, 2004)	Bu	dry	ivestock watering	ırrigation	Aquatic ecosystems
pH Value @ 23°C	Gene 7. 7. 7. 9. 9. 9. 9. 9. 9. 9. 9	Consideration 5.0-9.5	Dome 5.0-9.5	Bathing 8.6-5.4	Fanuqu 5.0-10	Ns Ns	6.5-8.4	enbV 6.5 – 9.0 ²
Conductivity (mS/m @ 22°C)	70 mS/m above intake to a maximum of 150 mS/m	170	150	520	Ns	40-270	Ns	Ns

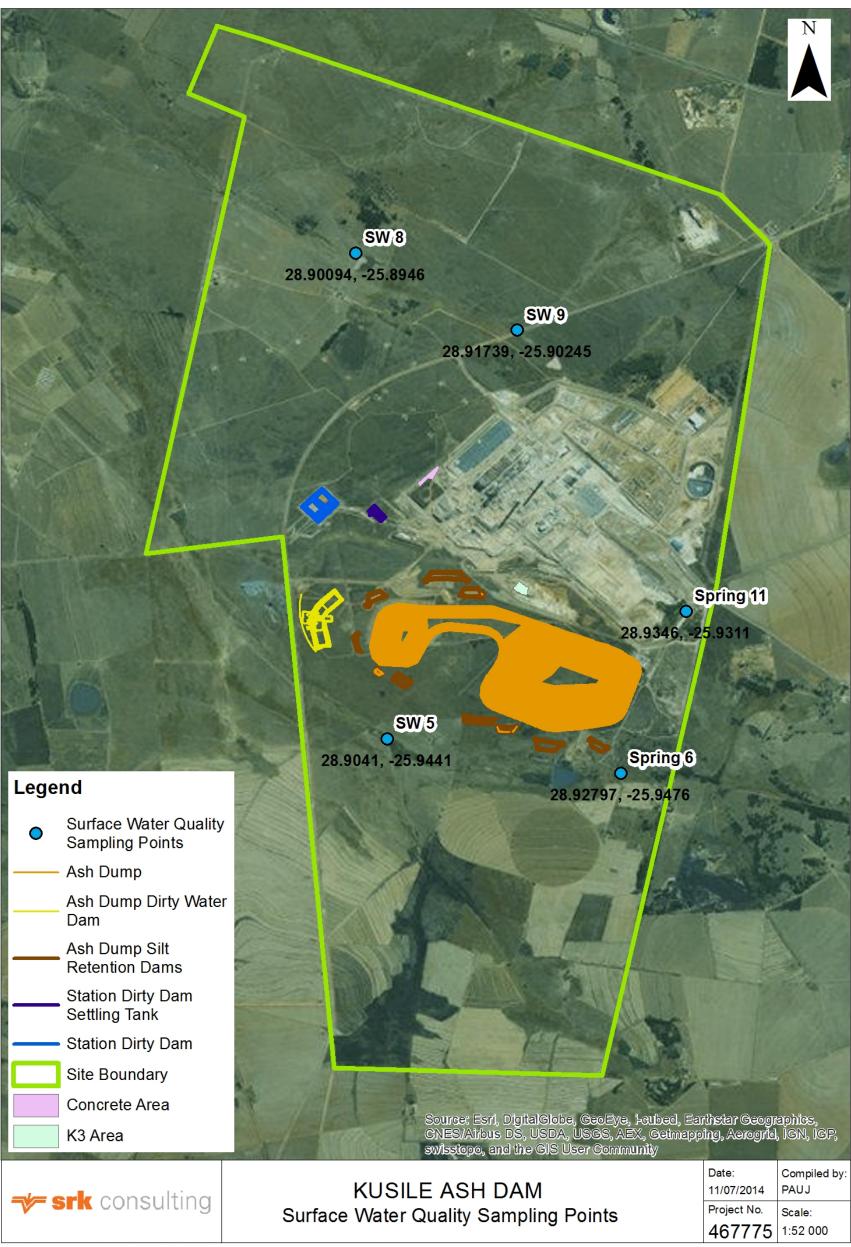
Variables	General limit, Guidelines and Standards								
	GA	Stds	Guidelines						
(mg/l unless otherwise specified)	s for up to	SANS241: 2011	ite from WHO						
	 General Limit values for up to 2000m³/d	Lifetime consumption	Domestic use (sulfate from WHO Guideline, 2004)	Bathing	Laundry	Livestock watering	Irrigation	Aquatic ecosystems	
Total Dissolved Solids		1200	1000	3400	1000-5000	260-1775	260 ^{&}	<15% change from normal cycle; no change in amplitude/frequency of cycles	
Calcium, Ca		Ns	150	80	1000	Ns	Ns	Ns	
Magnesium, Mg		Ns	100	70	500	500-1000	Ns	Ns	
Sodium, Na		200	200	Negligible effects	2000	0-2000	70 ^{&}	Ns	
Sodium as SAR							1.5 soil 2.0 crop		
Potassium as K		Ns	50	500	Ns	Ns	Ns	Ns	
Sulfate, SO ₄		500 ^{&}	500	600	1000	Ns	Ns	Ns	
Chloride, Cl		300	200	No effects	2000-3000	100-700	100 ^{&}	Ns	
Nitrate as N	15	11	6	20		Ns	Ns	Ns	
TIN									
Fluoride, F	1	1.5	1	No effects	02-Jun	2	2	1.5	

Variables	General limit, Guidelines and Standards								
	GA	Stds	Guidelines						
(mg/l unless otherwise specified)	s for up to	SANS241: 2011	te from WHO						
	General Limit values for up to 2000m³/d	Lifetime consumption	Domestic use (sulfate from WHO Guideline, 2004)	Bathing	Laundry	Livestock watering	Irrigation	Aquatic ecosystems	
Free and Saline Ammonia as NH ₄	6	1.5			Ns	Ns		0.015 as unionised ammonia	
Aluminium as Al		0.3	Ns	Ns	5	5	5	0.01	
Iron as Fe	0,3	2 (health)	1	5	10	0.02: equipment	5	0.32	
		0.3 (aesthetics)				0.1: crops			
Manganese as Mn	0,1	0.5 (health)	0.4	0.1	10	0.2: equipment	0.02 ^{&}	0.37	
		0.1 (aesthetics)				5: crops			
Zinc as Zn	0,1	5	3	No effects	No effects	20	0.001	0.0036	
Boron as B	1	Ns						Ns	

6.2 Water Quality Assessment

Water quality information was taken from the monthly water monitoring program conducted by Zitholele Consulting and contained in the report No: 12926:9 (September 2013). As several of the sampling points are not perennial only 30 of the 47 sampling points yielded any water. The positions of the monitoring points are provided in Figure 6-1. No new sampling was undertaken for this study under this contract.

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Path: J:\467775_KUSILE SWS\8GIS\GISPROJ\MXD\467775_Sampling_Points_11072014.mxd

Figure 6-1: Water Sampling Points

6.2.1 Water Quality Results

The analysis of results in this report is based on sampling taking place, on a monthly basis from the last quarter in 2008 until middle 2012. SW 8 and 9 were however only sampled twice and four times respectively and therefore the level of confidence on these samples results are lower. The significance of the surface water sampling points to the ash co-disposal facility is shown in the Table 6-2 below.

Table 6-2: Surface Water Sampling Points relevant to the Ash Co-disposal Facility

Site Name	Y co-ord	X co-ord	Site Type
Spring 6	-25.94760	28.92797	Spring to the south of the Ash co-disposal facility. Water quality of this spring could be an indication of the groundwater quality
SW5	-25.94410	28.90410	Surface water point upstream of the Ash co-disposal facility in the Klipfontein Spruit after confluence with the Holfontein spruit
Spring 11	-25.93110	28.93460	Spring to the north of the Ash co-disposal facility. Water quality of this spring could be an indication of the groundwater quality
SW 8	-25.8946	28.90094	Surface water point north to the dam in a small un named tributary of the Klipfontein Spruit (Regarded as downstream of activities)
SW 9	-25.90245	28.91739	Surface water point north to the dam in a small un named tributary of the Klipfontein Spruit (Regarded as downstream of activities)

Table 6-3: Summary of the Surface Water Quality Results taken between 2008 and 2012 of relevant surface points

Sample ID	рН	EC (mS/m)	Dissolved Solids (mg/L)	Suspended Solids (mg/L0)	Turbidity (NTU)
Spring 6					
Max	7.80	84.0	680.0	32.80	22.80
Med	7.3	54.0	383.0	5.20	5.13
Min	7.3	1.29	67.0	0.8	1.46
Number of samples	44	44	44	36	32
Spring 11					
Max	9.28	39.0	248.0	408.0	392.0
Med	6.96	7.2	48.0	11.0	10.5
Min	6.11	6.0	36.0	0.2	0.53
Number of samples	36	36	36	34	27
SW8*					
Max	7.7	11	84	150	389
Med					
Min	7.3	1.06	73	84	62
Number of samples	2	2	2	2	2
SW5					
Max	8.03	38	240	142	22.8

Samp	le ID	рН	EC (mS/m)	Dissolved Solids (mg/L)	Suspended Solids (mg/L0)	Turbidity (NTU)
	Med	7.98	34	32	32	5.13
	Min	7.6	9	74	8.2	1.46
Nun	nber of samples	44	44	44	44	44
SW9**	k					
Max		8.03	38	240	142	188
Med		7.98	34	226		39
	Min	7.6	9	74	32	36.7
Nun	nber of samples	4	4	4	4	4
uality nes	Ideal	6.0-9.0	0-70	0-450	No	0-1
*Water Quality Guidelines	Marginal/No Health effect	4-6,9-11	71-150	450-1000	Guideline Value	1-5
*	Unacceptable	<4, >11	>300	>1000		>5

^{*} Only two samples were taken during the monitoring period and therefore the reliability of this data is low

- 1. Colour coding is used to denote whether values measured comply with the South African Water Quality Guidelines (DWAF, 1996).
- 2. Where the lab gives results concentrations as $\mu g/l$ and the South African Water Quality Guidelines (DWAF, 1996) gives concentrations as mg/l, the guideline values were converted to $\mu g/l$

6.2.2 Turbidity

All 5 surface water sites showed high levels of turbidity. Turbidity levels at monitoring site SW 5, are classified as having marginal / no health effects whilst SW8, SW9 and both spring water points being classified as unacceptable for domestic use (according to the SAWQG). The turbidity and the suspended solids are normally correlated and therefore no discussion on suspended solids is further given

Turbidity in surface water sites over time is shown in Figure 6-2 below. The graph shows that:

- Turbidity levels in surface water are cyclical;
- Turbidity levels spike early in the rainy season, which is expected as surface water systems flush after the first high rainfall events;
- The graph also indicates that the water quality is deteriorating, as progressively more sites show elevated levels of turbidity, which might be due to increased construction activities in the area.

^{**}Only four samples were taken during the monitoring period and therefore the reliability of this data is low

^{*** (}Department of Water Affairs and Forestry, 1996)

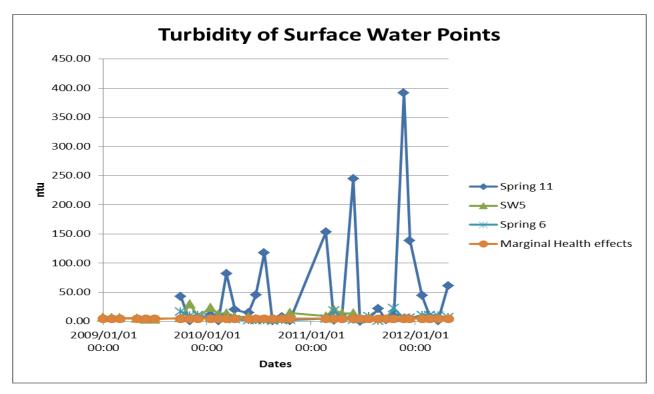


Figure 6-2: Turbidity of surface water points compared to Marginal health effects for domestic water use

6.2.3 Electrical Conductivity (EC)

The total dissolved solids (TDS) are a measure of the quantity of various inorganic salts dissolved in water. The TDS concentration is directly proportional to the electrical conductivity (EC) of water. Since EC is much easier to measure than TDS, it is routinely used as an estimate of the TDS concentration. Therefore only the EC will be discussed here. The trends of the SW5, Springs 6 and 11's conductivity can be seen in Figure 6-3 below.

For the period sampled, only spring 6 has occasionally exceeded the ideal limit for domestic use as can be seen in Figure 6-3.

Spring 11 shows a very blow conductivity compared to the Spring 6 and SW 5. No upward trend (which at this time and stage can be expected, is detected. These sampling points all present good background values before activities have started. Insufficient sampling has taken place at SW8 and SW 9. However, the few samples taken all were within the ideal range for domestic use.

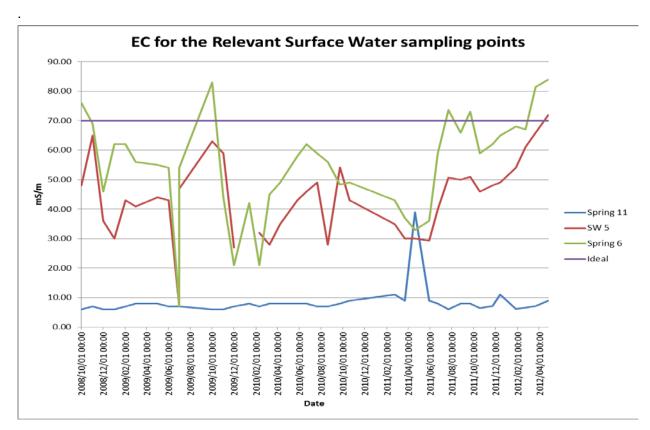


Figure 6-3: Electrical Conductivity trends for sampling done (2008- 2012)

Notes: SW 8 and 9 is not included due to lack of data

6.2.4 pH

pH values for all three sampling points were mostly all within the ideal range for domestic use with Spring 11 only on one occasion having an increased pH which still fell within the No effect range. No conclusion could be drawn as to why this reading was so different due to a lack of verified field data of that time.

Not enough sampling has taken place at SW8 and SW 9. However, the few samples taken all were within the ideal range for domestic use.

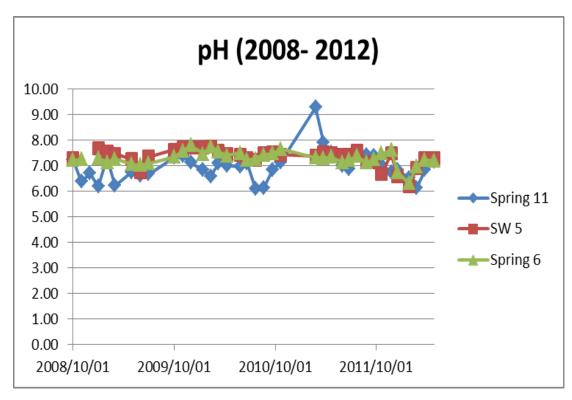


Figure 6-4: pH trends for SW5, Spring 6 and 11

6.2.5 Macro-constituents

The analysis results for macro-constituents measured in surface water samples are show in Table 5-4 below. The median value is indicated.

The surface water sites of relevance to this ash co-disposal facility are within the ideal water quality range according to the SAWQG for Domestic Use with the exception of:

- SW 5 with a calcium concentration (59.05 mg/l) within the marginal to no health effects
 range and spring 6 with a calcium concentration of (80.2) which falls just within the
 unacceptable level.
- Sulfate on levels in spring 6 exceeds the ideal level for domestic use and falls within *the marginal/ no health effects range*
- All other parameters are within the ideal range

Table 6-4: Summary of the macro constituents of surface water quality (median values0

Sample ID		Potassium (K) mg/l	Sodium (N) mg/l	Chloride (Cl) mg/l	Fluoride (F) mg/l	Nitrate(NO ₃) mg/l	Sulfate (SO ₄) mg/l	Calcium (Ca) mg/l	Magnesium (Mg) mg/l	Ammonia As N mg/l
Spring 6		2.4	6.1	3.9	0.2	0.5	234	80.2	13.8	³ <2.5
Spring '	Spring 11		5.2	2.9	0.00	1.6	4.2	5.5	2.5	<2.5
SW5		2.3	8.3	4.6	0.3	0.2	167	59.1	12.1	<2.5
SW 8		3	7.3	4.05	0.26	0.1	9.64	7.1	3.7	
SW 9		3.42	14.20	8.66	0.26	0.18	60.64	27.10	15.80	<2.50
	Ideal	0-50	0-100	0-100	0-1.0	0-6	0-200	0-32	0-50	0-1
Water Quality	Marginal/No Health effects	50-100	100- 200	200- 600	1.0-1.5	6-10	200-400	32-80	50-100	1-10
Unacceptable		>100	>200	>1200	>1.5	>10	>400	>80	>100	>10

Table Notes:

- 1. Colour coding is used to denote whether values measured comply with the South African Water Quality Guidelines (DWAF, 1996).
- 2. Where the lab gives results concentrations as $\mu g/l$ and the South African Water Quality Guidelines (DWAF, 1996) gives concentrations as mg/l, the guideline values were converted to $\mu g/l$
- 3. The median value has been
- 3. Method for using for analysis's detection level is higher than the ideal water quality limit
- 4. SW8 maximum values are reflected since only 2 samples were taken over the period

6.2.6 Micro-constituents

Only aluminium manganese and iron have been sampled on a regular basis in the surfaces water points and therefore only these constituents are discussed below

Aluminium

The analysis results for aluminium measured in surface water samples are shown in Table 6-5 below Maximum Aluminium concentrations at, SW 5, SW8 and SW 9 and Spring 6 and Spring 11 all are unacceptable for use for human health. Since these are maximum values they may not be a true reflection of the real aluminium concentration of the surface water since the median values, except for Spring 6, is significant lower than the maximum level. The potential for erroneous conversions of measuring units may also be the reason for the discrepancy. Analysis of results was based on data supplied by the client.

Spring 11's median value indicates that use for domestic consumption may have marginal to no health effect. However SW5 has a median value which is unacceptable for human consumption have marginal to no health effects. According to the SAWQG the aluminium concentrations of the remaining sites are unacceptable for domestic water use, According to samples taken previously the following trends can be seen with the aluminium concentrations:

- Aluminium concentrations seem to be cyclical, with spikes during the rainy seasons.
- Trends indicate a drop in aluminium levels during the dry seasons over time,
- · Water quality with regards to aluminium concentrations seems to be stable over time; and
- There is a strong correlation between aluminium concentrations found in sediment samples and aluminium concentrations found in water samples. (Zitholele Consulting, 2013)

Table 6-5: Aluminium Concentrations as measured between 2008 and 2012 in the various surface sampling points

Sa	mple ID	рН	Aluminium Max(mg/l)	Aluminium Med(mg/l)	Aluminium (Min)					
Spring 6	<u> </u>	7.3	32.20	<0.03	<0.03					
Spring '	11	6.96	2.64	0.36						
SW5		7.98	65.70	7.45	0.03					
SW8		7.7	251	0.47	1.5					
SW 9		7.8	186		0.26					
ity	Ideal	0-1.0mg/l								
Water Quality Guidelines	Marginal/No Health effects		1 -2.5							
% On On	Unacceptable	>2								

Aluminium oxide and hydroxide are amphoteric, that is, they are insoluble in water around neutral pH, but dissolve under strongly acidic or strongly alkaline conditions. As such, the interactions of aluminium are strongly influenced by pH, the chemistry of the aluminium hydroxide and the nature of available organic and inorganic complexing ligands. This being demonstrated, since the concentration of aluminium is lower in the Springs where the pH is closer to being neutral

6.2.6.1 Iron

The surface water sites show concentrations within the marginal to no health effects range with SW 5 having the highest concentration (20.0mg/l). According to samples taken previously the following trends can be seen with the iron concentrations:

- There are minor elevations of iron concentrations during rainy seasons over time;
- The iron concentration trend seems stable over time; and
- There is a strong correlation between iron concentrations in the sediment samples and iron concentrations found in water samples. (Zitholele Consulting, 2013)

The concentration of dissolved iron in water is dependent on the pH, redox potential, turbidity, suspended matter, the concentration of aluminium and the occurrence of several heavy metals, notably manganese. The natural cycling of iron may also result in the co precipitation of trace metals such as arsenic, copper, cadmium and lead.

Table 6-6: Iron Concentrations as measured between 2008 and 2012 in the various surface sampling points

Sample	e ID	Max(mg/l)	Med(mg/l)	Min(mg/l)
Spring 6		4.99	0.09	<0.03
Spring 11		11.18	3.06	0.0
SW5		20.0	0.3	<1.0
SW 8		4.14		1.43
SW 9		3.33	0.70	0.34
uality es	Ideal	0.1 -0.03	Very slight effects on taste and marginal other aesthetic effects Deposits in plumbing with associated problems may begin to occur. No health effects; the water is generally well tolerated	
Water Qual Guidelines	Marginal/No Health effects	0.03-30		
Mg Gu	Unacceptable	30-100	Long-term health effects gradually increase	

6.2.6.2 Manganese

Surface water sites, SW 8, and Spring 11 have concentrations within the marginal to no health effects range with SW 5 having the highest concentration. According to samples taken previously the following trends can be seen with the Manganese concentrations:

- Manganese concentrations fluctuate over time during wet and dry seasons;
- Manganese concentrations have no definite cyclical trend as seen with turbidity levels;
- There is an upward trend in manganese concentrations over time, thus deteriorating water quality; Manganese concentrations however, are mostly under the unacceptable threshold as far as water quality for domestic use goes.
- The median for spring 6 and SW 5 would indicate that the high values shown as maximums were possibly just spikes since the minimum is also particularly low

Table 6-7: Manganese Concentrations as measured between 2008 and 2012 in the various surface sampling points

Sample ID	Max(mg/l)	Med(mg/I)	Min(mg/l)
Spring 6	132	0.05	<0.03
Spring 11	1.43	0.04	<0.03
SW 8	103		0.01
SW 9	139	0.01	0
SW5	332	0.09	<1.0

A	Ideal	0-0.5	No health or aesthetic effects; marginal aesthetic problems occasionally found in the 0.02 -0.05 mg/l
Qualit	Marginal/No Health effects	0.05-20	
Water Quality Guidelines	Unacceptable	>20	Domestic use unlikely due to extreme aesthetic effects. Chronic toxicity: at high concentrations, possible acute effects

- 1. Colour coding is used to denote whether values measured comply with the South African Water Quality Guidelines (DWAF, 1996).
- 2. Where the lab gives results concentrations as $\mu g/l$ and the South African Water Quality Guidelines (DWAF, 1996) gives concentrations as mg/l, the guideline values were converted to $\mu g/l$.

Insufficient sampling of the other micro constituents was done over the sampling period. It is therefore not possible to make meaningful conclusions in terms of trends.

The water quality measured to date indicates that the water user requirements are being met and only aluminum and manganese showing elevated levels and falling within the unacceptable level for domestic water use. It is assumed that the higher levels are normal background levels since no activity as yet has taken place which could have increased these values

6.3 Water Quality Monitoring Program

The list of monitoring points relating to the ash disposal facility and associated infrastructure are summarised in Table 6-2. Additional to the sampling of the natural surface water points (which is sufficient for determining the impact of upstream activities and also the impact of the ash co-disposal facility on down stream activities), the sampling program should be extended to also include the following once the infrastructure has been built and commissioned.

- Ash Co-Disposal Facility Site Retention Dams;
- Ash Co-Disposal Facility Dirty water Dam;
- · Station Dirty Dam; and
- Station Dirty Dam Settling Tank

Sampling frequency should be as per the Kusile Water Use Licence issued by the Department of Water Affairs

6.3.1 Water Sampling Monitoring

Kusile to ensure that all their sampling procedures and methods are complying with the Water Use Licence

This will ensure that the data obtained can be confidently used to interpret water chemistry thus facilitating meaningful water modelling, risk assessment and the choice of suitable remedial measures.

7 Potential Environmental Risks and Mitigation Measures

For the purpose of this assessment the Ash co-disposal facility Disposal Facility is defined as the Ash Co-disposal facility, Ash Co-disposal facility Site Retention Dams, Ash Co-disposal Facility Dirty water Dam, Station Dirty Dam and Station Dirty Dam Settling Tank

This section identifies activities associated with the development and operation of the Dirty Dams and the Ash Co-disposal facility Disposal Facility that potentially can have an impact on the receiving surface water environment, for each major component of Ash Co-disposal facility development, being the construction, operational, closure and decommissioning phases. The general activities that are common to construction of an Ash Co-disposal facility and associated infrastructure are the following:

- Establishment of site access road and perimeter fencing;
- Establishment of contractors camp and lay-down areas;
- Removal of the vegetation;
- Removal and stockpiling of the topsoil;
- Earthworks and excavation of foundations for infrastructure e.g. roads, culverts, etc.;
- Provision of stormwater management measures;
- Construction of concrete structures;
- Phased construction of Ash Co-disposal facility basic infrastructure;
- Rehabilitation of disturbed areas after general site construction is completed;
- Operation of the Ash Co-disposal facility, on-going revegetation of slide slopes, maintenance and monitoring;
- Decommissioning and Closure of the Ash Co-disposal facility system once design capacity is reached;
- Rehabilitation of Ash Co-disposal facility top surface once decommissioning is completed;
- Post Closure including maintenance and monitoring.

Following the results from the water quality results taken in September 2013 and the historical data submitted by the water monitoring program there appears to be a deterioration of water quality over time as construction continues on the Kusile Power Plant. The high levels of aluminium and iron in the sediment samples contributes to higher concentrations being passed on into the water, combined with increased turbidity especially during the wet seasons.

The risks to surface water quality have already started with construction and mitigation measures will need to be applied to minimise the effects thereof. Table 7-1 below details the environmental risks with their associated mitigation measures.

A floodline study was undertaken to assess the placement of the infrastructure in relation to surface water bodies. The report is attached as Appendix A: Floodline Study Report.

Table 7-1: Environmental Risks and Mitigation Measures

Environmental Risk Construction Phase List of activities associated with construction phase: Construction of Ash Co-disposal facility Disposal Facility; Construction of Ash Co-disposal facility Dirty Dam; Construction of Station Dirty Dam; Construction of Station Dirty Dam Settling Tank;

Environmental Risk Mitigation Measure/s Construction of Emergency Ash Dump Area; Construction of the flue gas desulphurisation wastewater treatment plant; Construction of clean water diversions; and Construction of Spoil Areas - Concrete Spoil Stockpile and the K3 Stockpile Increase in turbidity of surface water during construction The runoff from the upstream clean water catchment is to caused by an increase in runoff from the cleared and be diverted away dirty water dams and ash dump disposal stripped areas or from topsoil stockpiles which is high in facility. Temporary surface water ditches are to be suspended solids (Aluminium, Manganese, and Iron). constructed on the upstream boundary of the ash dump, which will meet regulation 704 requirements regarding the separation of clean and dirty water runoff. All clean water runoff will therefore be diverted away from the cleared Accidental spillages of hazardous substances from Management measures regarding the maintenance of all construction vehicles used during the site clearing and Power Plant vehicles must be undertaken. This will ensure grubbing. that any spillages or leakages of fuel and oil are reduced. Reduction of catchment yield as a result of the footprint The loss of catchment area as a result of the dirty water areas of the dirty water dams and the Ash Dump Disposal dams and the Ash Dump Disposal Facility and other Facility. The footprint areas will no longer form part of the associated infrastructure cannot be mitigated. The only natural downstream catchment thereby potentially resulting way to mitigate the above mentioned impacts is to not in a decrease of runoff downstream proceed with the Power Plant which has already started. Therefore the impact rating for pre and post mitigation measures will remain unchanged. Increase of surface runoff and potentially contaminated Within the cleared area along the downstream boundary of the Ash Dump Disposal Facility, temporary ditches are to water that needs to be maintained in the areas where site clearing and grubbing occur. be constructed along with temporary excavated storage areas. All dirty water runoff will then be captured and contained within the temporary storage facility. Excess storage of rainfall within the dirty water dams and During the period of construction of the dirty water dams and settling tanks, high storm events could result in settling tanks during the construction phase. excessive ponding within the dirty water dams and settling tanks. Depending on the extent of the ponding this water could either be allowed to remain and evaporate naturally or it could be pumped out. Separation of clean water runoff upstream of the dirty water Based on Reg 704 requirements regarding stormwater dams and settling tanks. Water upstream of the dirty water management it is noted that all clean and dirty water must dams and settling tanks is considered clean and will have be separated. Therefore clean water emanating from to be separated from the dirty water area. Dirty water upstream of the dirty water dams and settling tanks will be Spillages from the dirty water dams and settling tanks into diverted away and discharged to the nearby watercourse or environment. The clean water diversion will be sized to the environment must be managed. accommodate the 1:50 year storm event. The dirty water dams will also have a minimum freeboard from spillway to crest of 0.8 m as per Reg 704 requirements.

Operation Phase

List of activities associated with operation phase:

Dumping of ash/gypsum into the ash dump disposal facility;

The dirty water collection channels from the ash dump disposal facility will be routed to the Ash dump dirty dam;

Ash and gypsum will be delivered by conveyor to a radial stacker near the ash/gypsum disposal facility, for subsequent loading, hauling and placement into paddocks;

The Emergency Ash Dump (EAD) will be used occasionally for the temporary storage of quenched ash for periods of up to 24 hours, before being removed for permanent disposal on the appropriately licensed waste disposal facility;

All potentially contaminated water on the Kusile Power Station will be managed in the Station Dirty Dam;

Stormwater management infrastructure operation, monitoring and maintenance;

Air and Water Quality Monitoring (surface & groundwater);

The Station Dirty Water Dam Settling Tanks (SDD ST) will receive gravity discharges of dirty water from the power station terrace.

Spillages from the dirty dams and wastewater treatment

A monitoring program for structural maintenance of the

Accidental spillages of hazardous substances from

of the power station.

decommissioning vehicles used during the closure phase

Environmental Risk	Mitigation Measure/s
plant.	dirty dams and wastewater treatment plant needs to develop and maintenance on leakages or spills should be carried out immediately.
Inadequate removal of silt will result in a steady decrease in the storage capacity of the SDD ST.	The SDD ST will consist of two equal capacity concrete basins that clarify contaminated water from the power station terrace before it travels by gravity pipeline to the SDD. The two compartments will allow for occasional maintenance and inspection access (preferably during the dry season) without interrupting the functionality of the SDD ST under normal circumstances.
Maintenance of upstream clean water controls.	Upstream clean water controls should be maintained regularly by site monitoring, to ensure no blockages by vegetation or debris occur. Also to ensure berm walls that has collapsed or have been damaged be repaired
Increase in volume of contaminated water that needs to be managed on the Kusile Power Station footprint.	A stormwater management maintenance program needs to be maintained regularly to ensure that the stormwater system is functioning sufficiently.
Closure Phase	
List of activities associated with closure phase:	
Demolishing and removal of infrastructure, dirty dams, etc.;	
Final rehabilitation and revegetation of top surface of Ash Du	mp;
Post-Closure Water Quality Monitoring (surface & groundwat	er);
Removal of clean water diversion.	
Seepage of water out of the Ash Dump into the environment.	A monitoring program of ground and surface water needs to be implemented and maintenance on any seepage needs to be carried out immediately if detected.

Management measures regarding the maintenance of all power plant vehicles must be undertaken. This will ensure

that any spillages or leakages of fuel and oil are reduced.

8 Methodology

A quantitative risk assessment methodology will be used for the risk assessment. This method makes use of the basic risk assessment approach of deriving an expression for risk from the product of likelihood and consequences. It works by attributing absolute values to likelihood (probability) and consequences. The methodology is summarised in Figure 8-1.



Figure 8-1: Summary of quantitative risk assessment methodology

The main objective of the risk assessment is to identify the negative impacts that can be avoided and/or mitigated and the benefits of the positive impacts during the construction and operation phases of the codisposal facility on the environment.

8.1 Phase 1: Identification of Risks

All the risks associated with the project (positive and negative) have been determined.

8.2 Phase 2: Quantitative Risk Assessment

The risk assessment will involve the quantification of the risks associated with the project. The potential significance of potential environmental risks identified has been determined using the significance rating as described below. The terminology has been taken from the Guideline Documentation on EIA Regulations as follows:

Severity / magnitude; Reversibility; Duration of impact; and Spatial extent.

Table 8-1: Consequence and probability ranking

Severity / magnitude(S)	Reversibility (R)	Duration (D)	Spatial extent (E)	Probability (P)
5 – Very high / don't know	1 – Reversible (regenerates naturally)	5 – Permanent	5 – International	5 – Definite / don't know
4 – High		4 – Long term (impact ceases after operational life)	4 – National	4 – High probability
3 – Moderate	3 – Recoverable (needs human input)	3 – Medium term (5 – 15 years)	3 – Regional	3 – Medium probability
2 – Low		2 – Short term (0 – 5 years)	2 – Local	2 – Low probability-
1 – Minor	5 – Irreversible	1 - Immediate	1 – Site only	1 – Improbable

Severity / magnitude(S)	Reversibility (R)	Duration (D)	Spatial extent (E)	Probability (P)
0 - None				0 - None

The maximum value which can be obtained is 100 significance points. The risks have been rated as High, Moderate or Low significance by combining the consequence of the impact and the probability of occurrence:

Consequence = severity + reversibility + duration + spatial scale Consequence X Probability = Significance

- More than 60 significance points indicate High environmental significance;
- Between 30 and 60 significance points indicate Moderate environmental significance;
- Less than 30 significance points indicate Low environmental significance.

0

9 Results of the Risk Assessment

9.1 Construction Phase

9.1.1 Surface water quality

Surface water quality in the catchment may be impacted upon during site clearing and construction of the Ash Dump and its associated infrastructure.

- Sedimentation caused by an increase in runoff from the cleared areas or from topsoil stockpiles which is high in suspended solids;
- Poor lateral drainage of access roads and Ash Dump base preparation where stormwater may pond alongside roads and preliminary construction berms;
- Soil compaction, causing an increase in runoff during rainstorm events increasing turbidity in the surface water.

The boundaries of the study area for the Ash Dump are situated within the catchment of the Klipfonteinspruit and its tributaries. The overall topography is generally flattish with undulating hills with local drainage lines within the Ash Dump footprint area. Water will tend to drain into the nonperennial tributaries of the Klipfonteinspruit. Therefore the probability that contaminated runoff will reach the Klipfonteinspruit and eventually the Wilge River via surface water drainage channels during the construction phase is considered probable, if not appropriately mitigated. The primary impact will be contained to the immediate area of the Ash Dump and its associated infrastructure. Although the impact will be of short duration during a storm event and sometime thereafter it will continue throughout the project thus the impact is considered for the duration of the project. Should the impact materialise it will deteriorate the functionality of the surface water which could make it unfit for use by any other water users. This may be the case during the dry winter months when the site drainage courses are dry and the water reaching the water courses will be the only source. The site is however located in a summer rainfall season with very low precipitation taking place during the winter months The potential impact will further be easily reversible since the Water Act requires that appropriate clean and dirty water segregation. The overall impact has been rated as having a **MODERATE** significance in Table 8-1. The probability that the impact may occur remains likely, particularly associated with the need to divert existing water courses around the Ash Dump footprint, and therefore the significance will not be reduced to a lower significance but the significance rating will be reduced from 56 to 36.

Catchment yield loss will occur with the construction of the Ash dump and associated infrastructure. These risks cannot be mitigated and is rated as **HIGH** as depicted in Table 8-1 below.

9.1.2 Accidental spillages of hazardous substances

The Ash Dump development increases the probability of localised accidental spillages of hydrocarbons (diesel, oils etc.) from earthmoving and construction equipment and transport of equipment and personnel to and from the site of hazardous substances. The impact will be contained to the site only and will be of a short duration as spillages can usually be remediated immediately.

Spillages and runoff from the construction camp construction activities:

Spillages at the construction camp will be contained to site and will be remediated continuously for the duration of construction. The contaminated runoff will be contained and reused as necessary e.g. for dust suppression. The potential intensity should this impact occur will be **MODERATE** as it may impact on the water quality. However all spillages will be contained to site but will probably reoccur for the duration of the construction phase. The impact has been rated as having a **LOW** significance once mitigated.

The probability that spillages and runoff from the bunded area within the contractors lay-down and vehicle maintenance areas will result in the contamination of surface water is unlikely. Contaminated water will be contained on site; spillages are expected to be remediated immediately therefore the risk will be for a short duration although the risk is considered for the duration of the construction phase.

9.1.3 Stormwater management

Stormwater management is one of the key issues that must be addressed in the surface water assessment. Due to the land clearing of vegetation and topsoil for construction purposes, construction of access roads, construction camps and the Ash Dump area and associated infrastructure, the compaction of soil, contaminated runoff from these areas will definitely increase resulting in an increase of the volume of contaminated water that needs to be handled on the Kusile Power Plant footprint. This is confirmed by the increases in turbidity, aluminium and iron concentrations in the surface water monitoring results. This water will be concentrated and either flow away in the tributaries or pond until it evaporates. The impact may not just be contained to site but could potentially enter the surface water system. This impact will occur throughout the life time of the project. The impact was rated as having an overall significance of **MODERATE** and cannot be mitigated to a lower significance as set out in the Table 9-1 below.

Table 9-1: Summary of Environmental Significance Ratings of impacts on surface water during Construction

Construction Phase														
	Ratir	ng Be	fore	Mitiga	tion N	leasu	ires	Rating After Mitigation Measures						
Risk	S	R	D	Е	С	Р	Significance =C*P	S	R	D	Е	С	Р	Significance =C*P
Increase in turbidity of surface water during construction caused by an increase in runoff from the cleared and stripped areas or from topsoil stockpiles which is high in suspended solids (Aluminium and Iron).	4	3	4	3	14	4	56 - Moderate	3	3	4	2	12	3	36 - Moderate
Accidental spillages of hazardous substances from construction vehicles used during the site clearing and grubbing.	4	3	3	2	12	3	36 - Moderate	3	3	2	1	9	2	18 – Low
Reduction of catchment yield as a result of the footprint areas of the dirty water dams and the Ash Dump Disposal Facility and	3	3	4	3	13	5	65 - High	3	3	4	3	13	5	65 - High

Construction Phase	ruction Phase Rating Before Mitigation Measures Rating After Mitigation Measures													
	Ratir	ng Be	fore	Mitiga	tion M	leasu	res	Rat	ing A	fter M	itigatio	on Me	asure	S
Risk	S	R	D	Е	С	Р	Significance =C*P	S	R	D	Е	С	Р	Significance =C*P
associated infrastructure. The footprint areas will no longer form part of the natural downstream catchment thereby potentially resulting in a decrease of runoff downstream														
Increase of surface runoff and potentially contaminated water that needs to be maintained in the areas where site clearing and grubbing occur.	4	3	4	3	14	4	56 - Moderate	3	3	4	2	12	3	36 - Moderate
Excess storage of rainfall within the dirty water dams and settling tanks during the construction phase.	2	3	2	1	8	2	16 - Low	1	3	1	1	6	2	12 - Low
Separation of clean water runoff upstream of the dirty water dams and settling tanks. Water upstream of the dirty water dams and settling tanks is considered clean and will have to be separated from the dirty water area. Dirty water Spillages from the dirty water dams and settling tanks into the environment must be managed.	4	3	4	3	14	4	56 - Moderate	3	3	4	2	12	3	36 - Moderate

9.2 Operation Phase

9.2.1 Measures implemented to manage surface water

During normal operations of the Ash Dump and associated infrastructure the affected water will be contained in the ADDD. Clean stormwater will be diverted away from the Ash Dump and associated infrastructural operational areas by cut-off channels and diversion berms designed to handle the 1:50 year storm event.

Contaminated runoff water, generated during rainstorm events, on the operational footprint area will be contained in specifically designed structures to enable sedimentation and desilting of the runoff. The quality of the return water will be monitored on a regular basis and re-cycled as process water make-up.

Water containment facilities (SDD ST, SDD, and ADDD) will be designed, constructed, operated and maintained to have a minimum freeboard of 0.8 metres above full supply level and all other water systems related thereto shall be operated in such a manner that it is at all times capable of handling the 1:50 year flood-event on top of its mean operating level.

The Ash Dump Disposal Facility will be engineered to be fully compliant with Regulation 704 in terms of clean and dirty water segregation.

Groundwater and surface water quality, and quantity, monitoring systems have already been established for Ash Dump Disposal Facility.

The SDD ST will consist of two equal capacity concrete basins that clarify contaminated water from the power station terrace before it travels by gravity pipeline to the SDD. The two compartments will allow for occasional maintenance and inspection access (preferably during the dry season) without interrupting the functionality of the SDD ST under normal circumstances there by mitigating the risk of silt build-up. This will have a mitigated significance of **LOW** as depicted in Table below.

9.2.2 Surface water quality

Surface water quality may be impacted upon during the operational phase by the Ash Dump activities and associated infrastructure, if not adequately mitigated and managed. The probability that the impact will manifest in an impact with a moderate potential intensity, meaning a reduction in the functionality of the surface water which makes it unfit for use by any other water user, is possible but unlikely, because the Ash Dump has been designed according to the principles indicated above. The activity and therefore the impact will occur during the life of the project but will be contained to site. Therefore, impacts associated with spillages on surface water quality were rated as having a **LOW** significance once mitigated as depicted in the summary Table 9-2 below.

The risk of sedimentation and increase in turbidity due to soil erosion and runoff from Ash Dump and cleared areas will continue from the construction phase and therefore has been addressed in the construction phase.

Spillages generated from Ash Dump and the dirty water systems as well as the runoff from these systems can have an impact on the surface water. The potential impact will occur for the duration while the Ash Dump is in development and subsequently when the Ash Dump is decommissioned and closed. The primary impact will be contained on site and will have a moderate intensity potential should the impact manifest with a probability of being moderate likelihood. Therefore the risk was rated as **MODERATE** if unmitigated but **LOW** once mitigated as depicted in Table 9-2 below.

The impact of pollution due to spillages of hazardous substances or leaks from vehicles and equipment during incidents or maintenance is carried over from the construction phase and therefore has been addressed in the construction phase.

9.2.3 Stormwater management

Should the Kusile Power Station footprint receive significant rainfall over a period of time, there is the potential for the stormwater systems and the clean and dirty water segregation system to be inundated with excess volumes of water. Should the maintenance of the stormwater systems be in place, the mitigated effect of increased volumes of contaminated water having to be handled by the Kusile Power Station footprint would be rated as LOW as depicted in the table below. Sufficient maintenance of

upstream clean water controls will also reduce the risk of non-compliance in terms of dirty and clean water separation and will have a significance rating of LOW once mitigated

Table 9-2: Summary of Environmental Significance Ratings of impacts on surface water during Operation

Operation Phase	Operation Phase													
	Ra	ting B	efore	e Mitig	ation	Meas	sures	Rating After Mitigation Measures						
Risk	S	R	D	Е	С	Р	Significance =C*P	S	R	D	Е	С	Р	Significance =C*P
Spillages from the dirty dams and wastewater treatment plant.	4	3	4	3	14	3	42 - Moderate	3	3	2	1	9	2	18 - Low
Inadequate removal of silt will result in a steady decrease in the storage capacity of the SDD ST.	2	3	1	2	8	3	24 - Low	1	3	1	1	6	2	12 – Low
Maintenance of upstream clean water controls.	4	3	2	2	11	3	33 - Moderate	2	3	2	1	8	2	16 - Low
Increase in volume of contaminated water that needs to be managed on the Kusile Power Station footprint.	4	3	4	3	14	3	42 - Moderate	3	3	2	1	9	2	18 - Low

9.3 Closure and decommissioning phase

During the closure and decommissioning phase of the Ash Dump and associated infrastructure, all additional infrastructures will be removed and the footprint area rehabilitated as with the Ash Dump being revegetated to manage on-going dust generation and erosion.

The surface water quality could possibly be further impacted by the closure and decommissioning activities due to spillages of hazardous substances (e.g. hydrocarbons and oils) from earthmoving equipment and sedimentation and increase in turbidity due to the disturbance of soils.

Seepage of water from the Ash Dump could occur although once mitigated the risk will have a significance of LOW as depicted in Table 9-3 below.

Table 9-3: Summary of Environmental Significance Ratings of impacts on surface water during Closure

Decommissioning an	Decommissioning and Closure Phase													
	Rat	ting B	efore	Mitig	ation	Meas	sures	Rating After Mitigation Measures						
Risk	S	R	D	Е	С	Р	Significance =C*P	S	R	D	Е	С	Р	Significanc e =C*P
Seepage of water out of the Ash Dump into the environment.	4	3	4	3	14	3	42 - Moderate	3	3	2	1	9	2	18 - Low
Accidental spillages of hazardous	4	3 3 2 12 3 36 - Moderate						3	3	2	1	9	2	18 – Low

Decommissioning and Closure Phase														
	Ra	Rating Before Mitigation Measures				Rating After Mitigation Measures								
Risk	S	R	D	Е	С	Р	Significance =C*P	S	R	D	Е	С	Р	Significanc e =C*P
substances from decommissioning vehicles used during the closure phase of the power station.														

10 Conclusion

The following can be concluded from the study:

Many of the water related environmental impacts are considered as moderate significance, in the absence of appropriate mitigation measures. There is the risk of spillage of ash and gypsum into the surface water system both from the Ash Dump itself and from the dirty water dams and wastewater treatment plant. Once mitigated though, these risks are significantly reduced.

Of concern is the increase in turbidity and suspended solids in the surface water monitoring. The mitigation measures will need to be implemented immediately during the current construction phase and managed during operation to maintain acceptable water quality levels.

Although the identified construction and operational risks associated with Ash Dump and its associated infrastructure may be considered to be significant on an individual basis, because the Ash Dump will be subject to specific legislative specifications, these impacts can be mitigated and managed.

Expected Mitigation and Management Measures to protect surface water resources:

- The Ash Dump system is to be operated to ensure that the accumulation of water in the dirty dams and wastewater treatment plant does not present a stability risk and that drainage of dirty dams accommodates the 1:50 year flood event;
- All dirty dams are to be operated to ensure that the 1:50 year flood event is contained plus free-board at full operating level of 0.8 m
- The Ash dump and associated infrastructure will be provided with formal engineered drainage and seepage collection systems appropriate to the collection of impacted waters for reuse purposes;
- The Ash Dump system will be compliant to Regulation 704 in diverting clean water from the upper catchment area around the site to the natural environment, and containing dirty water within the Ash Dump water management system;
- A monitoring program for structural maintenance of the dirty dams and wastewater treatment plant needs to developed and an maintenance on leakages or spills should be carried out immediately;
- A stormwater management maintenance program needs to be maintained regularly to ensure that the stormwater system is functioning sufficiently;
- A monitoring program of ground and surface water needs to be implemented and maintenance on any seepage needs to be carried out immediately if detected.

It is expected that consideration will also be given to the on-going updates to the National Waste Management Strategy including the Waste Classification Regulations, Waste Information System

Regulations and National Norms and Standard and Standard for the Disposal of Waste to Solid waste management services.

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All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

11 References

- Department of Water Affairs and Forestry. (1996). South African Water Quality Guidelines (Second Edition)

 Volume 1 Domestic Water Use. Pretoria: Department of Water Affairs and Forestry.
- Department of Water Affairs and Forestry. (2000). Guideline document for the implementation of regulations on use of water for mining and related activities aimed at the protection of water resources. Pretoria.
- Department of Water Affairs and Forestry. (2006). *Best Practice Guideline G1 Storm Water Management*. Pretotria.
- Department of Water Affairs and Forestry. (2007). *BPG A4:Guideline for Pollution Control Dams*. Pretoria. Department of Water Affairs and Forestry. (2008). *BPG A5: Guideline forWater Management for Surface Mines*. Pretoria.
- Ecosun. (Report E 457/06/B). Ecological Assessment Wetlands and Surface Water associated with the proposed Coal Fired Power Station in the Witbank Area.
- Knight Piesolt. (2013). Wetlands Method Statement Kusile Power Station_ Combustion Waste Terrace.
- Panel B Consortium joint Venture PBC JV#19. (2008). *Emergency Ash Dump Layer Works Design, Prelimanary Design Report 5452-40-005 Rev O.* ESKOM.
- Panel B Consortium_ PBCJV TO#31. (2010). Ash Dump Terrace Layer Works Design, Detail Design Report 5452-90-011 Rev 5. ESKOM.
- Panel B Consultants joint Venture PBC JV-TO #31. (2010). *Kusile power Station Station Dirty Dams Design Report 5452/80/008 REV2.*
- Panel B Consultants joint Venture WMS 5452/110/014 (Rev 1). (2010). *Construction of the Ash Dump Embankment Culvert*. ESKOM.
- Zitholele Consulting. (2013). Surface and Groundwater monitoring for Kusile power Station. ESKOM.

Appendices

Appendix A: Floodline Study Report

Kusile Power Plant 1:50 & 1:100 Year Floodlines

Report Prepared for

ILISO Consulting

Report Number 467775/1



Report Prepared by



June 2014

Kusile Power Plant

1:50 & 1:100 Year Floodlines

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Executive Summary

The purpose of this study was to carry out the 1:50 and 1:100 year floodline study for the Klipfonteinspruit and its tributary situated south of the CDF (Current Design Facility) where it approaches and crosses the new D686 tarred road. During the EMP development phase, floodline determination along the remainder of the tributary was not considered necessary as the floodline were estimated to be in excess of 100m downhill from the nearest infrastructure related to the CDF. DWA has however requested the determination of the 1:100 year floodlines around the CDF and this are required for the impact assessment phase of the project. In view of this, Iliso Consulting appointed SRK to conduct a 1:50 and 1:100 year floodline study for the remainder of the Klipfonteinspruit tributary south of the CDF.

The report covers the 1:50 and 1:100-year floodlines for the Klipfonteinspruit and its tributaries.

Summary of principal objectives

The principal objective of this project is to conduct the 1:50 and 1:100 year floodline in order to assess if the any part of the Kusile Power Station infrastructure is not situated within the 1:50 and 1:100 year floodlines.

Outline of work programme

The floodlines were determined based on the existing watercourse condition, future land-use flood peaks and survey available at the time of study. The data that was used consisted of the Surveyor 0.5m contours supplied by the client and the 24 hour rainfall.

Recommendations

- Development layout planning to take into account the position of the 100-year floodline.
- The positioned of the CDF and its infrastructure to be outside of the 1:100 year floodplain as shown on Drawing 467775/001.

Action Points

- No new development to encroach onto the 1:50-year floodplain
- All future floor levels to be above the 1:100-year flood level.
- The floodlines be revised should watercourse and/or control structures be modified in the future.

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Disclaimer

The opinions expressed in this Report have been based on the survey data information supplied to SRK Consulting (South Africa) (Pty) Ltd (SRK) by ILISO Consulting (ILISO). The opinions in this Report are provided in response to a specific request from ILISO to do so. SRK has exercised all due care in reviewing the supplied information. Whilst SRK has compared key supplied data with expected values, the accuracy of the results and conclusions from the review are entirely reliant on the accuracy and completeness of the supplied data. SRK does not accept responsibility for any errors or omissions in the supplied information and does not accept any consequential liability arising from commercial decisions or actions resulting from them. Opinions presented in this report apply to the site conditions and features as they existed at the time of SRK's investigations, and those reasonably foreseeable. These opinions do not necessarily apply to conditions and features that may arise after the date of this Report, about which SRK had no prior knowledge nor had the opportunity to evaluate.

1 Introduction and Scope of Report

Kusile Coal-Fired Power Station is currently under construction and has an anticipated output 4 800 MW, covers approximately 2 500 ha of land on the Farm Hartebeesfontein 537 JR and the Farm Klipfontein 566 JR in the Witbank area. Floodlines form part of the surface water impacts that are normally required for the EIA/EMP for the construction, operational, decommissioning and post closure phases. Floodlines were previously (Kusile Stream Diversion & Dewatering EMP by Panel B Consultants Joint Venture)determined for the tributary of Klipfonteinspruit that was running through the Coal Stork Yard area prior to being diverted to a channel that runs against the Plant Boundary. ILISO Consulting saw the need to conduct floodline study for the tributary of Klipfonteinspruit that was diverted on the upstream and Klipfonteinspruit running on the southern side of the power plant activities. Floodlines are determined as part of Regulation 704 to ensure that all developments situated closer to the rivers are not at risk of being flooded during a 1:50 year and 1:100 year flood events.

Brief details are given below.

2 Background and Brief

2.1 Background of the project

Kusile power station is in construction and floodlines are required to ensure that the power station infrastructure and new developments are not situated within the 1:50 year and 1:100 year floodlines. In view of this, SRK Consulting (SRK) was appointed by Iliso Consulting to carry out a floodline study on the above site. Regulation 704 of the national water Act, 2008 requires that any development associated with the power station must not be placed within the 1:100 year floodline.

Nature of the brief

The aim of this study is to conduct the 1:50 and 1:100 year floodline study for two of the streams running in close proximity of power station activities (Klipfonteinspruit running on the southern side of the power station activities and the channelized tributary running on the eastern side of the Coal Stockyard until it confluences with Klipfonteinspruit on the western side at \pm 4km downstream of the Coal Stockyard). Additional floodlines were determined for additional tributaries of Klipfonteinspruit and the floodlines are indicated on Drawing 467775/001 forming part of this report. Relevant details are given in this report.

3 Program Objectives and Work Program

3.1 Program objectives

The project objectives are as follows:

- Data Collection;
- Data Verification;
- Model Setup;
- Flood Hydrology Calculations;
- Hydraulic Modelling to obtain 1:50 year and 1:100 year floodlines;
- Summary Reports and maps showing Floodlines; and
- Reviewing of the Report and Floodlines.

3.2 Purpose of the Report

This report provides with the findings of the floodline study and gives recommendations to Iliso Consulting for current and future power station developments.

4 Description of Study Area and Watercourses

The Kusile Power Plant river catchments all drain into the Wilge River. The Klipfonteinspruit and its tributaries have a total catchment area of 60.4 km². The diverted stream including the non-diverted part of the stream on the downstream has a total catchment area 12.8 km². The area covered by the catchments is mostly rural and undeveloped covered largely by grass and very few trees. The study area is shown in Figure 4-1 below.

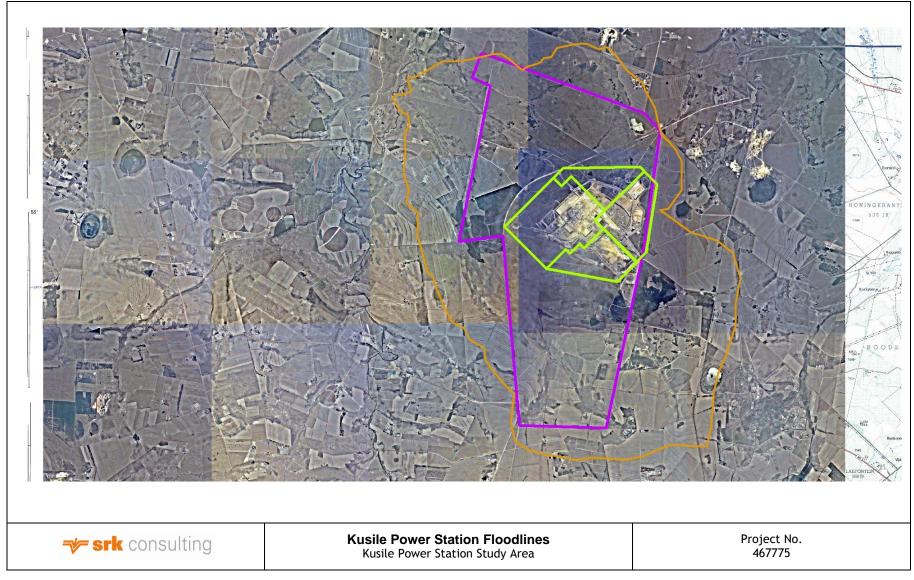


Figure 4-1: Kusile Power Station Study Area

The main watercourse (Klipfonteinspruit) is a well-defined channel that consists of a few road crossings while the tributaries are shallow and overgrown with grass. There is currently no development on both the river banks as the power station is still in construction. The river segment lengths are in Table 4-1 below.

Table 4-1: River Segment Length

Rivers situated within the Kusile Boundary							
River Name Segment Length (km) Cumulative Length							
Klipfonteinspruit	_						
Tributary	KLFS2T2	3.9	3.				
Klipfonteinspruit							
Tributary	KLFS2T1	2.5	6.4				
Klipfonteinspruit	KLFS3	3.3	6.8				
Klipfonteinspruit	KLFS2	4.0	10.8				

5 Topographical Details

The general topography was determined using 0.5m contours. From these 0.5m contours, the cross sectional profile and the profile of the road crossings were determined.

6 HECRAS Model Compilation

The 0.5m contour was entered into the HECRAS (Version 4.0) model. All "natural cross sections" were abstracted from the DEM (digital elevation model). The HECRAS model main parameters are summarised in Table 6-1 below.

Table 6-1: HECRAS Model Main Parameters

Parameter	Average Value/Selection	Reason
Manning 'n'	0.035 (main flow channel)	Defined channel with vegetation
	0.0300 (floodplains)	Moderate vegetation (mainly grass) and thick vegetation and developments
Boundary conditions	Normal flow depth	Control structures present
Flow regime	Mixed flow	Slope and cross section changes requiring super and sub-critical flow regimes

The HECRAS model cross-sections were named in accordance with the defined River Referencing System (RRS). Further details of the HECRAS model parameter files are given in Appendix A.

7 Flood Hydrology

In order to obtain realistic and integrated flood peak data for the Kusile study area, the catchment area draining into the tributary of Klipfonteinspruit (KLFS2T) was sub divided into the upstream subcatchments contributing to the diverted channels and downstream sub-catchment that drains into the natural stream. The Rational and Alternative Rational methods built into the Utility Programs for Drainage Software (UPD) were then compiled for the main Klipfonteinspruit. The Peak Flows for the subdivided catchments were determined using Visual SCS as the program was designed to model smaller catchments accurately <30 km². The catchments commanded by the study area are given in Table 7-3. Based on the hydrological parameters used in the hydrological methods for the Kusile study area, peak flow rates for the catchment conditions are give in Table 7-1 below.

Table 7-1: Summary of Flood Peaks (Future Development Condition)

River Segment & Chainage	Peak Flow Rates (m³/s)			
	1:50	1:100		
KLFS2	359	427		
KLFS3	326	387		
KLFS2T1	101	131		
KLFS2T2a	27	35		
KLFS2T2b	31	41		
KLFS2T2c	41	53		
KLFS2T2d	44	58		

7.1 Rainfall Data

Rainfall for the model was based on IDF (intensity-duration-frequency) curves derived for this study area by J C Smithers and R E Schulze. The Rainfall station 0514537 which is the closest to the study area with reliable and most recent data was used. The estimated design rainfall depths for durations ranging from 15 minutes to 7 days and for return periods ranging from 2 to 200 years for the Kusile study area were calculated. The calculated 1 day rainfall depths for selected return period are as shown in Table 7-2 below.

Table 7-2: 1-day Rainfall Depths

Return Period	1:2 Year	1:5 Year	1:10 Year	1:20 Year	1:50 Year	1:100 Year
Rainfall depth (mm)	59	81.4	98.5	116.5	142.9	165

7.2 Catchment Data

The catchment of the watercourse consists mainly of grass and very few trees. The catchment areas commanded by the river segments are summarised Table 7-3 below.

Table 7-3: Summary of Catchment Area

River Segment	Catchment Area (km²)
KLFS2	49.5
KLFS3	34.9
KLFS2T1	12.8
KLFS2T2a	3.4
KLFS2T2b	4.0
KLFS2T2c	6.0
KLFS2T2d	6.9

The catchments of the study area are as shown in Figure 7-1 below.

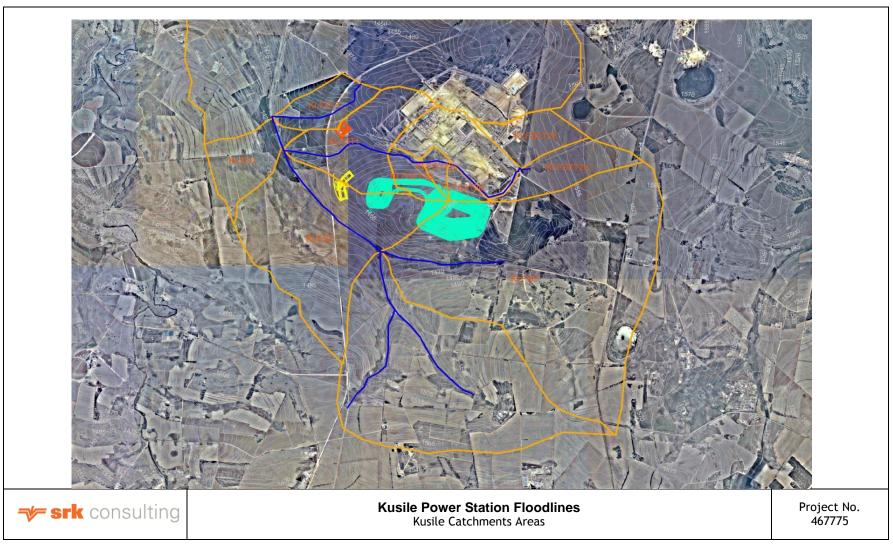


Figure 7-1: Kusile Catchments Areas

8 Floodline Determination and Results

The 1:50 and 1:100-year floodlines were determined based on the HECRAS model and peak flow rates as given in Table 7-1 above for existing watercourse conditions.

Details and certified floodlines are shown on drawing 467775/001 in Appendix B.

The HECRAS model output data is given in Appendix A.

From the floodline study, the following was observed:

- The existing development and infrastructure is not affected by the 1:50 year and 1:100 year floodlines.
- The diverted channel running on the south eastern and south western sides of the coal stock yard can handle the 1:50 year and 1:100 year flood events.
- The 1:50 and the 1:100 year average flood depths and average flood velocities along the floodplains are shown below in Table 8-1 and Table 8-2, respectively.

Table 8-1: Summary of Average flood depths along floodplains

	Average Flood depths (m)						
Chainage	1:5	0 Year	1:100 Year				
Onamage	Hydr depth L	Hydr depth R	Hydr depth L	Hydr depth R			
KLFS2	0.75	0.76	0.82	0.83			
KLFS3	0.35	0.40	0.39	0.44			
KLFS2T1	0.27	0.27	0.33	0.33			
KLFS2T2a	0.97	0.97	1.10	1.10			
KLFS2T2b	1.04	1.04	1.19	1.19			
KLFS2T2c	1.26	1.26	1.42	1.42			
KLFS2T2d	1.30	1.30	1.48	1.48			

Table 8-2: Summary of Average flood velocity along floodplains

	Average Flood velocity (m ³ /s)						
Chainage	1:5	0 Year	1:100 Year				
	Vel Left	Vel Right	Vel Left	Vel Right			
KLFS2	1.95	2.01	2.08	2.14			
KLFS3	1.53	1.63	1.66	1.83			
KLFS2T1	1.14	1.15	1.28	1.27			
KLFS2T2a	4.69	4.69	5.03	5.03			
KLFS2T2b	4.87	4.87	5.24	5.24			
KLFS2T2c	4.83	4.83	5.16	5.16			
KLFS2T2d	4.92	4.92	5.28	5.28			

9 Legal and Council Requirements

The **1:100-year** floodline is required in terms of the National Water Act, Act 36 of 1998, Chapter 14 Part 3 as given below.

144. For the purposes of ensuring that all persons who might be affected have access to information regarding potential flood hazards, no person may establish a township unless the layout plan shows, in a form acceptable to the local authority concerned, lines indicating the maximum level likely to be reached by flood waters on average once in every 100 years.

10 Conclusions

The following is concluded:

- The existing development and infrastructure at Kusile Power Station is situated outside the 1:50 and 1:100 year floodlines.
- The diverted channel can handle the 1:50 year and 1:100 year flood events.

11 Recommendations

The following is recommended:

- The floodline data to be used for layout planning and township applications.
- No new development to encroach onto the 1:50-year floodplain
- All future floor levels to be above the 1:100-year flood level.
- The floodlines be revised should watercourse and/or control structures be modified in the future.

Pre	pare	d by

J. Mathole

Reviewed by

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SPIK CONSUMING

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D. Mahlangu, Director

All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

Appendices

Appendix A: Hecras Output Model

		17 77	0.41		2.031				1518.49	1518.28	1518.28	15/1.61	35.⊥	JANUTIVERC	202/	VC0C17L7
0	38.71		0.37		1.9				1518.38	1518.2		1521.61	26.8	5857 50yr	5857	KLF2T5857
0	37.13	16.63	0.45		2.11			0.012039	1521.6	1521.37	1521.37	1523	35.1	5895 100yr	5895	KLF2T5895
0			0.39		1.97			0.012761	1521.49	1521.29	1521.29	1523	26.8	5895 50yr	5895	KLF2T5895
0	61.7	13.61	0.22		2.58			0.045391	1524.87	1524.64	1524.53	1524.72	35.1	5940 100yr	5940	KLF2T5940
0			0.24		2.54			0.038931	1524.8	1524.58	1524.47	1524.72	26.8	5940 50yr	5940	KLF2T5940
1.21			0.16	0.07	1.9	0.79	1.23	0.036656	1526.58	1526.46	1526.4	1526.36	35.1	5978 100yr	59/8	KLF2159/8
1.05	127.05	14.86	0.13	0.06	1.84	0.35	1.19	0.043909	1526.54	1526.42	L	1526.36	26.8	5978 50yr	5978	KLF2T5978
0		23.58	0.18		1.49			0.020467	1527.45	1527.35	1527.34	1527.37	35.1	6013 100yr	6013	KLF2T6013
0	133.47		0.16		1.28			0.017725	1527.4	1527.32	1527.32	1527.37	26.8	50yr	6013	KLF2T6013
0	60.75		0.24		2.45			0.037668	1528.26	1528.07	1527.95	1528.18	35.1	6043 100yr	6043	KLF2T6043
0	56.4	11.52	0.2		2.33			0.040849	1528.18	1528	1527.9	1528.18	26.8	6043 50yr	6043	KLF2T6043
1.50			0.1.0	0.00	1	1.00	0.0	0.0	2010							
15		19 45	0 13	0.03	1.82	1.68	0.64	0.043728	1528.9	1528.78	1528.73	1528.57	35.1	6056 100vr	6056	KLF2T6056
1.51	148.3		0.11	0.02	1.64	1.49	0.49	0.04359	1528.85	1528.75	1528.71	1528.57	26.8	50yr	6056	KLF2T6056
1.32	133.45		0.16	0.08	1.83	1.31	1.13	0.03341	1529.64	1529.53	1529.48	1529.36	35.1	6072 100yr	6072	KLF2T6072
1.26	131.16	16.82	0.14	0.06	1.66	1.09	0.95	I_	1529.59	1529.5	1529.46	1529.36	26.8	6072 50yr	6072	KLF2T6072
0.77		24.7	0.06	0.31	0.61	0.65	1.73	0.012562	1530.59	1530.5		1530.34	35.1	6111 100yr	6111	KLF2T6111
0.67	131.37		0.04	0.28	0.46	0.39	1.62	0.012349	1530.55	1530.45	1530.42	1530.34	26.8	50yr	6111	KLF2T6111
1.1	80.75	20.19	0.1	0.21	0.89	2.07	1.43		1531.45	1531.3		1530.81	35.1	6208 100yr	6208	KLF2T6208
1.09			0.08	0.17	0.75	1.91	1.27	0.015287	1531.38	1531.25	1531.23	1530.81	26.8	6208 50yr	6208	KLF2T6208
1.28		17.18	0.15	0.17	1.28	2.59	1.43	0.019354	1531.83	1531.64	1531.57	1531.07	35.1	100yr	6229	KLF2T6229
1.19	64.01		0.12	0.16	1.07	2.29	1.27	0.017142	1531.74	1531.59		1531.07	26.8	50yr	6229	KLF2T6229
0.93		20.07	0.12	0.09	0.81	1.85	0.69		1532.23	1532.06		1531.5	35.1	6257 100yr	6257	KLF2T6257
1.01	54.65		0.09	0.06	0.74	1.8	0.56	0.01308	1532.14	1531.99	1531.98	1531.5	26.8	6257 50yr	6257	KLF2T6257
2.13	55.1/	00.11	0.04	0.04		2.23	0.30	201000.0	00.7CCT	1332.43	T336.33	70.7CCT	33.1	TOOM	020/	VEL 5 10507
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2 15	49.63	402	0.01	0.00		2 98	0.56	0.070732	1532.74	1532.42	1532.29	1532.02	26.8	6287 50vr	6287	KLF2T6287
1.31	77.89	17.47	0.09	0.18		2.49	1.56	0.020991	1534.34	1534.18	1534.09	1533.64	35.1	6330 100yr	6330	KLF2T6330
1.28			0.06	0.16	0.76	2.29		0.021009	1534.26	1534.11	1534.04	1533.64	26.8	6330 50yr	6330	KLF2T6330
	(m)	(m2)					Ш		(m)			(m)	(m3/s)			
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0		193/	0.34		21			0.017335	1497.02	1496.83	1496.79	1497.69	40.6	4629 TUUVI		KLF 214629
0	48.64	14.53	0.3		2.13			0.020937	1496.93	1496./6	Т	1497.69	31	4629 JOY		VEL 714072
										1000	100	107.00	2	50 50 50	-	CSVICSIN
0		15.26	0.32		2.66			0.029662	1498.21	1497.96	1497.85	1498.65	40.6	4681 100yr		KLF2T4681
0	45.11		0.3		2.26			1		1497.89	Г	1498.65	31	4681 50yr		KLF2T4681
															-	
0			0.29		2.27			1	1499.58	1499.4	1499.32	1499.71	40.6	4732 100yr		KLF2T4732
0	49.69	12.47	0.25		2.49			0.035655	1499.53	1499.32		1499.71	31	4732 50yr		KLF2T4732
1.14			0.15	0.1	2.01	0.78	1.23	0.031407		1501.06	1501.01	1500.9	40.6	4792 100yr		KLF2T4792
0.9	172.66	21.45	0.15	0.09	1.64	0.57	0.97	0.020767	1501.12	1501.04	1501	1500.9	31	4792 50yr		KLF2T4792
1	197.99	21.1	0.11	0.13		1.10				10001		100				
1.1			0.11	0.10	4	1 12				1502.2		1502.04	40.6	4840 100vr		KLF2T4840
1 16	172 94	21 79	0.09	0.16	1.06	1.1	1.57	0.026525	1502.25	1502.17	1502.14	1502.04	31	4840 50yr	+	KLF2T484
0	150.63	24.56		0.16			1.65	0.027621	1503.2	1503.09	1503.06	1503.12	40.6	4883 100yr	+	KLF214883
0	150.46	24.18		0.16				Т		1503.05	Т	1202.12	- L	4003 JUYI		NEI 214000
								\neg		1000	Т	1502.42	2	000 500	Ī	KI EDTAGG
0	113.85	25.04		0.22			1.62	0.017907	1504.26	1504.14	1504.12	1504.44	40.6	4931 100yr		KLF2T4931
0	86.36	14.64		0.17			2.12	0.043168		1504.09	Т	1504.44	31	4931 50yr	-	KLF214931
								Т			Т					
0		16.64		0.23			2.44			1505.14	1505.05	1505.7	40.6	4971 100yr		KLF2T4971
	74.81	19.31		0.26			1.61	0.014225	1505.22	1505.09	1505.09	1505.7	31	4971 50yr		KLF2T4971
		10.00		0				\neg			T					
		23 03		0 30				\neg	1505.86	1505.7	П	1506.51	40.6	4993 100vr		KLF2T4993
	68.4	18.56		0.27			1.67	0.014483	1505.78	1505.64	1505.64	1506.51	31	4993 50yr		KLF2T4993
0.39	157.55		0.16	0.22	1.2	0.03	1.47	0.015027	1508.26	1508.16	1508.16	1508.16	40.6	5036 100yr		KLF215036
		25.14	U.13	er.o	CO.T		Ī	Т		1300.13	Τ	1.00.10	100	1000	T	KL 1000
				0 10	105			\neg		1508 13		1508 16	4	5036 SOvr		KI F2T5036
0	74.1	36.9	0.5		0.95			0.001101	1508.4	1507.75	1508.35	1509.66	35.1	5082 100yr		KLF2T508
0	68.17	32.42	0.48		0.83			0.00082	1508.32	1507.63	1508.29	1509.66	26.8	5082 50yr	Н	KLF2T5082
0	30.28		0.51		2.25			0.011387	1508.95	1508.69	1508.69	1510.56	35.1	5115 100yr		KLF2T5115
0		12.85	0.44		2.09						I	1510.56	26.8	5115 50yr	-	KLF2T5115
			0.0		7.2.1			0.00208	T005.03	1,000,7		1011.10	U.	100y		N. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.
	17.00	20.00			1			Ι		П		1511 10	35.1	11/2 100wr		K) E2T51/13
			0.53		1.14			0.002817	1508.96	1508.67	1508.9	1511.19	26.8	5143 50yr		KLF2T5143
0	29.8	15.46	0.52		2.27			0.011494	1509.46	1509.2	1509.2	1511.96	35.1	5176 100yr		KLF2T5176
0			0.44		2.11			0.012153	1509.33	1509.11	1509.11	1511.96	26.8	5176 50yr		KLF2T5176
0	30.01	15.53	0.52		2.26			0.011812	1511.16	1510.9	1510.9	1512.76	35.1	5219 100yr	-	KLF2T5219
		(m2)		ш.			(m/s)	(m/m)	(m)	1 1	(m)					
Frouge # Cnl	I OD WIGIN	IFIOW Area	Hydr Depth K	Hydr Depth L	\u00e41	vei Chni	אפו רפונ	L.G. Slope	C.G. CIEV	CITE W.S.	AA.O. LICA	I CIT CI	ע וסומו	MACI OLD LIGHT	I Thinks	Node

200	45.75	0.22		7.64	Ť	1	0.007012	1476 85	1476 59	1476 40	1478 04	40.6	3991 50vr	3001	KI E3T3001
50.4	20.27	0.4		2		2	_	1478.25	14/8.05	14/8.05	14/9./4	40.6	ΤΟΟΥΓ	4053	KLF214053
46.53	15.45	0.35		1.00	İ	i d	0.012/30	I	Т	1477.57	1470.74	AD C	100	AOES	KI ESTANES
		2		1 00				Τ	Т	1/77 07	1,770 7,1	2	500	4053	KI FOTAOS3
48.7	20.04	0.41		2.03		ω.	7 0.012073	1479.77	1479.56	1479.56	1481.69	40.6	4112 100yr	4112	KLF2T4112
45.24	16.3	0.36		1.9		6	6 0.012706	1479.66		1479.48	1481.69	31	50yr	4112	KLF2T4112
50.56	20.31	0.4		2		4			П	1480.63	1482.78	40.6	4154 100yr	4154	KLF2T4154
43.99	16.21	0.37		1.91		òo	3 0.01248	1480.73	1480.54	1480.54	1482.78	31	4154 50yr	4154	KLF2T4154
36.17	27.11	0.31		3.0			1020000	7010+1	1401.00	1400.00	140.004	10.0	TOOA	1101	701
2021	11 20			3 6	Ì				Т		1/83 6/	306	4184 100vr	4184	KI F2T4184
34.15	9.17	0.27		3.38		6	8 0.059376	1481.38	1480.97	1480.8	1483.64	31	4184 50yr	4184	KLF2T4184
48.96	20.15	0.41		2.01		00	9 0.011938	1482.29	1482.08	1482.08	1484.61	40.6	4215 100yr	4215	KLF214215
42.94	16.09	0.37		1.93		00	$\overline{}$			1482	1484.61	31	4215 50yr	4215	KLF2T4215
							$\overline{}$								
37.91	18.43	0.49		2.2		6		1483.44	1483.2	1483.2	1485.61	40.6	100yr	4245	KLF2T4245
36.01	15.12	0.42		2.05		5	2 0.012315	1483.32	1483.11	1483.11	1485.61	31	50yr	4245	KLF2T4245
26.12	9.02	0.35		4.5		7				1484.64	1486.68	40.6	100yr	4277	KLF2T4277
23.73	7.11	0.3		4.36		2	3 0.088462	1485.53	1484.83	1484.56	1486.68	31	50yr	4277	KLF2T4277
63.6	21.86	0.34		1.86		ω			1486.67	1486.67	1488.18	40.6	4317 100yr	4317	KLF2T4317
53.36	17.21	0.32		1.8		8	5 0.013448	1486.75	\neg	1486.59	1488.18	31	4317 50yr	4317	KLF2T4317
79.98		0.29		1.73		4	6 0.013854	1488.76	1488.62	1488.61	1489.51	40.6	4360 100yr	4360	KLF2T4360
77.33	19.4	0.25		1.6		ω				1488.56	1489.51	31	4360 50yr	4360	(LF2T4360
22.73	8.36	0.37		4.85		3				1488.96	1490.78	40.6	4399 100yr	4399	KLF2T4399
21.27	6.57	0.31		4.72		8	1 0.098508	1490.01		1488.88	1490.78	31	4399 50yr	4399	KLF2T4399
7															
98.4	25.21	0.26		1.61		9			1491.44	1491.44	1492.29	40.6	4444 100yr	4444	KLF2T4444
86.74	20.28	0.23		1.53		1	1 0.014721	1491.51	1491.39	1491.39	1492.29	31	4444 50yr	4444	KLF2T4444
									П						
54.4	13.4	0.25		3.03		6	6 0.054086	1493.46		1492.99	1493.55	40.6	100yr	4487	KLF2T4487
43.67	10.68	0.24		2.9		2			1493.1	1492.94	1493.55	31	4487 50уг	4487	KLF2T4487
							- 1	Ī							
69.05	22.57	0.33		1.8		3			1494.44	1494.44	1495.24	40.6	4535 100yr	4535	KLF2T4535
59.46	17.78	0.3		1.74		7	2 0.013857	1494.52	1494.37	1494.37	1495.24	31	4535 50уг	4535	KLF2T4535
49.38	15.06	0.3		2.7		000	3 0.032418	1495.93	1495.67	1495.56	1496.43	40.6	4582 100yr	4582	KLF2T4582
22.30	17.23	0.55		T./2		· ·	Т	Ī	T	T455.0	C+:0C+T	TC	IVOC	70C#	VEL 7 1 4 7 0 7
500	17.00	23		, ,		5			П	11000	1406 45	2	70	AFOO	/I EDITATEON
(m)		_	(m)	(m/s)	(m/s)	(m/s)	(m/m)	(m)	(m)		(m)	(m3/s) (r			

44.45 43.26 43.26 47.18 48.54	24.32	0.5					т			1,00.01		10.0	100 took		in the same of the
44.45 43.26 47.18			_	1.67		7	0.006307	1466.06	1465.81	1465.91	1468.39	40.61	(KOVr	3334 50yr	KLF213334
44.45 43.26 47.18							-								
44.45	23.72	0.5		2.24			0.011287	1466.89	1466.63	1466.63	1468.95	53.1	3380 100yr	3380	KLF2T3380
44.45	19.23	0.44		2.11			Т		1466.53	1466.53	1468.95	40.6	50yr	3380 50yr	KLF2T3380
44.45															
14.04	23.24	0.52	Ē	2.29			0.011173		1467.4	1467.4	1469.58	53.1	100yr	3428	KLF2T3428
40 41	18.8	0.47	51	2.16			0.01165	1467.53	1467.29	1467.29	1469.58	40.6	50yr	3428	KLF2T3428
47.65	24.58	0.52	51	2.16		7	0.010187	1468.21	1467.95	1467.97	1470.32	53.1	100уг	3480	KLF2T3480
43.98	20.42	0.46	4	1.99			0.00993	1468.08	1467.85	1467.88	1470.32	40.6	50yr	3480 50yr	KLF2T3480
							- 1								
59.86	25.79	0.43	J.	2.06		1		1468.77	1468.56	1468.56	1470.58	53.1	3527 100yr	3527	KLF2T3527
48.54	19.92	0.41	-	2.04			0.012295		1468.45	1468.45	1470.58	40.6	50yr	3527 50yr	KLF2T3527
57.62	23.84	0.41	3	2.23		1	0.014479	1469.37	1469.15	1469.12	1471.14	53.1	3569 100yr	3569	KLF2T3569
54.01	19.86	0.37		2.04			0.014289	1469.26	1469.07	1469.05	1471.14	40.6	50yr	3569 50yr	KLF2T3569
65.42	26.36	0.4		2.01				1470.07	1469.87	1469.87	1471.76	53.1	3616 100yr	3616	KLF2T3616
62.59	21.77	0.35	5	1.86		1	0.012793		1469.8	1469.8	1471.76	40.6	50yr	3616	KLF2T3616
							\neg								
53.28	29.26	0.55		1.81					1470.16	1470.26	1472.51	53.1	100yr	3655	KLF2T3655
51.3	25.21	0.49		1.61		-	0.006025	1470.31	1470.07	1470.18	1472.51	40.6	50уг	3655	KLF2T3655
22.74	77.70	0.77		7			- 1	T		1					
57 74	24 58	0 47	21	216		-	- 1		1470.74	1470.74	1473.43	53.1	3702 100vr	3702	KLF2T3702
44.77	16.2	0.36		2.51			0.02196	1470.89	1470.65	1470.57	1473.43	40.6	50yr	3702 50yr	KLF2T3702
00:00	30.00	9					\neg	Ī							
60.06	25 37	0.42		2.09			П	ĺ	1471.54	1471.54	1474.46	53.1	3748 100vr	3748	KLF2T3748
56.88	21.14	0.37	.~	1.92			0.012437	1471.65	1471.46	1471.46	1474.46	40.6	50yr	3748	KLF2T3748
10.01	10:02	0.75		100			\neg				,	001	1001		
50.01	25.61	0.43		207			\neg	Ī	1472 1	1472 1	1475 01	53.1	3794 100vr	3794	KI F2T3794
58.18	21.53	0.37		1.89			0.012056	1472.21	1472.02	1472.03	1475.01	40.6	50yr	3794 50yr	KLF2T3794
56.82	25.25	0.44		2.1		Ĭ	0.011749	1473.1	1472.88	1472.88	1475.85	53.1	3837 100yr	3837	KLF2T3837
53.28	20.62	0.39	7	1.97			0.01238	1472.99	1472.79	1472.79	1475.85	40.6	50yr	3837 50yr	KLF2T3837
	-						\neg								
60 26	25, 72	0.43	.1	2.06			. 1		1474.01	1474.01	1476.41	53.1	3884 100vr	3884	KLF2T3884
54.62	20.81	0.38	U 1	1.95			0.01241	1474.12	1473.92	1473.92	1476.41	40.6	50yr	3884 50yr	KLF2T3884
55.23	25.04	0.45	2	2.12		91	0.011636	1475.72	1475.49	1475.49	1476.99	53.1	3939 100yr	3939	KLF2T3939
50.39	20.23	0.4		2.01			\Box	П	1475.4	1475.4	1476.99	40.6	3939 50yr	3939	KLF2T3939
49.95	18.4/	0.37		2.87		4	0.028029	14/0.98	14/0.08	14/0.50	14/8.04)3.1	IAOOT TEEC	7227	VEL 2 1 3 3 3 1
	(m2) (m)	_	(m)	(m/s)	(m/s)	(m/s)	-	Œ)	(m)	_	_		3	300	NI TOPPOS
Vidth Froude # Chl	Flow Area Top Width	Hydr Depth R F	Hydr Depth L	Vel Right	Vel Chnl	Vel Left	E.G. Slope	E.G. Elev	Crit W.S.	W.S. Elev	Min Ch El	Q Total	Profile	River Sta Profile	Node

Node	River Sta Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	Heckas Output Table	ୢୗ୕୕	Vel Chnl	Vel Right	Hydr Denth I	Hydr Denth R	Flow Area	Top Width	Froude # Chl
		(m3/s)	(m)	1 1			(m/m)	Ш	\perp	Ш	(m)	(m)	(m2)		
KLF2T3286	3286 50yr	44.3				1465.83				1.31		0.55	33.94		
KLF2T3286	3286 100yr	57.9	1467.91	1465.83	1465.62	1465.94	0.003766			1.46		0.6		66	0
KI FOTT3046	3246 FOVE	AA 3		1465 68		1465 72	0 001654			0 00		0 50			
KLF2T3246	3246 100yr	57.9	1467.5			1465.82				1.04		0.63	55.58	88.75	
				П											
KLF2T3200	3200 50yr	44.3	1467.17	1465.61		1465.65	0.001392			0.83		0.55	53.24	97.27	0
KLF2T3200	3200 100yr	57.9	1467.17	1465.7		1465.74	0.001549			0.95		0.61		100.04	0
KLF2T3147	3147 50yr	44.3	1467	1465.54		1465.58	0.001555			0.82		0.5			0
KLF2T3147	3147 100yr	57.9				1465.66				0.94		0.56	61.77	110.65	
2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7															
KLF2T3098	3098 100vr	57.9	1466.51	1465.53		1465.58	0.002245			0.98		0.49	5935	122 22	
KLF2T3063	3063 50yr	44.3	1465.91	1465.24		1465.35	0.014306			1.49		0.23	29.66	129.39	0
KLF2T3063	3063 100yr	57.9				1465.42				1.64		0.27			
KI EDT3006	2026 500	440			146401	116157	0 00000		3 00						
KI F2T3026	3026 100vr	57.0	1/63	1/63 01	1/6/15	1/6/67	0.033202		2 07				11.40	25.57	
				П			0.01.0		ı,				T4:50		10.1
KLF2T2974	2974 50yr	44.3	1461.47	П	1462.11	1462.53	0.042682	1.34	3.45		0.09		13.05		1.85
KLF2T2974	2974 100yr	57.9	1461.47	1461.97	1462.21	1462.77	0.050566	1.7	3.99		0.11		14.82	41.62	
KLF2T2933	2933 50vr	443	1460 5	\neg	- 1	1461 84	0 0073	1 //8	3 67	1 27	0.30				
KLF2T2933	2933 100yr	57.9		1461.66	1461.68	1461.99		1.65	2.91	1.55	0.43	0.39	25.44	42.68	0.00
				П	ш										
KLF2T2890	2890 50yr	44.3			1460.98	1461.34	0.01868	1.37	3.2	1.02	0.17	0.11	14.7		1.33
KLF2T2890	2890 100yr	57.9	1460	1460.94	1461.11	1461.5	0.016894	1.58	3.41	1.28	0.22			36.85	
KLF2T2841	2841 50yr	44.3		1460.26	1460.29	1460.57	0.011529	0.76	2.46	0.93	0.1	0.13		39 17	1 04
KLF2T2841	2841 100yr	57.9	1459.5	i i	П	1460.73	1	1	2.83	1.15	0.13		21.47		
	3100														
KL 212700	2790 100	57.5		Т	Т	1459.98	81/110.0	1.01	2.48	1.11	0.15	0.17	18.88	41.02	
VEL 21 2790	2/90 TOOAL	5/.9	1459	1459.79	1459.83	1460.12	0.010451	1.18	2.64	1.28	0.2				
KLF2T2737	2737 50yr	44.3	1458.5	1459.06	1459.08	1459.31	0.012875	0.34	2.28	1.15	0.03	0.17		47.89	1.06
KLF2T2737	2737 100yr	57.9		Г	1459.18	1459.46	0.01522	0.58	2.66	1.42	0.05		22.54		
KLF2T2686	2686 50vr	44.3	1457.5	1458.12	1458 22	1458 51	0.019472	0.73	2 76	0 73	0.06				
KLF2T2686	2686 100yr	57.9		П	1458.33	1458.65	0.016463	1	2.9	1	0.11	0.11	20.55	43.3	1.24
לכארדרה לי	7677														
KLF212637	263/ 50yr	44.3	1457.12	1457.8	1457.8	1458.04	1458.04 0.009038	1.2	2.26	115	25.0	0 22	21 58	77 15	000

0.94	92.82	42.6	0.2	0.28	1.11		1.38	1 0.009216	1450.14	1449.9	1449.9	1449.17	87.6	2042 100yr	204	KLF212042
0.94	86.49	34.69	0.16	0.23	0.97	2.11	1.26	0.009885	1450.02	1449.81	1449.81	1449.17	67.4	2042 50yr	204	KLF2T2042
1.24	77.63		0.18	0.23	1.36		3 1.61	0.016483	1450.62	1450.33	1450.22	1449.52	87.6	2083 100yr	208	LF2T2083
1.26	72.28	26.81	0.14	0.18	1.19		3 1.41	0.017818	1450.5	1450.23	1450.14	1449.52	67.4	2083 50yr	208	KLF2T2083
0.98		39.39	0.24	0.25	1.28	2.53		0.009686		1450.94		1450.08	87.6	2128 100yr	212	KLF2T2128
0.93	78.19	33.29	0.2	0.2	1.08		1.1		1451.07	1450.84	1450.83	1450.08	67.4	8 50yr	2128	KLF2T2128
	00.10	.00														
1 27	58.46	29.48	0.11	0.06	1.01		Ì		1451.83	1451.48		1450.5	87.6	2174 100yr	217	KLF2T2174
1.22	54.4	25.1	0.07	0.02	0.76	2.71	0.35	0.016653	1451.66	1451.37	1451.29	1450.5	67.4	2174 50yr	217	KLF2T2174
1.04	65.78	35,49	0.1	21.0	0./0		0.00	0.01127	1432.43	7402.10		1701.00	0,.0	TOOA.	-	71.664
1.07		28.8	0.05	0.06	0.52	2.36		L	1	1452.09	1452.00	1451.35	07.4	2221 100	222	KI EDTODO
				2	2			7		145,00		1451 25	67 /	1 50vr	777	(I EOTOOO)
1.34		28.19	0.08	0.18	0.85	3.23	2 1.49	0.019032	1452.96	1452.58	1452.44	1451.62	87.6	2249 100yr	224	KLF2T2249
1.37	52.46		0.03		0.48		9 1.27	1		1452.47	Г	1451.62	67.4	2249 50yr	224	KLF2T2249
								П								
1.02		34.89	0.33	0.26	1.6		5 1.37			1453.3		1452.5	87.6	2296 100yr	229	KLF2T2296
0.97	57.13	29.72	0.27	0.21	1.38	2.43	3 1.17	0.009708	1453.46	1453.19	1453.18	1452.5	67.4	2296 50yr	229	KLF2T2296
1.1/		31.31	0.31	20.0	7.8.1	2.98	0.32	196510.0	1454.14	1433.6	1400.72	C.7C+T	0/.0	JAOOT GCC7	200	NLF212333
1.10			0.20		100		1			1 1 2 2	Т	1 2 2 2	27	100	1	חבברדום
-	53 13	25 78	96.0		1 63	2 77		0 014473	1453 98	1453 69	1453.62	1452.5	67.4	2339 50vr	233	KLF2T2339
1.15	53.94	30.59	0.39	0.19	1.98	3.32	8 1.24	0.012538	1454.82	1454.45	1454.33	1453	87.6	2389 100yr	238	KLF2T2389
1.1	50.59	25.84	0.32	0.14	1.69		0.98	0.011792		1454.33	1454.24	1453	67.4	2389 50yr	238	KLF2T2389
1.16	49.39	29.67	0.34	0.21	1.85		9 1.34	0.013029	1455.41	1455.03		1454	87.6	2435 100yr	243	KLF2T2435
1.16			0.28	0.15	1.67	2.95	7 1.11	0.013547	1455.23	1454.9	1454.81	1454	67.4	5 50yr	2435	KLF2T2435
	10.21	10.70	Ç.	0.00												
200	AO 21		VC U	0.08	1 23			- 1		1455 48	1455 48	1454 5	57.9	2468 100vr	246	KI F2T2468
0.98	36.17	19.27	0.18	0	1.07	2.36	7 0.06	0.010077	1455.64	1455.36	1455.36	1454.5	44.3	2468 50yr	246	KLF2T2468
1.29		18.74	0.12	0.08	1.06	3.15	0.81	0.017463	1456.16	1455.78	1455.66	1454.5	57.9	2498 100yr	249	KLF2T2498
1.19	33.42	16.34	0.08	0.04	0.78		0.52	0.0155	1455.97	1455.67	1455.59	1454.5	44.3	2498 50yr	249	KLF2T2498
86.0	37.4	22.52	0.05	71.0	0.42	2.03	19.0	0.009382	1430./1	1450.37	1400.30	1433	3/.9	2341 JUUYI	254	NLF212341
		77 55	200	0 1		Ī		Ţ		1456 37	1456 36	1 455	0.23	100	75.4	ETTEM
1.06	32.05	17.5		0.05		2.55	7 0.51	0.01187	1456.55	1456.24	1456.22	1455	44.3	2541 50yr	254	KLF2T2541
1.51	34.53	17.21		0.01		3.37	7 0.31	0.025217	1457.42	1457.02	1456.85	1456	57.9	2584 100yr	258	KLF2T2584
1.5		14.07				3.15	<u>.</u>	0.025935	1457.26	1456.9		1456	44.3	2584 50yr	258	KLF2T2584
0.93	51.21	26.62	0.27	0.28	1.29	2.44	1.33	0.008524	1458.17	1457.9	1457.9	1457.12	57.9	2637 100yr	263	KLF2T2637
				_		(m/s)	(m/s)	(m/m)	(m)	(m)		(m)				
	The section of		The popular	Liver Depute		100000000	1 4 51 5515	12.0000	F. C. C.C.	0116 11101		tarrest water man			Contract to the second	1000

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Node	River Sta Profile		Min Ch El		W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Ä	3	Vel Right	Hydr Depth L	Hydr Depth R	Flow Area	Top Width	Froude # Chl
		(m3/s)	(m)	1	(m)	(m)	(m)	(m/m)	(m/s)	(m/s)	(m/s)	[m]	(m)	(m2)	(m)	
KLF2T2008	2008 50yr		67.4	1448.51	1449.17	1449.28	1449.57	0.016889	1.58	2.96	1.43	0.22	0.19	26.22	68.25	1.2
KLF2T2008	2008 100yr		87.6	1448.51	1449.26	1449.39	1449.7		1.72	3.19	1.61	0.26				1.26
								1 1								
LF2T1961	1961 50yr	_	67.4	1447.5	1448.21	1448.35	1448.68		1.84	3.17	1.18	0.24				1.3
KLF2T1961	1961 100yr		87.6	1447.5	1448.3	1448.46	1448.85		2.03	3.45	1.42	0.29			60.21	1.38
1000	100		,	1111	1	1100	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2	3	2	2				
NLF2T1929	1920 400		17.70	744/1//	1440.02	70.044I	1440.27	Т	1.2	2.20	1.05	0.23				0.93
KLF211929	1929 100yr		8/.6	1447.27	1448.12	1448.12	1448.41	0.008848	1.31	2.45	1.23	0.27	0.25	39.05	73.12	0.94
KLF2T1902	1902 50yr		67.4	1447	1447.67	1447.72	1447.98	0.012736	1.25	2.56	1.3	0.19	0.2	28.49	64.87	1.09
KLF2T1902	1902 100yr		87.6	1447	1447.75	1447.82	1448.12	0.01286	1.45	2.82	1.49	0.24				1.12
KLF2T1878	1878 50yr	9	67.4	1446.54	1447.18	1447.29	1447.59	0.019791	1.34	2.87	0.94	0.15	0.09	24.65	63.15	1.32
KLF2T1878	1878 100yr		87.6	1446.54	1447.26	1447.4	1447.73	0.018973	1.55	3.12	1.18	0.2	0.13			1.33
KLF2T1841	1841 50yr		67.4	1446	1446.79	1446.74	1446.99	0.006819	0.83	2.04	0.99	0.17	0.21	35.65	72.56	0.81
KLF2T1841	1841 100yr		87.6	1446	1446.77	1446.84	1447.14		1.09	2.74	1.3	0.16				1.11
								\neg								
KLFZIIAIO	TOTO	l	0/.4	1440	1440.50	1446.56	1446./8		0.00	ZT.2	1.08	60.0				0.96
NLFZIIOIO	TOTO TOOM		0/.0	1440	1440.00	1440.00	1440.91	GTORON'O	0.85	2.29	7.25	0.13	0.24	40.31	82.4/	0.95
KLF2T1779	1779 50yr	0	67.4	1445.5	1446.23	1446.06	1446.34	0.003706	0.87	1.57	0.72	0.28	0.21	46.51	87.53	0.61
KLF2T1779	1779 100γι		87.6	1445.5	1446.32	1446.16	1446.46		0.99	1.76	0.85	0.33				0.64
KLF2T1736	1736 50yr		67.4	1445.5	1445.96		1446.11	0.007991	1.54	1.75	0.98	0.37			91.02	0.83
LF2T1736	1736 100yr		87.6	1445.5	1446.04		1446.22		1.55	1.94	1	0.37	0.2	46.65		0.85
KLF2T1701	1701 50yr	_	67.4	1444.84	1445.56	1445.56	1445.8	0.009327	1.25	2.27	0.97	0.24	0.16	31.99	69.46	0.94
KLF2T1701	1701 100yr		87.6	1444.84	1445.67	1445.67	1445.94	0.008071	1.32	2.38	0.9	0.29				0.9
E311663	1000		7,		111111111111111111111111111111111111111	447 07				3						
VEL V TOOD	IAOC COOT		07.4	C.+++T	1444.55	1445.07	1445.51	T	CO.T	2.03	1.03	U.LI			80.43	1.26
LF2T1663	1663 100yr		87.6	1444.5	1445.04	1445.16	1445.46	0.020858	1.28	3.04	1.9	0.14	0.25	32.07	84.1	1.37
KLF2T1631	1631 50yr	6	67.4	1444.02	1444.73	1444.71	1444.92	0.007735	1.28	2.15	1.28	0.29	0.29	37.55	88.39	0.87
KLF2T1631	1631 100yr		87.6	1444.02	1444.8	1444.8	1445.03		1.45	2,4	1.46	0.33				0.92
				L												
KLF2T1563	1563 50yr		67.4	1443.53	1444.12	1444.12	1444.32		1.17	2.05	0.97	0.21	0.16	35.44	92.84	0.95
KLF2T1563	1563 100yr		87.6	1443.53	1444.2	1444.2	1444.43	0.009409	1.32	2.21	1.11	0.26	0.2			0.94
KLF2T1513	1513 50vr		67.4	1443	1443 63	1443 63	1443 83		1 22	2 16	1 15	25.0				
KLF2T1513	1513 100yr		87.6	1443	1443.69	1443.71	1443.94	0.010245	1.51	2.41	1.31	0.3	0.24		99 97	000
							1	0.010		100	1.01			24.24		0.93
KI EST1464	1464 50vr		67 /		2				3	,	3		2		3	

Read Star Profite Carton Main Chi Carton Cart				h				HecRas Output Table] 🕝							1
165 165 165 162	Vode	River Sta Profile			_		E.G. Elev	E.G. Slope					Hydr Depth R	Flow Area		Froude # Ch
1428 Story 67.4 1442.81 144	(LF2T1464	1464 100yr	- 1		443.22	1443.16	- 1	397	1.08	2.02	1.17					0.79
1428 150pr 167.4 1442.81 1																
1488 1500yr 1576 1442,31 1442,89 1442,31 10.00011 10.035 2.15 1.15 0.13 0.31 0.31 0.32 10.37 10.37 13.58 13.58 13.58 10.07 10.07 1.15 1.15 0.13 0.31 0.32 13.58	LF2T1428	1428 50yr	67.4	1442.31		1442.81	1443		0.71	2	1.44	0.09	0.26			0.98
1383 50hr 67.4 1441.61 1442.81 1442.82 1442.47 0.012501 1.12 2.28 1.135 0.15 0.12 23.28 86.34 1319 1300hr 67.6 1441.61 1442.81 1442.32 1442.81 0.012565 0.72	LF2T1428	1428 100yr	87.6	1442.31	1 1	1442.89	1443.11	-	0.89	2.15	1.55	0.13	0.31			
1383 150 150 1444.52 1442.52 1444.																
1383 1399/ 1375 1444.62 1444.52 1444.52 1444.53 1444.54 1445.54 14	(LF2T1383	1383 50yr	67.4	1441.62		1442.26	1442.47		1.02	2.28	1.35	0.15	0.22			1.04
1323 50yr 67.4 1440.5 1441.26 1441.29 1441.25 0.024055 0.25 3.02 1.131 0.02 0.25 22.58 62.7	(LF2T1383	1383 100yr	87.6	1441.62		1442.35	1442.59		1.2	2.54	1.54	0.18	0.26			
137 100yr 876 1405 14015 140140 140181 1011867 0.7 32 1.95 0.0	LF2T1337	1337 50vr	67.4	1440.5	1441.26	1441.39	1441.7		0.26	3.01	1.81	0.01	0.21			1.45
1299 Syr 674 1439 1440.5 1440.5 1440.5 0.011665 0.4 2.44 0.44 0.04 0.04 0.06 27.84 56.76 1290 1200 1200 1200 1200 1433 1439.5 1440.6 1440.7 0.01273 0.7 2.74 0.7 0.08 0.08 0.08 32.85 66.19 1252 1200 1200 1200 1200 1438 1438.5 1438.	LF2T1337	1337 100yr	87.6	1440.5	1441.35	1441.49	1441.83		0.7	3.2	1.95	0.05	0.25			
1290 150 17 1493 1490 149								П								
1230 1250 1439.38 1440.28 1440.78	(LF2T1290	1290 50yr	67.4	1439.38	1440.6	1440.62	1440.9		0.4	2.44	0.44	0.04	0.04			1.04
1255 Solve 57.4	(LF2T1290	1290 100yr	87.6	1439.38		1440.75	1441.06		0.7	2.74	0.7	0.08	80.0			1.09
1152 2007	בזר דרם ו	4353	63	4450	1000	2001			2	3				3		
1422 10097 674 1438 1439.35 1439.46 1439.37 1439.46 1439.37 1439.46 1439.37 1439.46 1439.37 1439.47 1439.47 1439.47 1439.47 1439.47 1439.47 1439.48 1439.4	KI 212122	1353 100:-	07.0	1400	1400.02	1400.00	1440.43		1.50	3.74		0.1.0				
1220 SOlyr 67.4 1438 1439.55 1439.64 0.15609 1.29 2.55 1.64 0.17 0.25 30.62 92.48 1220 1000y 87.6 1438 1439.84 1439.54 1439.76 0.01787 1.54 2.91 1.99 0.27 0.28 35.24 96.51 1190 SOlyr 67.4 1438 1438.88 1439.76 1439.66 0.027335 1.34 2.79 0.67 0.14 0.05 25.15 77.45 1190 SOlyr 67.4 1438 1438.88 1439.76 0.019814 1.52 2.27 0.55 0.18 0.02 31.32 77.43 1190 SOlyr 67.4 1438 1438.89 1438.79 1438.60 0.00115 0.38 1.11 0.075 0.02 0.02 0.02 1101 SOlyr 67.4 1438 1438.89 1438.79 1438.60 0.00115 0.38 1.11 0.075 0.02 0.02 0.02 1101 SOlyr 67.4 1436.47 1438.69 1438.60 0.000046 0.25 0.34 0.02 0.02 0.02 1105 SOlyr 67.4 1438.41 1437.99 1438.60 0.000046 0.25 0.34 0.25 0.34 0.02 1105 SOlyr 67.4 1438.61 1438.69 0.000046 0.02 0.03 0.25 0.12 0.12 1105 SOlyr 67.4 1438.61 1438.69 0.000046 0.02 0.03 0.25 0.15 1006 Solyr 67.4 1438.61 1438.69 0.000046 0.02 0.03 0.25 0.15 1014 Solyr 67.4 1438.61 1438.69 0.000046 0.00000 0.0000 0.0000 0.0000 1014 Solyr 67.4 1438.61 1438.69 0.000046 0.00000 0.0000 0.0000 0.0000 0.0000 1014 Solyr 67.4 1438.61 1438.69 0.000005 0.011 0.05 0.05 0.05 0.05 0.00000 0.00000 1014 Solyr 67.4 1438.61 1438.61 1438.69 0.000005 0.011 0.000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.0000000 0.00000000	VELZITZZZ	TOOT 2021	07.0	1435	1435.5	1440.00	T440.44	0.021133	T.00	3.31	0.50	0.2				1.41
1200 100yr 876 1438 1439.4 1439.5 1439.6 101787 1.54 2.91 1.80 0.2 0.28 35.24 96.51 1190 100yr 67.4 1438 1438.68 1439.79 1438.08 1439.19 0.01381.4 1.52 2.97 0.95 0.18 0.09 31.32 77.43 1190 100yr 87.6	:LF2T1220	1220 50yr	67.4	1438.8	1439.35	1439.42	1439.64		1.29	2.55	1.64	0.17	0.25			1.18
1190 SOyr 67.4 1438 1438.69 1438.6	(LF2T1220	1220 100уг	87.6	1438.8		1439.5	1439.76		1.54	2.91	1.89	0.2	0.28			
1199 150/r 87.4 1438 1438.68 1438.79 1439.19 10.02335 1.34 2.79 0.05 0.14 0.05 25.15 77.43 1190 100/r 87.5 1.438 1438.76 1438.81 1439.19 0.019814 1.52 2.97 0.95 0.18 0.09 31.32 77.43 1190 150/r 87.5 1438.41 1437.91 1438.45 0.00156 0.82 1.21 0.75 0.62 0.54 69.56 95.75 1110 150/r 87.5 1438.47 1438.61 1438.7																
1190 100yr 87.6 1438 1438.76 1438.88 1439.19 0.019814 1.52 2.97 0.95 0.18 0.09 31.32 77.43 1150 100yr 67.4 1437 1438.41 1437.99 1438.46 0.0011.56 0.82 1.21 0.75 0.62 0.54 69.66 95.75 1150 100yr 87.6 1437 1438.47 1438.08 1438.71 0.000793 0.78 1.16 0.74 0.75 0.62 0.54 69.63 95.75 1101 100yr 87.6 1435.47 1438.43 1438.45 1438.49 0.00046 0.25 0.34 0.2 1.12 0.83 235.3 180.82 1101 100yr 87.6 1435.47 1438.43 1438.49 0.000046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1101 100yr 87.6 1435.51 1438.43 1438.49 0.000046 0.27 0.38 0.25 1.27 0.99 283.21 193.26 11055 100yr 87.6 1435.51 1438.49 1438.49 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 11014 100yr 87.6 1435.51 1438.49 1438.49 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 11014 100yr 87.6 1435.51 1438.49 1438.49 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 11014 100yr 87.6 1435.1 1438.49 1438.49 0.000005 0.11 0.16 0.09 1.91 1.46 2531.33 255.82 11014 100yr 87.6 1435.1 1438.49 1438.49 0.000005 0.13 0.19 0.11 0.10 0.09 1.91 1.46 2531.33 255.82 11014 100yr 87.6 1435.8 1438.69 0.000005 0.13 0.19 0.11 0.10 0.09 1.91 1.46 2531.33 255.82 11014 100yr 87.6 1434.68 1438.49 1438.49 0.000005 0.13 0.19 0.11 0.10 0.09 1.91 1.46 2531.33 255.82 11014 100yr 87.6 1434.68 1438.49 1438.49 0.000005 0.13 0.19 0.11 0.10 0.09 1.91 1.46 2531.33 255.82 11014 100yr 87.6 1438.49 1438.49 0.000005 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 11014 100yr 87.6 1434.68 1438.69 1438.69 0.00006 0.13 0.19 0.11 0.15 0.1 2.09 1.88 2597.64 266.79 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1267.64 1	(LF2T1190	1190 50yr	67.4	1438	1438.68	1438.79	1439.06	$\overline{}$	1.34	2.79	0.67	0.14	0.05			1.38
1150 SOyr	LF2T1190	1190 100yr	87.6	1438	1438.76	1438.88	1439.19	0.019814	1.52	2.97	0.95	0.18				
1150 50yr 67.4 1437 1484.1 1437.99 1438.40 0.001156 0.021 0.75 0.62 0.54 69.66 95.75 1150 100yr 87.6 1436.47 1438.43 1438.71 0.000793 0.78 1.16 0.74 0.75 0.62 0.54 69.66 95.75 1150 100yr 87.6 1436.47 1438.43 1438.44 0.000046 0.25 0.34 0.2 1.12 0.83 225.3 180.82 1101 100yr 87.6 1435.47 1438.69 1438.69 0.00046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1056 50yr 87.6 1435.51 1438.43 1438.69 0.000046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1014 50yr 87.6 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1014 50yr 87.6 1435.81 1438.69 0.000015 0.11 0.15 0.09 1.91 1.46 531.33 251.86 193 50yr 87.6 1434.68 1438.69 1438.69 0.000005 0.11 0.15 0.09 0.11 2.01 1.6 597.64 266.79 284.7 1438.69 1438.69 0.000005 0.12 0.13 0.15 0.11 2.20 1.88 596.98 2.69.78 193 50yr 87.6 1434.68 1438.69 1435.4 1435.4 1435.9 0.000005 0.12 0.13 0.15 0.11 2.20 0.18 596.98 2.69.78 284.7																
1150 100yr 87.6 1437 1438.07 1438.08 1438.71 0.000793 0.78 1.15 0.74 0.76 0.7 96.34 108.65 1101 100yr 67.4 1436.47 1438.43 1438.44 0.000046 0.25 0.34 0.2 1.12 0.83 225.3 180.82 1101 100yr 87.6 1436.47 1438.49 1438.69 0.000046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1005 100yr 87.6 1435.51 1438.43 1438.49 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 1005 100yr 87.6 1435.51 1438.49 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1004 50yr 67.4 1435.41 1438.49 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1004 50yr 87.6 1435.41 1438.49 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1004 50yr 87.6 1435.41 1438.49 1438.49 0.00005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 1004 50yr 87.6 1434.68 1438.49 1435.41 1438.49 0.00005 0.13 0.19 0.11 2.01 1.6 597.64 265.79 1435 1438.69 1435.41 1438.69 0.00005 0.13 0.19 0.11 2.01 1.6 597.64 265.79 1435 1438.69 1435.41 1438.69 0.00005 0.13 0.19 0.11 2.01 1.88 596.98 269.78 1435 1438.69 0.00005 0.13 0.19 0.11 2.01 2.01 2.01 2.02 667.9 284.7 1436 1438.69 0.00005 0.13 0.19 0.11 2.01 2.01 2.01 2.02 667.9 284.7 1436 1438.69 0.00005 0.13 0.13 0.14 0.15 0.11 2.01 2.01 2.01 2.01 2.01 2.01 2.01	(LF2T1150	1150 50yr	67.4	1437	1438.41	1437.99	1438.46		0.82	1.21	0.75	0.62	0.54			
1101 50yr 67.4 1436.47 1438.43 1438.44 0.000046 0.25 0.34 0.2 1.12 0.83 235.3 180.82 1110 100yr 87.6 1436.47 1438.69 1438.69 0.000046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1105.6 50yr 67.4 1435.51 1438.43 1438.44 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 1014 50yr 67.4 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1014 100yr 87.6 1435 1438.69 1438.69 0.00005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 1014 100yr 87.6 1434.68 1438.69 1438.69 0.00005 0.13 0.19 0.11 2.01 1.6 597.64 266.79 193 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.00005 0.12 0.15 0.1 0	LF2T1150	1150 100yr	87.6	1437	1438.67	1438.08	1438.71		0.78	1.16	0.74	0.76	0.7			0.32
1101 50yr 67.4 1436.47 1438.43 1438.44 0.000046 0.25 0.34 0.2 1.12 0.83 25.3 180.82 1101 100yr 87.6 1436.47 1438.69 1438.69 0.00046 0.27 0.38 0.23 1.27 0.99 283.21 193.26 1056 50yr 67.4 1435.51 1438.43 1438.69 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 10056 100yr 87.6 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 10014 50yr 67.4 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 10014 100yr 87.6 1435.81 1438.69 1438.69 0.000013 0.11 0.16 0.09 1.91 1.46 531.33 251.86 10014 100yr 87.6 1434.68 1438.44 1435.32 1438.45 0.000005 0.13 0.19 0.11 0.11 0.01 1.6 597.64 256.79 10014 100yr 87.6 1434.68 1438.69 1435.3 1438.69 0.000005 0.13 0.19 0.11 0.15 0.1 0.01 1.6 597.64 256.79 10014 100					1											
11011100yr 87.6	(LF2T1101	1101 50yr	67.4	1436.47	1		1438.44	0.000046	0.25	0.34	0.2	1.12	0.83			0.08
1056 50yr 67.4 1435.51 1438.43 1438.44 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 1056 100yr 87.6 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1014 50yr 87.6 1435 1438.69 1438.69 0.000005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 1014 100yr 87.6 1434.68 1438.69 1438.69 0.000006 0.13 0.19 0.11 0.11 0.10 0.15 597.64 266.79 193 100yr 87.6 1434.68 1438.69 1438.69 1438.69 0.000005 0.12 0.15 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.15 0.11 0	LF2T1101	1101 100yr	87.6	1436.47	i		1438.69	0.000046	0.27	0.38	0.23	1.27	0.99			
1056 50yr 67.4 1435.51 1438.43 1438.44 0.000011 0.15 0.22 0.13 1.67 1.33 396.55 221.06 1056 100yr 87.6 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1014 50yr 67.4 1435 1438.69 1438.69 0.000005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 1014 100yr 87.6 1434.68 1438.69 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 1993 50yr 67.4 1434.68 1435.32 1438.49 0.000005 0.12 0.15 0.1 2.01 1.88 596.98 269.78 1993 100yr 87.6 1434.68 1435.41 1435.42 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 284.7 1938 50yr 67.4 1434.68 1434.79 1434.79 1434.92 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 87.66 1434 1434.79 1434.79 1434.79 1435.94 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66 186.69 18																
1056 100yr 87.6 1435.51 1438.69 1438.69 0.000013 0.18 0.25 0.15 1.82 1.43 454.93 235.82 1014 50yr 67.4 1435 1438.44 1438.43 1438.44 0.000005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 1014 100yr 87.6 1435 1438.69 1438.69 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 1014 100yr 87.6 1434.68 1438.69 1438.41 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 1015 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 1016 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000006 0.12 0.15 0.11 2.01 2.02 667.9 1017 1018 1019 1019 1019 1019 1019 1019 1019 1019 1019 1019 1019 1018 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.01 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1438.69 0.000005 0.12 0.18 0.11 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1438.69 0.000005 0.12 0.18 0.11 2.01 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1438.69 1438.69 0.000005 0.12 0.18 0.11 2.01 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1438.69 1438.69 0.000005 0.12 0.18 0.11 2.01 2.01 2.02 667.9 1014 100yr 87.6 1434.68 1438.69 1438.69 1438.69 0.000005 0.12 0.18 0.11 2.01 2.01 2.02	LF2T1056	1056 50yr	67.4	1435.51			1438.44		0.15	0.22	0.13	1.67	1.33			0.04
4 1014 50yr 67.4 1435 1438.44 1435 1438.69 1438.44 0.000005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 4 1014 100yr 87.6 1435 1438.69 1438.69 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	LF2T1056	1056 100yr	87.6	1435.51	1438.69		1438.69		0.18	0.25	0.15	1.82	1.43			0.05
4 1014 50yr 67.4 1435 1438.44 1438.44 0.000005 0.11 0.16 0.09 1.91 1.46 531.33 251.86 4 1014 100yr 87.6 1435 1438.69 1438.69 0.000006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 93 50yr 67.4 1434.68 1438.44 1435.32 1438.44 0.000004 0.1 0.15 0.1 2.09 1.88 596.98 269.78 993 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 284.7 973 Culvert 973 Culvert 1434 1434.7 1434.7 1434.92 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.79 1434.79 1435.04 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66 98 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.60																
4 1014 100yr 87.6 1435 1438.69 1438.69 0.00006 0.13 0.19 0.11 2.01 1.6 597.64 266.79 993 50yr 67.4 1434.68 1438.44 1435.32 1438.44 0.000004 0.1 0.15 0.1 2.09 1.88 596.98 269.78 993 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 284.7 973 Culvert 973 Culvert 1 293 50yr 67.4 1434.7 1434.7 1434.9 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.79 1434.79 1434.93 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66 97.67	LF2T1014	1014 50yr	67.4	1435	1438.44		1438,44	Т	0.11	0.16	0.09	1.91	1.46			
993 50yr 67.4 1434.68 1438.44 1435.32 1438.44 0.000004 0.1 0.15 0.1 2.09 1.88 596.98 269.78 993 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 284.7 973 Culvert 973 Culvert 1434.67 1434.7 1434.92 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 938 50yr 87.6 1434 1434.79 1434.79 1434.92 0.008475 1.39 2.42 1.42 0.31 0.32 42.61 87.66 938 100yr 87.6 1434 1434.79 1434.79 1434.93 1.30 2.42 1.42 0.31 0.32 42.61 87.66	LF2T1014	1014 100yr	87.6	1435	1438.69		1438.69	\neg	0.13	0.19	0.11	2.01	1.6			0.03
993 100yr 87.6 1434.68 1438.69 1435.4 1438.69 0.000005 0.12 0.18 0.11 2.21 2.02 667.9 284.7 993 100yr 87.6 1434.8 1438.7 1434.7 1434.9 0.008379 1.39 2.42 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.7 1434.7 1434.9 1.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.6 97.6 97.6 97.6 97.6 97.6 97.6 97.6 9	1 F2T993	993 50vr	67 4	1434 68		1/35 33	1/38//		2	2		3 00	1 00			
973 Culvert 1434.79 14	I ESTGGS	003 100	976	1424 60	1	1 100:01	1430 60		041	010	044	20.7	1.00			
973 Culvert Culvert 1 1434.7 1434.7 1434.9 0.008445 1.22 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.7 1434.79 1435.04 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66 938 100 100 100 100 100 100 100 100 100 10	TL 71 232	JAOOT CEE	0/.0	1434.08		1435.4	1438.69	טטטטטט:	0.12	O.I.S	0.11	2.21	2.02			0.03
938 50yr 67.4 1434 1434.7 1434.92 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.79 1434.79 1435.04 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66	LF2T973	973	Culvert													
938 50yr 67.4 1434 1434.7 1434.92 0.008445 1.22 2.22 1.26 0.25 0.26 35.25 82.41 938 100yr 87.6 1434 1434.79 1434.79 1435.04 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66 87.60 87.6								Т								
938 100yr 87.6 1434 1434.79 1434.79 1435.04 0.008379 1.39 2.42 1.42 0.31 0.32 42.61 87.66	LF2T938	938 50yr	67.4			1434.7	1434.92		1.22	2.22	1.26	0.25	0.26			0.9
	LF2T938	938 100yr	87.6		1434.79	1434.79	1435.04	0.008379	1.39	2.42	1.42	0.31	0.32			0.92
	KI ESTO16	016 50	67 /	1 122 72	1424 76	1404 00	143467	00000	3	200	3				1	

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1.28		30.49	0.33	0.14	2.06		1.19	0.016915	1427.32	1426.98	1426.85	1426	87.6	380 100yr	38	KLF2T380
1.27	59.82	25.15	0.27	0.1	1.84	5 2.97	0.95	0.017342	1427.17	1426.87	1426.76	1426	67.4	380 50yr	38	KLF2T380
								-1								
1.25		32.32	0.26						1428.06	1427.75	1427.64	1427	87.6	423 100yr	42	KLF2T423
1.22	66.91	26.99	0.21	0.24	1.53	5 2.73	1.66	0.01658	1427.91		1427.57	1427	67.4	423 50yr	42	KLF2T423
1.19			0.33	0.54		Ī			7.074T	0C:074T	1420,27	C.724T	0,.0	TOOM	4	100
	60 63	20.00	0 00		1 00	217		0.012901		-1	1/178 77	1/177 5	87.6	466 100vr	45	KI FOTASS
1.14			0.29	0.29			1.7		1428.55	1428.27	1428.19	1427.5	67.4	466 50yr	46	F2T466
1.15			0.25	0.36	1.49		1.87	0.012503	1429.22	1428.86	1428.74	1427.5	87.6	504 100yr	50	KLF2T504
1.12	50.98	25.62	0.19			3.03				1428.74	1428.64	1427.5	67.4	504 50yr	50	KLF2T504
								\mathbf{I}								
1.37		27.79	0.21	0.31	1.6		2.07	0.018369	1429.84	1429.43	1429.24	1428.34	87.6	543 100үг	54	KLF2T543
1.39	51.49	22.29	0.16	0.25	1.38		1.86	0.019769	1429.68	1429.31	1429.14	1428.34	67.4	543 50yr	54	KLF2T543
1.13	70.23	34.58	0.3							1429.97	1429.87	1429	87.6	570 100yr	57	KLF2T570
1.12		28.28	0.25	0.31	1.49	2.89	1.72	0.012543	1430.12		1429.78	1429	67.4	570 50yr	57	F2T570
1.3		31.77	0.21		1.57	3.21	1.97		1430.76		1430.31	1429.5	87.6	603 100yr	60:	KLF2T603
1.27	68.24	26.29	0.17	0.25				0.017453	1430.62	1430.34	1430.23	1429.5	67.4	603 50yr	60	F2T603
							İ			-1						
0.95	81.71	40.62	0.31	0.26	1.46			_	1431.38		1431.11	1430.41	87.6	652 100yr	65	KLF2T652
0.94		33.42	0.26		1.33	2.21	1.16	0.009529	1431.25	1431.02	1431.02	1430.41	67.4	652 50yr	53	KLF2T652
								— †								
1.39			0.16			3.59		\neg	1432.01	1431.6	1431.41	1430.5	87.6	697 100yr	69	KLF2T697
1.44	54.73	21.45	0.11	0.14	1.11		1.34	0.022146	1431.87	1431.49	1431.3	1430.5	67.4	697 50γг	69:	KLF2T697
								\neg								
1.04		37.34	0.31		1.5			\neg	1432.54	1432.26	1432.17	1431	87.6	734 100vr	73,	KLF2T734
0.98	71.17	31.56	0.27	0.3	1.31	2.84	1.41	0.008849	1432.4	1432.15	1432.09	1431	67.4	734 50yr	73,	KLF2T734
		76:16	0.10					\neg	1701.00	1102:00	11000	1	9	Took		7
114		30 10	0.16		1 13		Ī	-	1437 95	1437 63	1/37 53	1431 5	87.6	770 100vr	77,	KI E2T770
1.11	58.69	26.38	0.12	0.1	0.91	2.68	0.83	0.013101	1432.79	1432.51	1432.43	1431.5	67.4	770 50vr	77(KLF2T770
0.89			0.21		1.05	2.42			1433.32		1433.05	1432	87.6	806 100yr	80	KLF2T806
0.91	69.96	32.24	0.16	0.19	0.89		1.02	0.008537	1433.19	1432.93	1432.93	1432	67.4	50yr	80	21806
1.28	67.26	30.9	0.2	0.28	1.5	3.16	1.86	0.01706	1433.74	1433.41	1433.28	1432.51	87.6	845 100yr	84	KLF2T845
1.7.1		00:47	2 5	22.0		I	Ī	L	1,000	П	1400.10	17.3071	1	O TO VOY!	9	1010
1 21		24 88	0 15	0.22	1 21	2 97	1 66	0.018724	1433 6	1433 31	1433 19	1432 51	67 4	50vr	84	:7T84T5
1.01	82.28	39.48	0.25	0.36	1.34	2.57		0.010366	1434.38	1434.12	1434.1	1433.36	87.6	892 100yr	89:	KLF2T892
0.97		33.35	0.21		1.17	2.32	1.56		1434.25	1434.03	1434.02	1433.36	67.4	892 50yr	89	-21892
1.33	78.84	32.35	0.17	0.31	1.44	3.07	2.09	0.019156	1434.75	1434.45	1434.34	1433.73	87.6	916 100yr	91	KLF2T916
	(m)	(m2)			(m/s)	(m/s)	(m/s)	-	(m)		(m)					
			The purpose in	יואמו טכטנו ר	ACI MRIIC	AGI CIIIII	אכו בכונ	ר.ט. טוססכ	ר.ט. רוכי	CITE VV.S.	אאים. רוכא	Ci C	עוסופו		1000	14000

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								나는	tput Table							
Node	River Sta Profile			Min Ch El	. Elev	Crit W.S.	Elev	pe	₽	<u> </u>	ght	Hydr Depth L	Hydr Depth R	Flow Area	Top Width	Froude # Chl
		le/cm)		(HII)	Ann	fini	init	funfunf	(111/3)	(III/3)	(c/lil)	(III)	(mil)	(mz)	fuil	
KLF1T1792	1792 50yr		67.4	1464.85	1465.16	1465.34	1465.75	0.061859	0.77	3.49	2.02	0.03	0.12	20.18	84.58	2.13
KLF1T1792	1792 100yr		87.6	1464.85	1465.21	П		0.05467	1.09	3.71	2.22	0.05	0.15	24.95	89.75	
KLF1T1715	1715 50yr		67.4	1461.92		1462.57	1462.82	0.024239	1.14	2.63		0.1		26.3	81.17	1.4
KLF1T1715	1715 100yr		87.6	1461.92	1462.53			0.026148	1.41	2.95	0.15	0.13	0	30.7	85.8	1.48
KLF1T1670	1670 50yr		67.4	1460.55	1460.9	1461.05	1461.39	0.044647	0.84	3.15	1.75	0.04	0.12	22.07	85.17	1.84
KLF1T1670	1670 100yr		87.6	1460.55	1460.95	П			1.16	3.39	1.92	0.07	0.15		91.92	
KLF1T1637	1637 50yr		67.4	1459.29	1459.74	1459.86	1460.14	0.030706	0.89	2.84	1.08	0.06	0.08	24.78	92.85	1.56
KLF1T1637	1637 100γг		87.6	1459.29	1459.78				1.22	3.19	1.3	0.09			98.72	1.64
KLF1T1584	1584 50yr		67.4	1456.93	1455.52		1455.66	0.013464	1.7			0.29		39.68	135.97	
KLF1T1584	1584 100yr		87.6	1456.93	1455.58	1455.58		0.013108	1.81			0.33		48.39		
KLF1T1528	1528 50yr		67.4	1454.63	1452.1	1452.1	1452.24	0.013976	1.66			0.27		40.59	148.18	
KLF1T1528	1528 100yr		87.6	1454.63	1452.15	1452.15			1.8			0.32		48.6	150.09	
KLF1T1498	1498 50yr		67.4	1453.91	1449.5	1449.69	1450.57	0.279096	4.57			0.13		14.76	111.43	0
KLF1T1498	1498 100yr		87.6	1453.91	1449.53	П		0.278271	4.81			0.14		18.2		
KLF1T1412	1412 50vr		67.4	1451.18	1447.33	1447.33	1447.49	0.013313	1 73			0.2		38 93	128 25	
KLF1T1412	1412 100yr		87.6	1451.18					1.85			0.35		47.24		0
VI E1T1240	1340 50.5		67 /	2000					3							
KLF1T1349	1349 100yr		87.6	1449.26	1446.69		1446.91	0.014891	2.06			0.36		42.51	117.06	
KLF1T1281	1281 50yr		67.4	1447.35	1445.85	1445.59		0.002877	1.14			0.51		59.22	115.58	
KLF1T1281	1281 100yr		87.6	1447.35	1445.95	1445.68	1446.03	0.003208	1.22			0.52		71.81	137.14	
KLF1T1226	1226 50yr		67.4	1446.08			1445.64	0.013525	1.8			0.32		37.47	117.77	
KLF1T1226	1226 100yr		87.6	1446.08	1445.55	1445.55			1.91			0.36		45.97		
KI F1T1172	1172 SOvr		67.4	1445 15	1444 77	1444 78		0 01611/	161			0.24		41 03		
KLF1T1172	1172 100vr		87.6	1445.15	1		1444 98					0.26		47 97	187 /6	
						П	П								100.10	
KLF1T1090	1090 50yr		67.4	1443.45	1443.38	1443.4	1443.53	0.019215	1.69			0.22		39.92	180.67	0
KLF1T1090	1090 100yr		87.6	1443.45	1443.43	1443.45	1443.59	0.017365	1.75			0.25		50.16		0
KLF1T1016	1016 50yr		67.4	1441.9	1442	1442.03	1442.16	0.018529	1.78	0.79	0.41	0.25	0.03	38.51	172.12	0.94
.F1T1016	1016 100γr		87.6	1441.9	14	1	1442.24	0.020109	1.98	1.09	0.67	0.27	0.05	45.2	182.64	1.05
KLF1T946	946 50vr	1	67.4	1440.03	1440 = 7		1440 00	0.019416	116	77/	1 27		0			

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0.45	123.67	115.14	0.34	0.27	0.67	1.4	0.58	0.00175	1479.6		1479.5	1478.5	157.8	6742 100yr	674.	KLF6742
0.42	119.12	103.72	0.4	0.35	0.71	1.24		L	14/9.48		14/9.41	14/8.5	125./	0/42 SUYI	10/4	NLF0/42
								\neg	4470		1000	1470 5	1267	FOR	674	166747
0.42	113.57	116.29	0.42	0.43	0.73	1.38	0.74	0.00155	1479.68		1479.58	1478.5	157.8	8 100уг	678	LF6788
0.4	111.91	104.57	0.4	0.4	0.67	1.23	0.67	0.001408	1479.55			1478.5	126.7	6788 50yr	678,	KLF6788
0.62	91.88	83.6		0.52	0.93		1.23		1479.78		1479.59	1478.5	157.8	6824 100yr	682	KLF6824
0.58	88.82	74.7	0.34	0.46	0.88	1.78		-	1479.65	1479.23		1478.5	126.7	6824 50yr	682	KLF6824
T.00	77.14	00.70		0:10		0.01		_								
1 2 !	75 10	30 45		0.16		3.01		0.021973		1416.47	1416.35	1415.68	87.6	91 100yr	9	KLF1T91
1.4	69.92	24.84		0.12		T	1.24		1416.66	1416.38		1415.68	67.4	91 50yr	9	KLF1T91
1.,	0,11	1						- 1								
1.73	57.71	24.68				3.55		പ	1419.35	1418.91	1418.71	1418	87.6	182 100yr	18.	KLF1T182
1.61	55.15	21,43				3.15		0.03145	1419.15	1418.8	1418.65	1418	67.4	182 50yr	18.	KLF1T182
	45.70	13./		71.0		40.4		\neg		7.77.7	1.00	4.1.4	0	2007	i	
1.0	A2 70	10.7		0.10		4 63			ı	1422.2	1421 88	1421	87.6	271 100vr	27	KLF1T271
208	38 13	15 46		0.06			1.16	0.049549	1422.78	1422,08	1421.78	1421	67.4	271 50yr	27:	KLF1T271
1.0	01.7							一			T					
1 35	51.7	28.17				3.12		- 1	1425.64	1425.27		1424.37	87.6	365 100yr	36	KLF1T365
1.27	49.71	24.3				2.77		0.018006	1425.46	1425.16	1425.07	1424.37	67.4	5 50yr	36	LF1T365
1.78	32./1	19.72	0.02	0.03	0.44	4.45	0.64	0.032906	1427./1	1427.02	1426./	1425.5	8/.0	441 TOOAL	1	NLT 1 1 441
1.81	27.94	15.78				4.27	Ī		ľ	1426.86	1426.57	1425.5	67.4	441 SUVI	1	KLF11441
								\neg								
1.49	48.03	25.72				3.41		0.024055	1429.47	1429.05	1428.88	1428	87.6	503 100yr	50.	KLF1T503
1.44	67.44	21.40				0.14		Т		T#20.33	T+20.73	074T	,	Joy	2	LY FI COL
4	44.20	21 16				214				1428 93	1428 70	1428	67 /	S SOVE	5	KI F1TS03
1.59	57.34	26.03				3.37		0.029223	1431.16	1430.75	1430.58	1429.84	87.6	567 100yr	56	KLF1T567
1.61	52.96	21.11				3.19		0.03129	1431.01	1430.65	П	1429.84	67.4	567 50yr	56.	KLF1T567
	, 2::0	Ú.	0.1.0	0:10				- 1						1		
1 22	77 9	21 21	0.23	0 28	17	2 15		- 11	1433 19	1432.87	1432.75	1432.1	87.6	654 100vr	65,	KLF1T654
1.27	69.42	26.62	0.19	0.24	1.47	2.83	1.72	0.017868	1433.04	1432.78	1432.68	1432.1	67.4	654 50yr	65,	KLF1T654
1.76	94.48	28.3	0.06	0.19	1.01	3.43	2.16	0.037437	1435.58	1435.22	1435.05	1434.59	87.6	746 100yr	74,	LF1T746
1.8	86.49	22.78	0.03	0.17	0.62	3.22	2.05	0.041499	1435.47	1435.14	1434.99	1434.59	67.4	746 50yr	741	KLF1T746
1.15	117.88	41.08	0.04	0.27	0.49		1.72	0.015503	1436.79	1436.59		1436.05	87.6	797 100yr	79	KLF1T797
111	112.48	34.98		0.23	0.23	2.11			1436.69	1436.52	1436,49	1436.05	6/.4	/9/ 50yr	6/	KLF11/9/
					3				430.00	1200		1000	3	1	1	1747707
2.02	79.8	24.47		0.16			2.16		1438.76	1438.27	1438.06	1437.59	87.6	868 100yr	86	KLF1T868
1.99	74.49	20.27		0.13			1.92		1438.6	1438.19		1437.59	67.4	868 50yr	86	KLF1T868
1.26	152.89	40.91	0.2	0.17	1.48	2.87	1.37	0.017316	1440.95	1440.73	1440.63	1440.03	87.6	946 100yr	94	KLF1T946
	Ш	Ц	\perp	1 1	Ш	ш	(m/s)	(m/m)	Ш	Ш						
	TOP SAIDCH	1000	Ligar Deputit	העטו הפטנוו ב	ACLVIBIL	Vel Citi	אבו רבונ	E.G. Slope	L.O. LICY	CHUV.S.	AA.D. FICA	IAILLI CU CI	ת וטומו	1 101110	INVESTIGATION OF THE PROPERTY	Mode

14

		Initiate Cta Intafila	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	F	- 1				_							7-21.d2 # CKI
COND Spyr. 125.7 12782 147921 147921 147926 0.012597 2.15 0.05 0.17 0.014 2.95 0.015 0.0		NACI OTA	(m3/s)	(m)	- 1								_			- Code
6049 1509/r 125.8 14785 14785 14785 14785 14785 14785 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14786 14787 14787 14788 14787 14788 1478	LF6704	6704 50yr	126.7			479.11	1479.34	84	1.09	2.15	0.96			60.09	Ш	0.99
G664 Spyr 125.7 1476.5 1477.81 1477.81 1478.82 0.052327 2.28 4.29 2.28 0.27 0.14 2.8 2.74 0.21 0.14 2.8 2.74 0.22	LF6704	6704 100yr	157.8		П		1479.45		1.2	2.3	1.03	0.21			138.6	0.98
	LF6664	6664 50vr	126.7			1477.63	1478.39		ω ω	4.69	2.26	0.17			77.45	
6629 SOPY 126.7 1474.76 1475.77 1475.76 1475.77 1475.76 1475.77 147	LF6664	6664 100yr	157.8		1 1	1477.67	1478.55		2.83	4.92	2.47	0.21			81.9	
6639 10099 1523	DC993	6639 50vr	1267			1475 75	1476 46	0 046913	2 15	4 56	1 97	0 16	014		68 67	
6888 6897 1267 12672 147124 14752 14752 147528 0.000979 1.25 2.77 1.24 0.23 0.24 0.23 0.44 55.68 170 0.24 0.25 0.2	ו בעעטט	6679 100vr	157 8		7	1475 85	1476 72	n n47718	1.93	4.98	2.27	0.14			75 74	
6585 SDPY 125.0	10050	MOOT CZOO	10,10		T	1.1000	1-17-0-7	0:017	į		!					
	LF6585	6585 50yr	126.7			1475.2	1475.58	0.009379	1.25	2.87	1.54	0.24			66.69	
Column C	LF6585	6585 100yr	157.8			1475.33	1475.75	Т	1.37	3.03	1.72	0.3		55.63	70	
Color Colo	I ECE 33	65350	1267			1/7/ 76	1/75 11		1	7 77	1 2/	0.0			77 77	
	ובעבסט	6533 1007	157 0		1	1/7/ 88	1/75 27		1 61	2 02	1 36	0.36			78 57	
6665 Solve 125.7 1473 1473.71 1473.81 1474.24 10019594 2.09 3.27 1.97 0.35 0.32 40.96 68.84 6645 Solve 125.8	LF0333	Moor ccco	157.0			T4/4.00	17.0/41		1.01	2.53	1.00	0.00			/0.5/	
646 100/r 1578 1473	LF6464	6464 50yr	126.7		П	1473.84	1474.24		2.09	3.27	1.97	0.35			68.84	
6411 150yr 126.7 1472.5 1473.23 1473.24 1473.54 0.01005.4 1.66 2.68 1.73 0.35 0.37 0.03 0.03 0.03 0.01 0.01 0.01 0.01 0.01	LF6464	6464 100yr	157.8		П	1473.96	1474.42		2.26	3.58	2.18	0.39			71.01	
Color Colo					T						<u>.</u>	0			3	
	LF0411	OALL SOVI	120./		Т	7472.24	7475.30	-	T.00	2.00	1./2	0.50			05.47	
6352 Solv 1267 1472 1472.84 1472.72 1472.03 0.005114 1.17 2.13 1.62 0.35 0.56 69.09 107.94 6352 100v 157.8 1472 1472.94 1472.81 1472.56 1472.94 1472.81 1472.95 0.025.67 1.99 2.31 1.76 0.39 0.62 79.43 112.88 6341 Solv 1267 1471.93 1472.66 1472.66 1472.94 0.009957 1.6 2.61 2.12 0.33 0.51 56.27 105.49 6341 Solv 1267 1471.9 1472.67 1472.67 1472.67 1472.67 1472.67 1472.67 1472.67 6324 Solv 1267 1471.5 1472.1 1472.27 1472.67 0.025.23 1.85 3.5 2.03 0.22 0.26 40.16 89.85 1.6 6324 Solv 1267 1471.5 1472.1 1472.27 1472.8 0.009572 1.74 2.8 2.23 0.39 0.56 66.34 112.17 6255 Solv 1267 1471 1471.76 1471.76 1472.03 0.09911 1.65 2.43 1.79 0.36 0.40 57.77 1112.6 6218 Solv 1267 1471 1471.75 1471.85 1471.85 1472.81 0.009971 1.65 2.43 1.79 0.36 0.47 57.43 114.43 6218 Solv 1267 1469.5 1470.63 1470.83 1471.27 0.025486 2.65 4.20 0.26 4.20 0.28 45.59 98.38 1.20 6119 Solv 1267 1465.5 1469.59 1469.59 1470.09 0.015809 1.63 4.09 1.85 0.24 0.24 0.28 45.59 98.38 1.20 6119 Solv 1267 1465.5 1468.97 1469.59 0.012027 1.66 4.75 1.68 0.36 0.31 4.71 8.19 0.012027 1.66 4.75 1.68 0.36 0.31 4.71 8.19 0.012027 1.66 4.75 1.68 0.36 0.31 4.71 8.19 0.012027 1.66 4.75 1.68 0.36 0.31 4.71 8.19 0.012027 1.66 4.75 1.68 0.012027 1.66 4.75 1.68 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1.66 4.75 0.012027 1	L CATT	0711 100%:	107.0		П	177.0.0	14,5,7			10:11	1.00	9			0,:55	
6352 100yr 1578 1472 1472.94 1472.81 1473.15 0.005267 1.25 1.76 0.39 0.62 79.43 112.8	LF6352	6352 50yr	126.7		П	1472.72	1473.03		1.17	2.13	1.62	0.35			107.94	
6341 Solv 126.7 1471.93 1472.66 1472.94 0.009957 1.6 2.61 2.12 0.33 0.51 56.27 105.49 105.49 6341 Solv 157.8 1471.93 1472.76 1472.76 1472.76 1472.76 1472.70 0.009957 1.74 2.8 2.23 0.33 0.51 66.34 112.17 1 6324 Solv 126.7 1471.5 1472.1 1472.27 1472.87 0.02933 2.04 3.5 2.03 0.22 0.25 40.15 89.85 1 6226 Solv 126.7 1471.5 1471.76 1471.76 1471.76 1472.33 0.009711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.24 2.25 100vr 126.7 1471.85 1471.85 1472.33 0.009711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.24 0.23 47.84 93.87 1 62218 Solv 126.7 1469.	LF6352	6352 100yr	157.8				1473.15		1.29	2.31	1.76	0.39			112.58	
6341 Soyr 126.7 1471.93 1472.66 1472.94 0.09957 1.6 2.61 2.03 0.51 56.27 105.49 6341 Doyr 127.8 1471.93 1472.76 1472.76 1472.60 0.009572 1.74 2.8 2.23 0.33 0.51 56.34 112.17 1 6324 Soyr 126.7 1471.5 1472.1 1472.27 1472.87 0.02533 1.85 2.03 0.22 0.26 40.16 89.85 1 6324 Soyr 126.7 1471.5 1472.1 1472.27 1472.87 0.026933 2.04 3.69 2.24 0.28 0.32 47.84 93.87 1 6265 Soyr 126.7 1471.81 1471.76 1472.73 0.00931 1.65 2.43 1.79 0.36 0.41 57.77 111.26 0 6228 Soyr 126.7 1469.5 1470.83 1471.85 1472.15 0.009374 1.77 2.6 1.96 0.41 0.47 57.43 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>																
6341 100yr 157.8 1471.93 1472.76 1472.80 0.09672 1.74 2.8 2.23 0.39 0.56 66.34 112.17 1472.11 1472.17 1472.67 0.009672 1.74 2.8 2.23 0.39 0.56 66.34 112.17 1472.11 1472.17 1472.17 1472.17 1472.17 1472.17 1472.27 1472.23 1.85 3.5 2.03 0.22 0.26 40.16 89.85 1 6265 50yr 126.7 1471 1471.76 1472.37 1472.33 0.099711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.40 57.77 111.26 0.41 0.99711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.41 0.99711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.24 0.99711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.099711 1.65 2.43	LF6341	6341 50yr	126.7				1472.94		1.6	2.61	2.12	0.33			105.49	
6324 50yr 126.7 1471.5 1472.1 1472.27 1472.8 0.02233 1.85 3.5 2.03 0.22 0.26 40.16 89.85 1 6324 100yr 157.8 1471.5 1472.19 1472.37 1472.8 0.020933 2.04 3.69 2.24 0.28 0.32 47.84 99.87 1 6265 50yr 126.7 1471 1471.76 1471.76 1472.03 0.099711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.251 50yr 157.8 1471 1471.85 1471.85 1471.27 0.026486 2.65 4 2.07 0.41 0.47 67.43 114.43 0.251 100yr 157.8 1469.5 1470.7 1470.92 1471.41 0.02573 2.89 4.24 2.26 0.4 0.28 45.59 98.38 1 6218 50yr 126.7 1469.5 1469.5 1470.7 1470.92 1471.41 0.02573 2.89 4.24 2.26 0.4 0.28 45.59 98.38 1 6119 50yr 126.7 1469.5 1469.4 1469.71 1470.25 0.015603 1.88 4.35 1.81 0.3 0.29 45.46 81.49 1 6119 50yr 126.7 1466.5 1468.79 1469.59 1469.53 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.49 0.29 45.46 81.49 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1469.59 0.012057 1.61 4.48 0.29 0.24 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1468.99 1469.59 0.012057 1.61 4.48 0.29 0.24 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1466.5 1468.79 1468.99 1469.59 0.012057 1.61 4.48 0.29 0.24 0.24 0.23 33.41 1 6119 50yr 157.8 1469.5 1469.5 1468.99 1469.5 10012057 1.61 4.48 0.29 0.24 0.24 0.23 33.41 1 6119 50yr 157.8 1469.5 1469.5 1469.5 1469.5 1469.5	LF6341	6341 100yr	157.8		Т	1472.76	1473.06	-	1.74	2.8	2.23	0.39				
	166224	6327 500	1267		Т	1/77 77	147267		1 00	o n	2 03	2				
6225 SOyr 126.7 1471 1471.76 1471.76 1472.03 0.009711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0.00 6265 SOyr 126.7 1471 1471.76 1472.03 0.009711 1.65 2.43 1.79 0.36 0.4 57.77 111.26 0 6228 SOyr 126.7 1469.5 1471.85 1471.85 1472.15 0.009374 1.77 2.6 1.96 0.41 0.47 67.43 114.43 0 6218 SOyr 126.7 1469.5 1470.63 1470.83 1471.27 0.026486 2.65 4 2.07 0.34 0.24 38.56 92.78 6218 Soyr 157.8 1469.5 1470.73 1470.83 1471.27 0.026486 2.65 4 2.07 0.34 0.24 38.56 92.78 6218 Soyr 157.8 1469.5 1470.7 1470.83 1471.41 0.026493 2.26 0.4 2.02 0.24	156324	6324 100vr	157.8		Т	1/177 37	1/77 8	_	201	3 60	2 2/	95.0				
6265 S0yr 126.7 1471 1471.76 1471.76 1471.76 1471.76 1471.71 1471.76 1471.71 1471.71 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.85 1471.83 1471.85 1471.81 1268.85 2.65 4 2.07 0.34 0.24 38.56 92.78 98.38 1 6159 S0yr 126.7 1469.79																
	LF6265	6265 50yr	126.7		П		1472.03		1.65	2.43	1.79	0.36			111.26	
6218 50yr 126.7 1469.5 1470.63 1470.83 1471.27 0.026486 2.65 4 2.07 0.34 0.24 38.56 92.78 6218 100yr 157.8 1469.5 1470.7 1470.92 1471.41 0.02573 2.89 4.24 2.26 0.4 0.28 45.59 98.38 1 6119 50yr 126.7 1467.76 1469.34 1469.59 1470.09 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 1 6119 50yr 126.7 1467.76 1469.41 1469.71 1470.25 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 1 6119 50yr 126.7 1469.41 1469.71 1470.25 0.015603 1.88 4.35 1.81 0.3 0.29 45.46 81.49 1 6119 50yr 126.7 1468.53 1468.99 1469.53 0.012057 1.61 4.48 1.48 0.29 0.26 38.22 71.85 1 6070 50yr 126.7	LF6265	6265 100yr	157.8		П		1472.15		1.77	2.6	1.96	0.41			114.43	
6218 SOW 126.7 1469.5 1470.83 1471.27 0024886 2.65 4 2.07 0.34 0.24 38.56 92.88 6218 100yr 157.8 1469.5 1470.7 1470.92 1471.41 0.02573 2.89 4.24 2.26 0.4 0.28 45.59 98.38 1 6159 50yr 126.7 1467.76 1469.34 1469.59 1470.09 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 1 6159 50yr 157.8 1467.76 1469.44 1469.59 1470.09 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 1 6119 50yr 157.8 1467.76 1468.47 1469.51 1469.53 0.012057 1.61 4.48 1.48 0.29 0.24 0.23 38.22 71.85 1 6119 50yr 126.7 1466.5 1468.79 1469.53 0.012057 1.61 4.48 1.48					7											
6218 100yr 1578 1469.5 1470.7 1470.92 1471.41 0.02573 2.89 4.24 2.26 0.4 0.28 45.59 98.38 6159 50yr 126.7 1467.76 1469.34 1469.59 1470.09 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 6159 100yr 157.8 1467.76 1469.41 1469.71 1470.25 0.015603 1.88 4.35 1.81 0.3 0.29 45.46 81.49 6119 50yr 126.7 1466.5 1468.67 1468.99 1469.53 0.012057 1.61 4.48 0.29 0.26 38.22 71.85 6119 100yr 157.8 1466.5 1468.79 1469.69 0.01222 1.86 4.75 1.68 0.36 0.31 47.1 83.19 6070 50yr 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 5.16 5.16 5.16 5.16 5.16 5.16 5.16	LF6218	6218 50yr	126.7		Т	1470.83	1471.27		2.65	4	2.07	0.34				
6159 50yr 126.7 1467.76 1469.34 1469.59 1470.09 0.015809 1.63 4.09 1.59 0.24 0.23 37.52 72.85 6159 100yr 157.8 1467.76 1469.41 1469.71 1470.25 0.015603 1.88 4.35 1.81 0.3 0.29 45.46 81.49 6159 50yr 126.7 1468.57 1468.67 1468.99 1469.53 0.012057 1.61 4.48 0.29 0.26 38.22 71.85 6179 100yr 157.8 1466.5 1468.79 1469.51 1469.69 0.01222 1.86 4.75 1.68 0.36 0.31 47.1 83.19 6070 50yr 126.7 126.7 1468 1467.67 1468.53 0.036327 5.16 5.16 5.16 5.16 5.16 5.16 5.16 5.16	LF6218	6218 100yr	157.8		Т	1470.92	1471.41	0.02573	2.89	4.24	2.26	0.4				
6159 100yr 157.8 1467.76 1469.41 1469.71 1470.25 0.015603 1.88 4.35 1.81 0.3 0.29 45.46 81.49 6119 50yr 126.7 1466.5 1468.67 1468.99 1469.53 0.012057 1.61 4.48 0.29 0.26 38.22 71.85 6119 100yr 157.8 1466.5 1468.79 1469.69 0.01222 1.86 4.75 1.68 0.36 0.31 47.1 83.19 6070 50yr 126.7 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 5.16 5.16 2.16 2.16 2.17 2.17 2.17 2.17 2.17 2.17 2.17 2.17	LF6159	6159 50yr	126.7			1469.59	1470.09	\neg	1.63	4.09	1.59	0.24				
6119 SOyr 126.7 1466.5 1468.67 1468.99 1469.53 0.012057 1.61 4.48 1.48 0.29 0.26 38.22 71.85 6119 100yr 157.8 1466.5 1468.79 1469.1 1469.69 0.01222 1.86 4.75 1.68 0.36 0.31 47.1 83.19 6070 SOyr 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 5.16 24.57 33.41	LF6159	6159 100yr	157.8		T	1469.71	1470.25		1.88	4.35	1.81	0.3				
6119 100yr 157.8 1466.5 1468.79 1469.1 1469.69 0.01222 1.86 4.75 1.68 0.36 0.31 47.1 83.19 6070 50yr 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 5.16 24.57 33.41	LF6119	6119 50vr	126.7		\neg	1468.99	1469.53		1.61	4.48	1.48	0.79			71 85	
6070 50yr 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 24.57 33.41	LF6119	6119 100yr	157.8		П		1469.69		1.86	4.75	1.68	0.36				
60/0) Solyr 126.7 1466 1467.18 1467.67 1468.53 0.036327 5.16 24.57 33.41						1										
	KL 0070	6070 100-	157.0		Т	1407.07	1400.33	_		07.50				24.5/		

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1.17	42.72	37.49	0.21	0.13	1.23	4.56	7 0.9	5 0.011027	1451.75	1451.14	1450.72	1448.5	157.8	4621 100yr	KLF4621
1.29	21.44	27.63						Т			Т		1.077	TYOU TYOU	120.
		27.63				7 50	л			1			1267	4621 SOvr	KI E4601
1.21	82.83	49.9	0.51	0.31	2.38	4.27	7 1.7	1 0.012397	1452.31	1451.83	1451.61	1449.5	157.8	4666 100yr	6666
1.23	72.88		0.44	0.25	2.22			_					126.7	4666 50yr	KLF4666
								П			П				
0.97			0.3	0.34	1.48		5 1.62	$\overline{}$	1452.88	1452.62	1452.62	1452	157.8	4715 100yr	KLF4715
0.96			0.26	0.29	1.35					1		1452	126.7	4715 50yr	KLF4715
								$\overline{}$							
0.56			0.29	0.26	0.78	1.64			1453.08		П		157.8	4753 100yr	KLF4753
0.53	134.97	88.95	0.24	0.21	0.67	1.49	9.0	7 0.002719	1452.97		1452.86	1452	126.7	4753 50yr	KLF4753
0.66	134.69		0.73	0.32	1.72	1.94		3 0.004047		1452.89		1452	157.8	4795 100yr	KLF4795
0.		79.28	0.65	0.26	1.6	1.8	3 0.86	1 0.004053	1453.11	1452.8	1452.98		126.7	4795 S0yr	KLF4795
											П				
1.68	94.13	45.02	0.48	0.35	3.31	4.98		7 0.02632		1453.25	1453.02		157.8	4849 100yr	KLF4849
1.67			0.42	0.3	3.07	4.74	7 2.45		1453.63	1453.16		1452	126.7	4849 50yr	KLF4849
								=							
0.79			0.62	0.35	1.67		1 1.14						157.8	4904 100уг	KLF4904
0.79	106.65	62.58	0.52	0.27	1.52	3.04	1 0.97	9 0.004961	1454.19	1453.9	1453.88	1452	126.7	4904 50yr	KLF4904
0.60		,4:10	1	c	1.00		1	_					10,101	1400A	
	117.05		0.74	0,5	1 68	20				П	Т		157 8	100vr	KI ENON3
0.82	107.68	63.77	0.46	0.45	1.5	2.88	3 1.46	4 0.005643	1454.4	1454.13	1454.13	1452.5	126.7	4943 50vr	KLF4943
0.00	27.411	İ	0.70	0.02	1./	14:2	1.0	0,000//3	1+0+./0	T404.07		1433	137.0	TOOK!	VL14304
			27.0	063	17			П		1	1/6/66		1570	100/ 100	
0.66	108.89	76.56	0.68	0.57	1.56	2.28	7 1.39	6 0.003687	1454.6	1454.28		1453	126.7	4984 50vr	KLF4984
0.95	101.86	66.72	0.59	0.46	2.1	2.95	3 1.78	4 0.008033	1455.04	1454.72	1454.72	1453.5	157.8	5031 100yr	KLF5031
0.94		57	0.53	0.39	1.96		3 1.59	1 0.008133	1454.91	П			126.7	5031 50yr	
										П					
1.15			0.65	0.36	2.83		3 1.89						157.8	5076 100yr	
0.92	92.37	56.75	0.61	0.37	2.15	2.58	6 1.54	8 0.008106	1455.28	1454.96	1455.01	1454	126.7	5076 50yr	KLF5076
1.14			0.6	0.46	2.48	3.99	9 2.08	2 0.010989	1456.02		T	1454	157.8	5126 100yr	KLF5126
1.18	82.33	47.17	0.52	0.43	2.38		7 2.1		1455.89	1455.54	1455.45	1454	126.7	5126 50yr	
12.1	40.10	32.30	ç,	0.51	40.2	4.02	2.30	10210.0	1430.7	1430.20	147.0CH	C.+C+1	0./CT	JANOT TOTA	VELOTOT
		50.00	0.1	0.51	7 7 7	Ī		\neg		Т	Т		1570	7101 100	
1 1		47 12	0 47	0.45	2.1	3 57	202	0 010698	1456 52	1456 17	1456.07	1 454 5	126.7	5181 50vr	KI E5181
1.15		51.62	0.31	0.61	1.57							1455	157.8	5225 100yr	
1.19	64.57		0.26	0.57	1.48	4.16	9 2.49	8 0.011969	1457.08	1456.64	1456.42	1455	126.7	5225 50yr	KLF5225
1.04	103.3	63.27	0.47	0.56	1.97	3.51	4 2.22	9 0.009554	1457.79	1457.47	1457.41	1455.5	157.8	5277 100yr	KLF5277
				(m)			(m/s)	(m/m)	(m)	(m)	(m)	(m)			
A COMPANY OF STREET	A Property Commencer		hiyar bebuilt	חישו הבטנור ב	ACLIMBILE	ACI CITII	: Act Fett	L.G. Jiope	L.O. LICY	CITC VV.J.	AA.D. FICA	MILL CIT CI	oral.	ואואכו זימ ויוסוויכ	Tana Car

				000	יר י		2	0 00777	1444 75	1444	1/1/10	1 1 1 2	207 2	2709 100	2705	2000
0.94	125.71	114.76	0.66	0.58	2.19		1.99	9 0.007487	1444.59	1444.13	1444.14	1443	325.6	3798 50yr	3798	KLF3798
0.2																
0.62				0.95		2.52			1444.98			1443.02	387.3	3845 100yr	3845	KLF3845
0.6	146.11	163.5	1.06		1.87		1.64	2 0.00291	1444.82		1444.6	1443.02	325.6	3845 50yr	3845	KLF3845
0.64			0.83			2.35			1445.16			1443.5	387.3	3904 100yr	3904	KLF3904
0.64	157.31	160.04	0.73	0.63	1.57		3 1.42	5 0.003353	1445		1444.78	1443.5	325.6	3904 50yr	3904	KLF3904
0.77			0.94			2.61	1.63		1445.35	1444.91	1445.07	1443.81	387.3	3949 100yr	3949	KLF3949
0.8	173.75	144.65	0.83	0.5	2.19		3 1.57	1 0.005548	1445.21	1444.82	1444.94	1443.81	325.6	3949 50yr	3949	KLF3949
								- 1								
١	187.52	105.98	0.58				2.76		1445.76		1444.98	1444.02	387.3	4001 100yr	4001	KLF4001
1.6			0.52	0.35	3.33		3 2.57	5 0.023983		1445.13	1444.9	1444.02	325.6	4001 50yr	4001	KLF4001
1.1			0.24	0.4	1.37	3.18	1.92			1445.49	1445.41	1444.5	157.8	4092 100yr	4092	KLF4092
1.09	112.43	52.83	0.2	0.34	1.23		1.74	8 0.011415	1445.68	1445.4	1445.33	1444.5	126.7	4092 50yr	4092	KLF4092
1.16			0.32			3.03					Π	1445.5	157.8	4159 100yr	4159	KLF4159
1.14	128.51	53.32	0.29	0.25	1.67		1.54	9 0.013411	1446.49	1446.23	1446.15	1445.5	126.7	4159 50yr	4159	KLF4159
1.02		66.62	0.31	0.25	1.6	2.49		4 0.010863	1447.34			1446.33	157.8	4221 100yr	4221	KLF4221
0.99	122.05						3 1.24			1446.97	1446.97	1446.33	126.7	4221 50yr	4221	KLF4221
								- 1	Ì	П						
	114.02	62.6	0.4			3.05					1	1446.5	157.8	4255 100yr	4255	KLF4255
1.08			0.36	0.4	1.81		1.94	1 0.011579	1447.61	1447.34	1447.3	1446.5	126.7	4255 50yr	4255	KLF4255
								\neg			П					
1.04	ی			0.28	_	2.76		\neg				1447.5	157.8	4337 100yr	4337	KLF4337
1.01	103.3	54.28	0.38		1.8		1.36	0.010493	1448.49	1448.21	1448.19	1447.5	126.7	4337 50yr	4337	KLF4337
9								\neg		Т	П			1007		
96.0			0.48			2.68		- 1	Ī	Т	Т	1448	157.8	100vr	4387	KI F4387
0.96	107.36	57.54	0.42	0.35	1.77		1.58	8 0.009072	1448.98	1448.71	1448.71	1448	126.7	4387 50yr	4387	KLF4387
0./3					1.53			0.00455/		1449.04	1449.18	1448	15/.8	4431 100yr	4431	KLF4431
	100.00	20.11		0.50				0.00	11.010	Т	Т	1 1 1 0	120.7	2091	1	1 1 1 1 1
0.7					1 38			0 0004393	1449 26		1449 08	1448	1267	7/131 SOwr	1131	K) EAA31
1.14	100		0.57		2.43	Г	3 2.41	0.01128	1449.73	1449.4	1449.34	1448	157.8	4478 100yr	4478	KLF4478
1.1			0.53			3.61	2.19	П		1449.31	П	1448	126.7	4478 50yr	4478	KLF4478
		0.1.10								, ocito		1		TOOP	100.	1 1000
1 38		52 15						╗	1450 53	1450 13	П	1448 5	157.8	4532 100vr	4537	KI E4532
1.45	93.36	42.55	0.41	0.36	2.57	4.45	2.37	1 0.019534	1450.44	1450.04	1449.86	1448.5	126.7	4532 50yr	4532	KLF4532
1.13		54.18	0.4	0.4			1.86	0.010642	1451.18	1450.71	1450.51	1448.5	157.8	4578 100yr	4578	KLF4578
0.87	95.02	56.43	0.41	0.42	1.46	3.36	1.46		1450.93	1450.62	1450.53	1448.5	126.7	4578 50yr	4578	KLF4578
		(m2)			(m/s)	Ш	Ш	(m/m)	(m)			(m)				
rrouge # Cill	lob Width	Flow Area	nyar Depti z	Hydr Depth L	Vel Kignt	Vei Chini		L.G. Slope Vel Leit	r. G. r. av	CITE W.S.	VV.O. LIGV	VIII CII CI	ת וסומו	710110	INVESTIGATION OF	INCOC

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1977 5077 1975 14425 14439 144420 1008917 134 285 138 0.85 0.85 13464 149.07 1777 5077 1975 144424 14437 14438 0.08917 136 285 135 0.55 13445 14405 0.77 14442 14437 14438 0.08927 1.46 285 1.47 0.47 0.45 13445 0.45 0.45 13445 0.65 0.77 14442 14438 0.08928 1.48 2.25 1.49 0.47 0.45 0.45 13445 0.65 0.78 14445 0.08928 1.48 1.48 0.08928 1.48 2.25 1.49 0.47 0.45								\neg								
1555 1557 1575 14425 14435 144425 100997 176 286 114 189				0.79				Ε	1440.07		1439.87	1437.25	387.3	100yr	3095	KLF3095
SSSP/F 325.5 1442.5 1443.9 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1439.91</td> <td></td> <td>1439.74</td> <td>1437.25</td> <td>325.6</td> <td>50yr</td> <td>3095</td> <td>KLF3095</td>									1439.91		1439.74	1437.25	325.6	50yr	3095	KLF3095
1950 1973 14425 14439 14439 14439 1003917 176 286 188 0.76 0.81 1414 1909 1050 1050 1415 14449 1003917 138 282 193 0.82 0.82 193 0.83 193 0.83 0.83 193 0.83 193 0.83 193 0.83 0.83 193 0.83 193 0.83 0.83 193 0.83 193 0.83 0.83 193 0.83 0.83 193 0.83 0.83 193 0.83																
150pr 325.6				0.7						1439.73	1439.82	1438	387.3	100yr	3139	KLF3139
150pr 387.5 1442.5 1443.2 1444.5 1444.5 100937 1.76 2.66 1.8 0.76 0.81 141.4 130.57 150pr 387.5 1442.4 1443.5 1444.5 1444.3 100937 1.86 2.87 1.75 0.52 0.83 1442.5 1440.5 150pr 387.5 1442.4 1443.5 1443.5 1444.3 100937 1.86 2.87 1.75 0.52 0.52 0.53 134.5 150pr 387.5 1442.4 1443.6 1443.8 100922 1.26 2.88 1.75 0.79 0.6 151.1 150pr 387.5 1442.1 1443.6 1443.8 100922 2.2 3.02 1.18 0.67 0.67 151.2 150pr 387.5 1442.1 1443.6 1443.8 100927 2.2 3.02 1.18 0.67 0.67 151.2 150pr 387.5 1441.8 1442.3 1442.8 1443.8 0.00927 2.2 3.02 1.18 0.67 0.64 118.4 150pr 387.5 1441.8 1442.3 1442.3 1442.3 100947 2.2 3.0 1.9 0.65 0.64 118.4 150pr 387.5 1440.8 1442.3 1442.3 100918 2.2 2.2 3.0 1.9 0.65 0.64 133.5 150pr 387.5 1440.8 1442.3 1442.3 1442.3 0.00918 2.2 2.2 3.0 0.69 0.75 0.64 138.9 150pr 387.5 1440.8 1442.3 1442.3 0.00918 2.2 2.2 2.2 0.69 0.75 0.64 0.64 150pr 387.5 1440.8 1442.3 1442.5 1442.8 0.00918 2.2 2.2 0.69 0.69 0.73 125.3 150pr 387.5 1440.8 1442.3 1442.8 0.00948 2.2 2.2 0.69 0.75 0.64 0.63 0.69 0.73 150pr 387.5 1440.8 1441.9 1441.9 0.00948 2.2 2.2 0.69 0.77 0.64 172.3 125.3 150pr 387.5 1440.8 1441.9 1441.9 0.00741 2.4 3.5 0.00948 2.2 0.69 0.72 0.64 0.62 0.64 0.62 150pr 387.5 1440.8 1441.8 1441.9 0.00741 2.4 3.5 0.00948 2.2 0.6 0.8 0.7 0.6 0.7 0.7 150pr 387.5 1440.8 1441.8 1441.8 0.00741 2.4 3.5 0.00948 0.7 0.6 0.6 0.7 0.7 0.7 150pr 387.5 1440.8 1440.8 0.00948 0.00948 1.2 0.6 0.6 0.6 0.6 0.7 0.7 0.7 150pr 387.5 1440.8 1440.8 0.00948 0.00948 1.2 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6				0.62					П	1439.61	1439.69	1438	325.6	50yr	3139	KLF3139
550yr 335.6 1404.5 1404.05 1404.05 1404.05 1404.05 1404.05 1404.05 1404.05 1404.05 1404.05 1404.05 1404.39 0.003971 1.85 2.82 1.93 0.33 0.08 158.33 130.07 150pr 387.3 1404.2 1404.05 1404.39 0.003921 1.86 2.81 1.55 0.52 0.53 130.07 150pr 387.6 1404.1 1403.05 1404.39 0.00522 2.08 2.87 1.77 0.07 0.6 133.15 141.1 150pr 387.3 1404.1 1404.20 1404.38 0.00522 2.2 3.52 1.78 0.65 151.22 146.43 150pr 387.3 1404.1 1404.23 1404.38 0.008875 2.2 3.52 1.9 0.65 151.22 146.38 150pr 387.3 1404.2 1404.23 0.008975 2.2 3.52 1.9 0.65 0.54 183.39 110.0				0.62			T	- 1		1440.09	1439.93	1438.1	38/.3	TOOAL	3184	KLF3184
55yr 235.6 1442.5 1443.92 1444.25 000397 1.74 2.64 1.8 0.76 0.81 141.41 130.97 150yr 387.3 1442.4 1443.64 1443.94 1443.94 1443.94 000397 1.85 2.82 1.93 0.88 158.33 150.07 150yr 387.3 1442.4 1443.94 0005023 1.24 2.2 1.52 0.52 0.53 134.55 10005 150yr 387.3 1442.1 1443.95 1443.95 000522 1.2 1.73 0.79 0.6 133.15 141.32 150yr 387.3 1441.8 1443.95 1443.85 0.00522 1.2 3.2 1.73 0.79 0.6 133.15 141.32 160yr 387.3 1441.8 1443.25 1443.85 0.00527 2.2 3.52 1.91 0.75 0.61 133.45 14.32 160yr 387.3 1440.83 1442.24 1442.85 0.0								-	T	1439.93	1439.61	1436.1	323.0	100	2104	NLF3104
55(p) 235.6 1442.5 1443.93 1444.25 003977 1.76 2.64 1.8 0.76 0.81 141.41 13.097 15(0) 387.3 1442.4 1443.94 1443.96 143.96 0.03971 1.85 2.22 1.33 0.83 0.88 158.63 156.07 15(0) 387.6 1442.4 1443.96 1443.96 0.05023 1.24 1.2 0.052 0.33 134.95 140.05 15(0) 387.3 1442.4 1443.96 1443.71 0.05022 1.22 1.73 0.97 0.65 155.1 150.47 15(0) 387.3 1441.8 1443.20 1443.83 0.05022 2.2 3.52 1.91 0.05 0.57 0.57 0.57 1443.31 199.42 15(0) 387.3 1441.1 1442.24 1442.83 0.06581 2.05 0.57 0.53 0.54 183.21 1443.83 0.06581 2.07 0.08 0.54 83.93								-	Τ	1,000 05	1 1 20 01	1,300 1	מאב ה	705	210/	KI E2194
50yr 33.5.6 1442.5 1443.92 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1444.05 1445.05 145.07				0.71				\neg		1440.57	1440.52	1438.71	387.3	100yr	3235	KLF3235
50yr 33.5.6 1442.5 1443.92 1444.25 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1443.65 1444.89 0.003971 1.85 2.82 1.93 0.88 138.63 136.07 50yr 32.5.6 1442.4 1443.62 1443.62 1443.61 0.05522 1.54 2.6 1.55 0.52 0.53 134.55 1440.05 50yr 325.6 1442.41 1443.93 1443.25 1443.25 1444.21 0.05222 1.24 2.8 1.73 0.47 0.6 150.1 150.47 100yr 325.6 1441.81 1443.93 1443.25 1443.25 100522 2.2 3.35 1.78 0.67 0.54 133.15 144.21 100yr 325.6 1441.41 1442.23 1443.55 1443.25 1443.25 1443.25 1443.25 1443.25 1443.25 1443.25 1443.25 1443.25								\blacksquare		1440.44	1440.39	1438.71	325.6	50yr	3235	KLF3235
50yr 325.6 1442.5 1443.92 1443.92 1444.72 0.03317 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1443.62 1443.99 0.003971 1.85 2.82 1.93 0.88 128.63 136.07 50yr 325.6 1442.4 1443.62 1443.62 1443.72 0.05222 1.46 2.81 1.73 0.04 150.07 150.07 50yr 325.6 1442.41 1443.62 1443.62 1443.83 0.005222 2.28 2.87 1.73 0.07 0.6 133.15 144.32 100yr 325.6 1441.48 1442.32 1042.93 0.06481.23 2.05 2.23 1.23 0.67 0.54 118.43 129.47 100yr 325.6 1441.41 1442.24 1442.83 0.061901 3.12 4.43 2.97 0.65 0.54 118.43 129.43 100yr 327.6 1440.83 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>																
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50yr 325.6 1442.5 1443.92 1444.25 0.00397 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1443.05 1443.39 0.00397 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.95 0.005023 1.46 2.81 1.73 0.47 0.6 150.1 150.07 50yr 325.6 1442.1 1443.26 1443.27 0.005022 2.2 3.02 1.94 0.6 133.15 144.32 100yr 325.6 1441.48 1442.93 1443.29 0.00481 2.05 3.22 1.73 0.75 0.6 133.15 144.32 100yr 325.6 1441.44 1442.23 1443.39 0.00481 2.0 3.22 1.91 0.75 0.51 134.23 144.33 100yr 325.6 1441.41 1442.23 1442.39 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1440.86</td><td>1440.86</td><td>1439.26</td><td>325.6</td><td>50yr</td><td>3290</td><td>KLF3290</td></t<>										1440.86	1440.86	1439.26	325.6	50yr	3290	KLF3290
50yr 325.6 1442.5 1443.92 1444.25 0.03917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1440.55 1444.35 1443.64 1443.95 0.003971 1.85 2.82 1.93 0.83 138.63 136.07 50yr 325.6 1442.4 1443.65 1443.62 1443.62 1443.72 0.00522 1.26 1.25 0.52 0.53 134.56 140.05 100yr 325.6 1442.1 1443.85 1443.85 0.00522 2.22 2.28 1.73 0.79 0.6 133.15 141.32 100yr 325.6 1441.48 1442.93 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>																
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50yr 325.6 1442.5 1443.92 1444.22 0.03917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 150yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.62 1443.12 0.00522 1.46 2.81 1.73 0.47 0.6 150.1 150.47 100yr 387.3 1442.4 1443.35 0.00522 2.28 2.87 1.73 0.47 0.6 150.1 150.47 100yr 387.3 1442.4 1443.35 0.00522 2.2 3.02 1.84 0.87 0.67 151.22 144.33 100yr 387.3 1441.4 1442.93 1442.33 1005033 2.2 3.35 1.78 0.87 0.67 151.22 146.43 100yr 325.6 1441.4 1442.33 0.006527 2.2				0.64						1440.85	1441.27	1439.05	325.6	50yr	3339	KLF3339
50yr 325.6 1442.5 1443.92 1444.22 0.03917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 135.07 50yr 325.6 1442.4 1443.62 1443.62 1443.7 0.05023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 50yr 325.6 1442 1443.96 1443.7 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442.14 1443.96 1443.85 0.00522 2.2 3.02 1.84 0.67 0.61 151.22 146.43 50yr 325.6 1441.48 1442.93 1442.93 1443.95 0.065375 2.2 3.52 1.91 0.57 0.51 133.15 141.32 100yr 325.6 1441.9<									I							
50yr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 135.07 50yr 325.6 1442.4 1443.64 1443.95 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 325.6 1442.4 1443.62 1443.1 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 100yr 325.6 1442.4 1443.49 1443.85 0.00522 2.2 3.02 1.84 0.87 0.6 150.1 150.47 50yr 325.6 1441.48 1442.93 1443.85 0.06375 2.2 3.35 1.78 0.67 0.54 118.43 129.42 100yr 325.6 1441.24 1442.93 0.06				0.85				0.007226		1441.63	1441.63	1440.06	387.3	100vr	3395	KLF3395
50yr 325.6 1442.5 1443.92 1444.02 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.75 1443.62 1443.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442.1 1443.93 1443.93 0.00523 2.08 2.87 1.73 0.47 0.6 133.15 141.32 100yr 325.6 1441.48 1442.93 1442.93 1443.93 0.005361 2.0 3.35 1.78 0.67 0.54 133.15 144.33 100yr 325.6 1441.48 1442.93 1443.93 0.06481 2.0 3.35 1.78 0.67 0.54 118.43 129.42 50yr 325.6 1				0.77				0.007411		1441.49	1441.49	1440.06	325.6	50yr	3395	KLF3395
50yr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.62 1443.75 1443.62 1443.72 0.005023 1.46 2.81 1.7 0.47 0.6 150.1 150.47 100yr 325.6 1442 1443.93 1443.73 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1441.48 1442.93 1443.85 0.00522 2.2 3.25 1.73 0.75 0.6 153.15 141.32 100yr 387.3 1441.48 1442.93 1443.85 0.00522 2.2 3.25 1.78 0.67 0.54 133.15 141.32 100yr 387.3 1441.						Ĭ					1.00			, foot		
50yr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 325.6 1442.4 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 100yr 325.6 1442.1 1443.82 0.05321 2.08 2.87 1.73 0.79 0.6 150.1 150.47 50yr 325.6 1441.48 1442.93 1443.83 0.06375 2.2 3.02 1.84 0.87 0.67 151.22 146.3 50yr 325.6 1441.41 1442.24 1443.83 0.06				0.84					1442 46		1442 05	1440 5	387 3	100vr	3441	KI F3441
50yr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1443.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 387.3 1442.4 1443.75 1443.62 1443.1 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 387.3 1442 1443.49 0.05252 2.0 2.87 1.73 0.79 0.6 150.1 150.47 50yr 387.3 1441.48 1442.93 1443.83 0.00522 2.2 3.02 1.84 0.67 0.61 133.15 146.43 50yr 387.3 1441.48 1442.93 1443.83<				0.77			ĺ		1442.28		1441.92	1440.5	325.6	50yr	3441	KLF3441
Styr 335.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 335.6 1442.4 1443.64 1443.62 1443.62 1443.12 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 50yr 387.3 1442.4 1443.62 1443.12 0.00522 1.46 2.81 1.7 0.47 0.6 135.15 140.05 50yr 387.3 1442 1443.49 1443.45 0.00522 2.2 3.02 1.84 0.87 0.6 133.15 141.32 50yr 387.3 1441.48 1442.93 1443.85 0.00526 2.2 3.35 1.78 0.67 0.54 133.15 141.32 50yr 387.3 1441.4				0.70						1447.10	1442.29	1440.63	307.3	TOOL	7040	NLF340/
Styr 325.6 1442.5 1443.92 1444.22 0.03917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.62 1443.12 0.005023 1.54 2.6 1.55 0.52 0.53 134.55 140.05 50yr 325.6 1442.4 1443.62 1443.1 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442.1 1443.36 0.00522 2.28 2.87 1.73 0.79 0.6 133.15 141.32 100yr 387.3 1442.1 1442.93 1443.83 0.005375 2.2 3.02 1.84 0.87 0.67 151.22 146.43 50yr 387.3 1441.48 1442.93 1443.83 0.018				0.20			Ī	\neg		1442.00	1442 20	140.00	20.0	100	2407	KLI JAO7
Sbyr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442.4 1443.62 1443.12 0.005361 2.08 2.87 1.73 0.47 0.6 150.1 150.47 100yr 325.6 1442.1 1443.49 0.05361 2.08 2.87 1.73 0.47 0.6 150.1 150.47 100yr 387.3 1442.1 1443.93 100523 2.2 2.87 1.73 0.79 0.6 133.15 141.32 100yr 387.3 1441.48 1442.93 1443.85 0.00522 2.2 </td <td></td> <td></td> <td></td> <td>0.60</td> <td></td> <td></td> <td>1</td> <td>\neg</td> <td>1442 53</td> <td>1442 05</td> <td>1442 15</td> <td>1440 83</td> <td>375 6</td> <td>50</td> <td>3487</td> <td>KI E3/187</td>				0.60			1	\neg	1442 53	1442 05	1442 15	1440 83	375 6	50	3487	KI E3/187
Solyr 335.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 135.07 Solyr 325.6 1442.4 1443.64 1443.62 1443.12 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 387.3 1442.4 1443.62 1444.12 0.005223 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442.4 1443.85 1443.7 0.05361 2.08 2.87 1.73 0.79 0.6 150.1 150.47 50yr 387.3 1442.4 1443.83 1443.85 0.00522 2.2 3.02 1.84 0.87 0.67 151.22 146.43 100yr 387.3 1441.8 144				0.00			Ĭ	_	Ĭ	1442.5/	1442.11	1441	36/.3	TOOL	3520	KLF3520
Sbyr 325.6 1442.5 1443.92 1444.22 0.03917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.96 0.05023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 387.3 1442.4 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442 1443.49 1443.7 0.005321 2.08 2.87 1.73 0.79 0.6 150.1 150.47 50yr 325.6 1441.48 1442.93 1443.85 0.00532 2.2 3.02 1.84 0.87 0.6 133.15 141.32 100yr 387.3 1441.48 1442.93 1443.95<				0.00			T	7	T	140.07	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	4 4 4 4	2072	100	25.70	KI FOEOC
50yr 325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 100yr 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 50yr 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 100yr 387.3 1442.4 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 50yr 325.6 1442 1443.49 1443.85 0.00522 2.0 2.87 1.73 0.79 0.6 133.15 141.32 50yr 387.3 1442 1443.49 1443.85 0.00522 2.2 3.0 1.84 0.87 0.67 151.22 146.43 50yr 387.3 1441.48 1442.93 1443.85 <td></td> <td></td> <td></td> <td>0.58</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1442.24</td> <td>1447</td> <td>1441</td> <td>375.6</td> <td>50vr</td> <td>9656</td> <td>KI F3526</td>				0.58						1442.24	1447	1441	375.6	50vr	9656	KI F3526
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 387.3 1442.4 1443.75 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 325.6 1442.4 1443.75 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 387.3 1442.4 1443.49 1443.85 0.00522 2.08 2.87 1.73 0.79 0.6 133.15 141.32 387.3 1442.4 1443.49 1443.85 0.00522 2.2 3.02 1.84 0.87 0.67 151.22 146.43 4 143.49 1443.49				0.75				т—		1443.06	1443.06	1441.48	387.3	100yr	3578	KLF3578
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 387.3 1442.4 1443.75 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 325.6 1442.4 1443.96 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 387.3 1442 1443.96 1443.85 0.00526 2.08 2.87 1.73 0.79 0.6 133.15 141.32 387.3 1442 1443.49 1443.85 0.00522 2.2 3.02 1.84 0.87 0.67 151.22 146.43				0.67				\Box	1443.39	1442.93	1442.93	1441.48	325.6	50yr	3578	KLF3578
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 387.3 1442.4 1443.75 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 387.3 1442.4 1443.75 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 387.3 1442.1 1443.75 0.005361 2.08 2.87 1.73 0.79 0.6 133.15 141.32 325.6 1442.1 1443.62 1443.7 0.005361 2.08 2.87 1.73 0.79 0.6 133.15 141.32				0.87				П	1443,83		1443,49	1442	38/.3	ΙΟΟΥΓ	3628	KLF3628
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 r 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 325.6 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 r 387.3 1442.4 1443.65 1443.62 1444.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47 325.6 1442 1443.63 1443.63 1443.63 2.88 2.87 1.73 0.79 0.6 133.15 141.32				7007		Ī			1442 00		1445 40	1444	2072	100	2000	VI FOCOCO
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 r 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 387.3 1442.4 1443.64 1443.96 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05 387.3 1442.4 1443.62 1443.12 0.00522 1.46 2.81 1.7 0.47 0.6 150.1 150.47				0.79					1443.7		1443.36	1442	325.6	SOVE	3628	KI F3628
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97 7 387.3 1442.5 1444.05 1444.39 0.003971 1.85 2.82 1.93 0.83 0.88 158.63 136.07 325.6 1442.4 1443.64 0.005023 1.54 2.6 1.55 0.52 0.53 134.56 140.05				0.47						1443.62	1443.75	1442.4	387.3	100yr	3680	KLF3680
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97				0.52					1443.96		1443.64	1442.4	325.6	50yr	3680	KLF3680
325.6 1442.5 1443.92 1444.22 0.003917 1.74 2.64 1.8 0.76 0.81 141.41 130.97				0.83				$\neg \vdash$	1444.39		1444.05	1442.5	387.3	100yr	3737	KLF3737
				0.76		П			1444.22		1443.92	1442.5	325.6	50yr	3737	KLF3737
(m3/s) (m) (m) (m) (m) (m/m) (m/s) (m/s) (m/s) (m) (m2) (m2)	(m)	(m2)	(m)	(m)			(m/s)	(m/m)	(m)							
er Sta Profile Q Total Min Ch El W.S. Elev Crit W.S. E.G. Elev E.G. Slope Vel Left Vel Chnl Vel Right Hydr Depth L Hydr Depth R Flow Area Top Width Froude # Chl		Flow Area	Hydr Depth R	_	Vel Right			E.G. Slope	E.G. Elev					Profile	River Sta	Node

03:21 PM

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0.96		200	7.5	0.8			2.54	41 0.00/XII	/ 1430./4	1430.37	1430.37	T428.5	387.3	TOSOLTOVY	DCOT	VLLTOOO
	191.92	135.38	0.48	0./3		ĺ		\neg	T	T	Т		0.020	1000 0001	1000	X171070
	200	207 20		0.73		I				Т	Т		375 6	500	1858	1 E1 858
	171.97	116.68	0.64	0.65	3.13	Ĭ	8 3.17	4 0.016078	1431.14	1430.69	1430.54	1429	387.3	1901 100yr	1901	KLF1901
1.35	158.74	102.18	0.58	0.63		4.55		_	T	Т	Т		325.0	TAOT POAL	TOGI	KLFISOI
			0					_	I	ï	Т		335.5	5	100	1001
1.15	163.63	127.67	0.71	0.68	2.72		4 2.64	6 0.010454	2 1431.76	1431.32	1431.2	1429.5	387.3	100yr	1949	KLF1949
3 1.14	156.13	112.47	0.65	0.62	2.55	4.16	8 2.49	2 0.010478	2 1431.62	П	1431.11		325.6	1949 50yr	1949	KLF1949
	170.89	148.36	0.69	0.78	2.12	3.84	5 2.29			1431.76			387.3	1999 100үг	1999	KLF1999
0.93	161.84	130.56	0.63	0.71		μ	3 2.16	4 0.006583	5 1432.04		1431.65	1429.5	325.6	1999 50yr	1999	KLF1999
		100				I										
0.83	177 81	165	0.73	0.88	1.91	3.64		\neg		П			387.3	2034 100vr	2034	KLF2034
	168.74	144.62	0.67	0.8			9 2.05	5 0.005059	1432.25	1431.86	1431.93	1430	325.6	2034 50yr	2034	KLF2034
		10	0.00	0.00						Т	П			100		
	170 58	154 95	0.56	0.85	1.72	3.56				П	T		387.3	2081 100vr	2081	KLF2081
0.87	164.49	136.42	0.5	0.76			5 2.12	1 0.005825	1432.51	1432.14	1432.16	1430.5	325.6	2081 50yr	2081	KLF2081
1.07	154.39	130.15	0.57	0.8		ļu	6 2./3	/ 0.009056	1433.07	1432.63	1432.56	1431	387.3	2135 100yr	2135	KLF 2135
	170.00	20:411	0.01	0.70	10:1			7	ĺ	T	Т		0.010	1001	2100	
106	1/19/66	11/1 80	051	0.73			2 7 7	0 000135	1/137 03	1/22 52	1/37 /6	1/31	275.6	500	2135	KI E2135
1.13	152.64	126.9	0.87	0.64	3.08		5 2.51	5 0.01025	1433.65	1433.21	1433.15	1431.64	387.3	100уг	2195	KLF2195
1.11	148.83	113.71	0.8	0.59		3.94		I_{\sim}		Г	Г		325.6	2195 50yr	2195	KLF2195
									Γ	Т	Т					
	159.51	142.26	0.57	0.68	1.88	3.28	5 2.1				1433.58	1431.98	387.3	2240 100yr	2240	KLF2240
0.91	153.51	124.36	0.49	0.6		ņ	3 1.98	8 0.006943	1433.88	1433.47			325.6	2240 50yr	2240	KLF2240
0.85	154.12	150.91	0.57	1	1.71		1 2.49	8 0.005591	1434.38	1433.91	1434.01	1432.5	387.3	2297 100yr	2297	KLF2297
0.82	149.09	135.88	0.52	0.92		2.97	3 2.31	3 0.005353	1434.23	1433.8	1433.92	1432.5	325.6	2297 50yr	2297	KLF2297
0.97	127.5	126.5	0.69	0.68	2.24	3.59	6 2.23	3 0.007456		1434.31	1434.29	1432.69	387.3	2348 100yr	2348	KLF2348
0.96	121.4	111.43	0.61	0.63	2.07		4 2.13	6 0.007534	1434.66	1434.18	1434.16	1432.69	325.6	2348 50yr	2348	KLF2348
								$\overline{}$		П						
0.96	128.59	129.24	0.65	0.82		3.55	2 2.48			П	1434.64	1432.97	387.3	2391 100yr	2391	KLF2391
	123.56	113.66	0.58	0.73	2.01		2 2.34	8 0.007432	1434.98	1434.51	1434.51	1432.97	325.6	50yr	2391	KLF2391
								\neg								
	141.64	163.94	0.6	0.95	1.45						1434.97	1433.14	387.3	100yr	2415	KLF2415
0.69	136.3	145.2	0.54	0.86		2.62	3 1.83	2 0.003713	1435.12	1434.61	1434.83	1433.14	325.6	50yr	2415	KLF2415
														100%	r	1
	132.47	116.26	0.72	0.8	2.83	4.32		- 1			1		387.3	2453 100vr	2453	KI F2453
1.19	127.34	101.64	0.67	0.71			4 2.85	7 0.011574	1435.37	1434.91	1434.78	1433.23	325.6	50yr	2453 50yr	KLF2453
0.99	146.48	137.81	0.84	0.87	2.52	4.1	8 2.57	9 0.007158	1435.89	1435.44	1435.43	1433.5	387.3	2492 100yr	2492	KLF2492
	(m)	-	-			(m/s)	(m/s)	1	m	ত্রি	3					
Froude # Chl	Top Width	Flow Area	Hydr Depth R	Hydr Depth L	Vel Right	Vel Chnl	Vel Left	E.G. Slope Vel Left	E.G. Elev	Crit W.S.	W.S. Elev	Min Ch El	Q Total	Profile	River Sta Profile	Node

1 05	164 92	134	0.76	0.72			2.63	1 0.009574	1425.81	1425.39	1425.36	1424.24	387.3	COVI	1286 100yr	KL-1286
1.03	160.98	120.44	0.7	0.66	2.55	3.24		1425.67 0.009328	1425.67	1425.29	1425.28	1424.24	325.6	Oyr	1286 50yr	KLF1286
	166.46	135.28	0.56	0.71	2.13	3.61	2.5		1426.24	1425.82	1425.77	1424.5	387.3	ООУГ	1331 100yr	KLF1331
1.03			0.51				2.33	0.008987	1426.1	1425.72	1425.67	1424.5	325.6	50yr	1331 5	KLF1331
			0.64	0.66		3.33	2.03	0.00641	1426.51	1426.11	1426.11	1424.5	387.3	100уг	1367 1	KLF1367
0.89	170.56	132.66	0.6		1.89		1.87	0.006414	1426.38	1426.01	1426.01	1424.5	325.6	Oyr	1367 50yr	KLF1367
0.73			0.55		1.44		1.36		1426.73		1426.42	1425	387.3	00yr	1407 100yr	KLF1407
0.72	189.65	153.21	0.48	0.44	1.32	2.51	1.25	0.004192	1426.59	1426.19	1426.32	1425	325.6	Оуг	1407 50yr	KLF1407
							Ī	- 1								
0.96			0.62					- 1	1426.94		1426.57	1425	387.3	00yr	1442 100yr	KLF1442
0.97	183.91	132.54	0.55	0.69	1.96	3.4	2.29	2 0.007722	1426.82	1426.47	1426.47	1425	325.6	Oyr	1442 50yr	KLF1442
		133.68	0.45		1.85	<i>(</i> 1)	1.65		1427.21	1426.79	1426.71	1425.5	387.3	00yr	1474 100yr	KLF1474
1.03	173.12		0.37	0.32	1.67	3.2	1.5	8 0.009317	1427.08	1426.69	1426.61	1425.5	325.6	Oyr	1474 50yr	KLF1474
											G!					
1.1			0.68					1 0.010483	1427.51	1427.12	1427.05	1426	387.3	00yr	1505 100yr	KLF1505
1.08	183.19	120.81	0.62	0.5	2.48	3.33	2.15	3 0.010437	1427.38	1427.03	1426.97	1426	325.6	50yr	1505 5	KLF1505
			0.75						1427.84		1427.46	1426	387.3	100yr	1541 1	KLF1541
1.01	187.12	130.23	0.67	0.6	2.35	3.52	2.18	0.008422	1427,72	1427.37	1427.36	1426	325.6	Oyr	1541 50yr	KLF1541
		100.00		0.00				\neg	17.00.01	17.00	1717	1	00.0	00)		1000
		135.95	0.75	0.55				_	1428.21		1427.73	1426	387.3	DOVr	1578 100vr	KLF1578
1.12	190.57	122.65	0.7	0.5	2.67	4.06	2.13	3 0.010289	1428.08	1427.73	1427.66	1426	325.6	Oyr	1578 50yr	KLF1578
		1	0.00	0.10		Ī			111000	11010	1.100.11	11200	i i	- Jook	1	1
	202 03		28.0	0.45				_	1428 53	1428 16	1428 11	1426 5	387 3	novr	1613 100vr	KI F1613
1.03		124.98	0.77	0.4	2.61	3.69	1.67	0.008683	1428.41	1428.07	1428	1426.5	325.6	Oyr	1613 50yr	KLF1613
1.05	189.26	138.36	0.73	0.49	2.57	3.75	1.97	0.009064	1428.94	1428.55	1428.46	1426.91	387.3	00yr	1659 100yr	KLF1659
	179.78		0.68	0.46	2.36			0.008334	1428.8	1428.43	1428.39	1426.91	325.6	Оуг	1659 50γε	KLF1659
1.05	10,10	100.40	0.70	0.1	1:00	,		0.0000	1720.00		17600	1.031.1	10, 10	- Poy	1,02 1004	VEI 11/02
			24. U	0 27	2 52			╗	1/70 33		1/28 8	1426 5	287 2	3	1700	E1702
1.04	170.04	116.19	0.69	0.31	2.44	3.82	1.43	0.008765	1429.2	1428.8	1428.68	1426.5	325.6	Ovr	1702 50yr	KLF1702
1.1		141.47	0.78	0.57	2.83	4.22	2.31		1429.74	1429.37	1429.3	1427.5	387.3	00уг	1746 100yr	KLF1746
1.1	192.01		0.72	0.52	2.71	4.07	2.17	0.010132	1429.62	1429.28	1429.21	1427.5	325.6	Оуг	1746 50yr	KLF1746
			0.00	0.70				$\neg \Gamma$	1.00.00	11000	H-1-10-1-1	1	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	_	1,00	Figure
86.0			0.58	0.76	2.04		2.46	Π.	1430.08	1429 73	1429.71	1427.5	387 3	OVI	1784 100vr	KI F1784
0.98	201.98	136.18	0.51	0.69	1.89	3.81	2.32	0.00794	1429.97	1429.64	1429.62	1427.5	325.6	Oyr	1784 50yr	KLF1784
1.08		145.1	0.5	0.73	2.06	4.21	2.66	0.0097	1430.43	1430.08	1430.02	1428	387.3	00уг	1823 100yr	KLF1823
1.06		129.21	0.45	0.67	1.92	4.04	2.49	0.009568	1430.31	1429.99	1429.94	1428	325.6	0yr	1823 50yr	KLF1823
	(m)	(m2)	(m)	(m)	(m/s)	(m/s)	(m/s)	(m/m)	(m)	(m)	(m)		(m3/s) (m)			
1						7			-						1	

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	0.59 0.66 0.72 0.9 0.74 0.89 0.94 1.04 1.04	0.67	2.34	3.22	2 2.21			T	1421.31	1417.75	426.7	9 100yr		
	0.59 0.66 0.72 0.9 0.74 0.89 0.94 1.04	0.67		Ī			1/21 75	1421 26		1/10 00			739	KLF739
	0.59 0.66 0.72 0.9 0.74 0.89 0.94 1.04					9 0.007005	П		1421.18	1419.99	359.4	9 50yr	739	KLF739
	0.59 0.66 0.72 0.9 0.94	0.07			7.02	0.00.11	200.1741		1721.50	2777	150.7	i rool.		
	0.59 0.66 0.72 0.9 0.74 0.89	0 07	7 77	200				П	1421 56	1420	426.7	763 100vr	76	KI F763
	0.59 0.66 0.72 0.9 0.74 0.89	0.8			9 1.9	3 0.004369	1421.73	1421.24	1421.44	1420	359.4	763 50yr	76	KLF763
	0.59 0.66 0.72 0.9	0.61			4 2.08	2 0.007504	1422.2	1421.74	1421.74	1420.49	426.7	802 100yr	80	KLF802
	0.59 0.66 0.72 0.9	0.51	2.69	3.45		\blacksquare		П	1421.57	1420.49	359.4	802 50yr	80	KLF802
	0.59 0.66 0.72					\neg								
	0.59 0.66 0.72	0.73	2.38			\neg			1421.9	1420.5	387.3	1 100vr	861	KLF861
	0.59	0.63		ω	6 2.25	7 0.008376	1422.07	1421.71	1421.72	1420.5	325.6	861 50yr	86	KLF861
	0.59	0.55	3.14		2.8	/ 0.015529	1422./	1422.22	1422.06	1421.02	38/.3	921 100Vr	92	KLF921
		0.52		3.94		1			1421.99	1421.02	325.6	921 50yr	92	KLF921
				П										
	1.04	0.52	3.03	3.31	1 1.91	2 0.007961	1423.12	П	1422.66	1421.47	387.3	963 100yr	96	KLF963
117.1 143.24	0.93	0.46			3 1.82	7 0.00833	1422.97		1422.55	1421.47	325.6	963 50yr	96	KLF963
								П						
185.56 195.07		0.61	2.1		6 1.52		1423.36		1423.13	1421.85	387.3	1002 100yr	100	KLF1002
161.68 190.24	0.88	0.55	2	2.33	1 1.47	2 0.00431	1423.22	1422.82	1423	1421.85	325.6	1002 50yr	100	KLF1002
					Ī									
146 5 195 77	0.77	0.54	2.63			٥		-1	1423.23	1422.17	387.3	1031 100vr	103	KLF1031
	0.69	0.48		3.01	1 1.96	8 0.0091	1423.48	1423.14	1423.14	1422.17	325.6	1031 50yr	103	KLF1031
	0.10	0.04							1460.00	1124.0	00,:0	TOOA	100	VE TOOL
167 78 191 37	0.48	0.84	1 63	2 64		3 0 006224		1423 43	1423 53	1422 5	387 3	1061 100vr	106	KI F1061
	0.43	0.77		Ī	7 2.18		1423.7	- 1	1423.45	1422.5	325.6	1061 50yr	106	KLF1061
				Ī		\neg		T				o root.	1	
123.7 179.43		0.63	2.59	3.41					1423.7	1422.79	387.3	1099 100vr	109	KLF1099
	0.47	0.57			3 2.77	8 0.014733	1424.08	1423.71	1423.62	1422.79	325.6	1099 50yr	109	KLF1099
147.02 182.85		0.7	1.93	Ī	2.3	/ 0.00//1/	1424.67	1424.28	1424.28	1423	387.3	1142 100yr	114	KLF1142
130./5 179.06	0.48	0.62		3.11		\top		Т	1424.19	1423	325.6	2 50yr	1142	KLF1142
						_		1						
		0.95			7 2.08	$\overline{}$	1424.92	1424.44	1424.67	1423.36	387.3	5 100yr	1185	KLF1185
160.85 176.14	0.59	0.88	1.49	2.31	1 1.94	9 0.004031	1424.79		1424.57	1423.36	325.6	50yr	1185	KLF1185
		0.72			4 3.07		1425.12		1424.58	1423.58	387.3	1214 100yr	121	KLF1214
135.2 166.28	0.66	0.78	2.08	2.8	8 2.32	7 0.006728	1424.97	1424.59	1424.67	1423.58	325.6	1214 50yr	121	KLF1214
		0.00						\neg	1 1000	1		100		The state of the s
		0.63				\neg		╗	1425.05	1424	3,87 3	1246 100vr	124	KI F1 246
125.36 172.3	0.46	0.56	1.83	2.96	1 2.08	2 0.008511	1425.32	1424.95	1424.94	1424	325.6	1246 50yr	124	KLF1246
(m)	(m2)	(m)	(m/s)	(m/s)	(m/s)	(m/m)	(m)	(m)	(m)	(m)	(m3/s) (
rea Top Width Froude # Chl	Hydr Depth R Flow Area	Hydr Depth L Hydr	Vel Right	Vel Chnl	Vel Left	E.G. Slope Vel Left	E.G. Elev	Crit W.S.	W.S. Elev	Min Ch El	Q Total	Profile	River Sta Profile	Node

0.63 297.38 221.42 0.34 0.68 321.25 225.84 0.36 0.14 145.66 234.61 1.01 0.17 162.99 235.8 1.01 0.11 65.16 113.76 2.23 0.09 76.38 126.46 2.15 0.17 111.47 139.18 1.14 0.21 122.91 142.37 1.18 0.63 130.27 155.98 1 0.7 145.86 160.53 1.02 0.53 122.61 153.11 1.04 0.6 140.4 158.85 1.03 0.71 171.57 173.82 0.68	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59 0.85 0.92 0.62	2.13 2.26 2.26 1.63	3.47	3 2.47 4 1.92	67 0.003774	1417.67	1417.2	1417.42	1415.5	359.4	217 50yr	KLF217
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98 145.86 160.53 122.61 153.11 140.4 158.85	1.19 1.27 0.6 0.67 0.35 0.35 0.54 0.59 0.85 0.92 0.62 0.69	2.13 2.26	3.47			Ī		T		250	747	717
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98 145.86 160.53 122.61 153.11 140.4 158.85	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59 0.85 0.92	2.13	3.47									
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98 145.86 160.53 122.61 153.11	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59 0.85 0.92	2.13				5 1418.12	1417.66	1417.61	1416	426.7	254 100yr	KLF254
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98 145.86 160.53	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59 0.85	2.41	3.33					П	1416	359.4	254 50yr	KLF254
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98 145.86 160.53	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59	2.41										
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37 130.27 155.98	1.19 1.27 0.6 0.67 0.3 0.35 0.54 0.59	١٧٧ ر	3.68		8.2 0.008437	1418.2	П	1417.74	1416	426.7	261 100yr	KLF261
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37	1.19 1.27 0.6 0.67 0.3 0.35 0.35	2.23		1 2.73	\neg	1418.05	1417.64	1417.64	1416	359.4	261 S0yr	KLF261
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18 122.91 142.37	1.19 1.27 0.6 0.67 0.3 0.35 0.35				\neg		ヿ					
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46 111.47 139.18	1.19 1.27 0.6 0.67 0.3 0.35	1.26	3.81						1416.5	426.7	301 100yr	KLF301
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46	1.19 1.27 0.6 0.67 0.3 0.35	1.06	3.53	8 2.37	3.4 0.01158	3 1418.4	1417.93	1417.83	1416.5	359.4	301 S0yr	LF301
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76 76.38 126.46	1.19 1.27 0.6 0.67 0.35				\neg		\equiv					
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8 65.16 113.76	1.19 1.27 0.6 0.67	1.99	6.11			5 1419.76		1418.01	1417	426.7	342 100yr	KLF342
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8	1.19 1.27 0.6 0.67	1.69		4 3.28).6 0.049064	1419.6	1418.4	1417.91	1417	359.4	342 50yr	KLF342
297.38 221.42 321.25 225.84 145.66 234.61 162.99 235.8	1.19 1.27 0.6 0.67											
297.38 221.42 321.25 225.84 145.66 234.61	1.19 1.27 0.6	1.03	2.74		0.010022	1420.7	1420.35	1420.35	1419	426.7	385 100yr	KLF385
297.38 221.42 321.25 225.84	1.19	0.89	2.59	6 2.39		7 1420.59	1420.27	1420.27	1419	359.4	385 50yr	KLF385
297.38 221.42 321.25 225.84	1.19											
297.38 221.42	1.19	0.79	1.48			1420.83			1419	426.7	434 100yr	KLF434
		0.71	1.34	7 1.09	71 0.000847	1420.71		1420.63	1419	359.4	434 50yr	KLF434
0.70	1.00	9			7	7777			1111	1000	TOOL	i.
31/ 60 217 11	1 06	0.84	1 48	1 06	\neg	1420.85		П		426.7	459 100vr	KI F459
0.7 291.38 212.62 0.33	ы	0.75	Ī		73 0.000838	1420.73		1420.65	1419	359.4	459 50yr	KLF459
1.017	1:10	1111	1:01		$\neg \Gamma$	7777		_	7777	720.7	2001	1000
	1 12	1 11	1 64		_	1420 9		1420 79	1419	426.7	500 100vr	KI F500
271.82 205.38	1.06	1.02	1.5	7 1.1	77 0.001017	1420.77			1419	359.4	500 50yr	KLF500
0.91 270.18 203.43 0.43	0.94	1.15	1.83	/ 1.18	95 0.0013/	1420.95		1420.81	1419	426./	535 TUUVI	KLF535
247.38 198.03	0.87	1.05			L	1420.82		Т	1419	359.4	535 50yr	KLF535
					\top			Γ				
246.62 188.21	1.01	1.44	2.07	9 1.39	0.001709	1421.02		1420.85	1419	426.7	571 100yr	KLF571
1.01 225.17 182.18 0.46	0.95	1.32	1.9	1 1.27	88 0.001571	1420.88		1420.73	1419	359.4	571 50yr	KLF571
717.61	0.89	T./6		1.40	0.002254	1421.1		1420.88	1419	425.7	TOON!	KLFOUX
T.03 7.7.7. 7.7.7. 0.53	0.83	7.07				1420.96		Т	1419	359.4	SOO SOOT	KLF6U8
10101	3				\neg			Т				
176.37 152.3	0.71	1.84	2.8	5 1.62		1421.27			1419.15	426.7	652 100yr	KLF652
0.79 158.95 146.69 0.68	0.65	1.7	2.6	8 1.48	11 0.003558	1421.11		1420.81	1419.15	359.4	652 50yr	KLF652
0.81 153.18 144.13 0.86	0.74	2.21			43 0.005822	1421.43	1420.91	1420.99	1419.5	426.7	681 100yr	KLF681
136.43 139.08	0.68	2.06	3.02	9 1.96	\Box	П	П	П		359.4	681 50yr	KLF681
1.32 101.23 134,03	0.74	14:7	2.00	1.04		7.0.1741		1421.20	7413.3	420.7	14004	VE / 10
(m2) (m)	(m)	(m) (m)	u) (s/m)	(m/s)	(m/m)	(m)	(m)	13	(m)	(m3/s)	710	E710
Flow Area	Hydr Depth L Hydr Depth R	gnt	Į	Vel Lett	E.G. Slope Vel Lett	E.G. EIEV	Crit W.S.	. FIEV	MIN CN EI	(C) (C)	KIVER STA PROTIE	Node

				000	20			0.000455				1502 6	20 1	1990 100	KI F1000
1.51	61.68	13.45	0.01	0	0.31	2.24	0.09	0.033232	1504.17	1503.99	1503.91	1503.6	30.1	1889 50yr	KLF1889
1.9/	47.00	71.03	O.H.	0.00											
1 .	17 66	11 80	0 13	0.09		3 67		0.048753		1506.07	1505.88	1505.41	39.1	1940 100vr	KLF1940
2.03	42.58	9.44	0.1	0.06	1.7		1.18		1506.4			1505.41	30.1	1940 50yr	KLF1940
1.43		17.18	0.08	80.0		2.44		0.02/2	1509.1	1508.9	1508.81	1508.41	39.1	ZULZ LUUYI	KLF 2U12
1.36	70.53	14.63	0.06	0.06	0.85		0.85	9				1508.41	30.1	2012 50yr	KLF2012
								_							
1.73		13.76		0.01		2.85	0.39	0.040564	1510.94	1510.67	1510.53	1510.02	39.1	2067 100yr	KLF2067
1.76	46.46	11.17				2.7		0.043797	1510.85	1510.6	1510.48	1510.02	30.1	2067 50yr	KLF2067
1.3	89.28	19.9	0.16	0.08				- 1	1513.04			1512.37	39.1	2139 100уг	KLF2139
1.25	83.73	16.74	0.14	0.06	1.3	2.06	0.77	0.021016	1512.96	1512.83	1512.78	1512.37	30.1	2139 50yr	KLF2139
5	1	20:03		0.00	0.00	L		0.000	10				9		
0 99	111 83	25 69	2	20.0	0.03			0.013687	1514.42	- 1	П	1514	39.1	2220 100vr	KLF2220
0.99	104.17	21.04		0.03		1.44	0.41	0.014591	1514.36	1514.26	1514.26	1514	30.1	2220 50уг	KLF2220
0.68	59.07T	33./3	CT.0	CT.O	17.0	1.5.1	0./1	2400000	T314.55	40.41CT	17.4.51	1014:01	33.1	1Å00T 7077	VII 2207
0.00		72.03	0.15	0 15	0.71		T	_	1517.00	151707	Т	15145	20.1	7797 100,-	KI E2287
	112 72	26 27	0 13	013	0.63	1 10	T	0.00534	1514 93	1514.8	1514 86	15145	30.1	7787 SOvr	KI F2287
0.95		24.44	0.1	0.1	0.76	1./1	0.76	0.011553	1515.48	1515.34	1515.34	1514.94	39.1	2331 100yr	KLF 2331
0.94	88.41	20.25	0.07	0.00	10.0			1	1313.41	Т	Т	174.94	50.1	IANC TCC7	VCL 7221
						İ			4141	1	1			777	
1.76	61.25	14.3	0.17	0.11	2.04	3.14	1.53	0.039825	1516.54	1516.25	1516.11	1515.76	39.1	2381 100yr	KLF2381
1.72	56.91	11.87	0.15	0.09	1.84	2.87	1.35		1516.44			1515.76	30.1	2381 50yr	KLF2381
1.5		15.94	0.17	0.15	1.7	2.93	1.57	0.027422	1518.06	1517.81	1517.69	1517.21	39.1	2426 100yr	KLF2426
1.49	57.94	13.06	0.14	0.13	1.51		1.4		1517.97	1517.75	1517.65	1517.21	30.1	2426 50yr	KLF2426
1.43	85.68	18.4	0.09	0.16	1.12	2.47	1.6	-	1520.01	1519.82	1519.75	1519.35	39.1	2499 100yr	KLF2499
1.39	80.39	15.37	0.07	0.13	0.96	2.25	1.42	0.026389	1519.93	1519.77	1519.71	1519.35	30.1	2499 50yr	KLF2499
1.53	65.32	14.81	0.12	0.11	1.33				1522.2	1521.86	1521.7	1521	39.1	2578 100yr	KLF2578
1.51	55.09	11.59	0.1	0.07	1.14	3.17	0.93	0.02619	1522.1	1521.79	1521.64	1521	30.1	2578 50yr	KLF2578
	10000		G i	9				_	1		1		i	1000	į
1 11	169 33	132 94	0.21	0.49		Ī		- 1	1416 69		П	1415	426.7	72 100vr	KI F72
1.1	162.78	118.28	0.19	0.41	1.16	3.28	1.93	0.010959	1416.54	1416.12	1416.03	1415	359.4	72 50yr	KLF72
0.54		100.#CI	o.i.a	0.77	1.02	3.43		\neg	70.7141	1	1	C:C1+1	420.7	142 10041	,tr142
	177 72	15/66	0.52	0 77	1 85			- 1		1	Т	1/15 5	7267	1/10 100	VI E1 / 2
0 93		136.48	0.46	0.71	1.69	3.12	2.26	0.007297	1417.17	1416.77	1416.77	1415.5	359 4	142 SOvr	1F142
0.92	176.88	157.82	0.66	0.75	2.1	3.3	2.29	0.006907	1417.69	1417.25	1417.27	1415.5	426.7	196 100yr	KLF196
0.91	172.66	140.13	0.58	0.69	1.92			1	1417.55	1417.16		1415.5	359.4	196 50yr	KLF196
	(m)	(m2)	(m)				(m/s)	-	(m)		-	(m)	(m3/s)		

10.1		10.71	0.10	7.1.0				-			- 1			1		
		17 9/		014						1482 35	- 1	1481.62	39.1	9 100vr	1169	KLF1169
1.04	38.3	14.34	0.12	0.09	0.9	2.19	8 0.76	8 0.012308	1482.48		1482.24	1481.62	30.1	9 50yr	1169	KLF1169
1.18	41.22	16.1		0.14	0./8		1.13	V9/CT0'0	1482.98	1482./3	1462.00	1482	1.50	JAOOT /ETT	ETT.	VELTT2/
1.1	20.00		0.00	0 1		, ,					П	1407	30.4	7 100	110	1 E1 107
	28 85	13 01	0.05	011	0.57		0.94	6 0.014404	1482.86	1482.65	1482.61	1482	30.1	1197 50vr	119	KLF1197
0.92		20.14	0.2	0.21	1.09	2.19	0 1.12	0.009076	1483.41	1483.19	1483.19	1482.51	39.1	TOOM	123	NLF1233
0.98	44.47	15.59		0.16		2.1					Т	1482.51	30.1	SOUVI	1233	KLF1233
								_		1		1,000 F1	202	TO.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1.11	51.41	18.02	0.11	0.15	0.91	2.31	7 1.15	6 0.014237	1483.86	1483.65	1483.6	1483	39.1	2 100yr	1272	KLF1272
1.12		14.63	0.07	0.12				$\overline{}$	Γ	Г	Ι.,	1483	30.1	1272 50yr	127	KLF1272
											П					
1.11	62.52	19.34	0.06	0.04			8 0.47	0		Г	L	1483.78	39.1	1312 100yr	131	KLF1312
1.05	59.04	16.65	0.04	0.02	0.5			7 0.0146	1484.37	1484.22		1483.78	30.1	1312 50yr	131.	KLF1312
								=7								
1.46	60.28	15.79	0.04	0.0	0.69	5 2.52		. 1			1485.08	1484.64	39.1	1357 100yr	135	KLF1357
1.47		12.99	0.02	0	0.38		0.11	1 0.030091	1485.31	1485.12		1484.64	30.1	1357 50yr	135	KLF1357
1.25		19.08	0.07	0.1		2.16						1485.89	39.1	1402 100yr	140	KLF1402
1.2	71.78	16.16	0.05	0.08	0.64		7 0.87	1 0.019687	1486.41	1486.26	1486.22	1485.89	30.1	1402 50yr	140.	KLF1402
1.37	78.82		0.05	0.08							П	1487.09	39.1	1455 100yr	145	KLF1455
1.36	74.56	15.08	0.03	0.06	0.52	1 2.04	7 0.84	3 0.026867	1487.63	1487.48	1487.42	1487.09	30.1	5 50yr	1455	KLF1455
														1		
1.53	64.93	16.32				2.4		_		1489.07		1488.62	39.1	1509 100yr	150	KLF1509
1.45	61.46	13.91				2.16	J,	8 0.030536	1489.18		1488.94	1488.62	30.1	1509 50yr	1509	LF1509
1.7	78.87	16.07		0.02		2.44	0.55					1491.16	39.1	1576 100yr	157	KLF1576
1.73	74.95	13.2		0		5 2.28	0.16	8 0.047143	1491.68	1491.5	1491.42	1491.16	30.1	1576 50yr	1576	KLF1576
	100	10:50				15		$\neg \tau$		11000	П	4.00.0	00:1	Tool	100	1.
1.51	62.02	15.73	0.09			2.6	7	\neg		1493.81	П	1493.3	39.1	1639 100vr	1630	KI F1639
1.42	58.13	13.48	0.07		0.94	2.31	J1	0.027746	1493.94	1493.75	1493.67	1493.3	30.1	1639 50yr	1639	KLF1639
1.51	10:00	72.21	0.01	0.00	0.02	3.22		0.040.0	14.00.41	1430.07	1400.01	1455,40	1.50	TOOA	1,0	VEL TAGE
_	AE 20	17 73	003	0.03		1	1	T	1	3		1/05/19	20 1	1100	170	1 E 1 701
1.94	42	10.08		0		2.99	7 0.22	1 0.05357	1496.31	1496	1495.86	1495.48	30.1	1701 50vr	170	KLF1701
1.46		16.33	0.03	0.05		2.42	0.81	8 0.028705	1498.48			1497.8	39.1	1756 100yr	175	KLF1756
1.39	60.54	14.06	0.01	0.04	0.23			1		1498.21	1498.14	1497.8	30.1	1756 50yr	175	KLF1756
											П					
2.03	73.09	14.03				2.79		4 0.063124	1501.84	1501.56	1501.44	1501.16	39.1	1837 100yr	183	KLF1837
2.07	68.86	11.39				2.64		6 0.069283	1501.76	1501.51	1501.4	1501.16	30.1	1837 50yr	183	KLF1837
	fung	funz)	ğuğ	fund	(c/m)	Virital	ichii)	Vinding	ing.	Vini	in it	(HI)	(1112/3)			
1 Cade # CI	AAIOCII	Vica	n ocpania	י הכלינו ב	Bill	(m/c)	ACI FOLL	והיטי זוסטב אבו רבור	ריטי דופע	VV . J.	י, בוכע	(ש)			MACI DIG LIGHT	4000

1.33		14.34	67.0	0.24	10.1	Ī	D. T. O	T 0.019220	1400.11	1407.01	1407.05	00.70tT	35.1	TOOL	704	10407
	05.00							-		T	Τ	146700	100	100		717/00
1 2		11.91	0.15	0.2	1.32	Ĭ	1.6	8 0.019341	1467.98	1467.72	1467.62	1467.08	30.1	2 50yr	482	KLF482
											П					
1.32			0.09	0.15						1468.74		1468	39.1	1 100yr	531	KLF531
1.27	31.18	11.75	0.06	0.11	0.68	2.64	5 1.06	9 0.018545	1468.9	1468.64	1468.55	1468	30.1	1 50yr	531	KLF531
1.46			0.03	0.08	0.49		3 1					1469	39.1	572 100yr	57	KLF572
1.46	32.26	11.06		0.05		2.74	7 0.73	0.026597	1469.81	1469.54	1469.43	1469	30.1	2 50yr	572	KLF572
											- 1					
	35.69	15.84	0.02	0.06	0.34		4 0.62	6 0.014964	1470.96	1470.7	1470.65	1469.97	39.1	5 100yr	625	KLF625
1.1		13.59		0.03								1469.97	30.1	5 50yr	62	KLF625
								_								
1.68	34.37	12.29		0.03		3.19	1 0.54	2 0.035001	1472.12		1471.6	1471.03	39.1	675 100yr	67	KLF675
1.68	32.56	10.2				2.95	9	8 0.036869	1471.98	1471.68	1471.54	1471.03	30.1	'5 50yr	675	KLF675
1.29			0.13	0.13	1.17		8 1.12		1473.39		1472.97	1472.33	39.1	726 100yr	72	KLF726
1.22	30.37	11.95	0.1	0.1	0.94	2.6	6 0.91	4 0.017066	1473.24	1472.98	1472.9	1472.33	30.1	6 50yr	726	KLF726
1.52		11.95	0.11	0.18	1.17	3.47	5 1.7	8 0.025035	1474.8	1474.4	1474.21	1473.5	39,1	1 100yr	791	KLF791
1.52	25.95		0.07	0.14	0.88	3.21	5 1.45	4 0.026565	1474.64	1474.29	1474.13	1473.5	30.1	1 50yr	791	KLF791
1.25	32.96	14.83				2.64	9	8 0.018159	1475.68	1475.4	1475.33	1474.65	39.1	831 100yr	83	KLF831
1.24		12.33				2.44	5	6 0.018515	1475.56	1475.32	1475.25	1474.65	30.1	831 50yr	83	KLF831
1.44	(4)	13.31				2.94	9	8 0.024609	1476.38	1476.06	1475.94	1475.4	39.1	863 100yr	86	KLF863
1.39		11.29				2.67	6	4 0.023776	1476.24	1475.97	1475.87	1475.4	30.1	863 50yr	86	KLF863
1.47	27.59	12	0.14	0.14	1.36	3.46	7 1.36	7 0.023317	1477.37			1476	39.1	902 100yr	90	KLF902
1.42	25.44	10.06	0.1	0.1	1.1	3.11	8 1.1	9 0.022808	1477.19	1476.85	1476.7	1476	30.1	902 50yr	90	KLF902
								\neg			П					
1.47		11.84	0.11	0.11		3.42				- 1	П	1477	39.1	943 100yr	94	KLF943
1.45	23.83	9.82	0.07	0.07	0.83		3 0.85	3 0.023783	1478.13	1477.78	1477.63	1477	30.1	943 50yr	94	KLF943
1.35		13.06	0.08	0.16	0.86	3.1	8 1.35		1479.47		7	1478.22	39.1	997 100yr	99	KLF997
1.32	26.77		0.04	0.12	0.56			1 0.019676		1479.01	1478.9	1478.22	30.1	997 50yr	99	KLF997
											П					
1.44	32.6	13.31	0	0.13	0.08	3	9 1.35					1479.5	39.1	1049 100yr	104	KLF1049
1.44	29.94	10.87		0.09		2.81	8 1.09	7 0.025018	1480.47	1480.18	1480.07	1479.5	30.1	1049 50yr	104	KLF1049
1.1	39.56	ZU./1		0.03		2.3	0.42	3 0.014129	1481.43	1481.19	1481.16	1480.5	39.1	1094 100yr	109	KLF1094
1.08	36.95	14.29								1	Т	1480.5	30.1	1094 50yr	109	KLF1094
								1		1	1					
1.28	35.77	14.75	0.06	0.02	0.72	2.67	5 0.3	9 0.018895	1481.99	1481.71	1481.62	1481	39.1	1127 100yr	112	KLF1127
							(m/s)	(m/m)	(m)	Ш		(m)				
TOGGC II CITE	I OD ANIOCI	1 10 80 71 00	Luyur Deptilia	Hydr Depth L	Vel xignt	Vel Citi	L.G. Stope Vel Lett	L.G. Stope	E.G. Elev	CIIL W.S.	W.S. Elev	IVIII CII EI	ת וסופו	ואיזעכו כונם די ניווכ	INVESTIGATION	INOGE

1 51	ΛΕ CΛ	רר בר	0.3	0.27	2.25		5 2.08	4 0.022525	1492.04	1491.54	1491.32	1490.5	81.3	3664 100yr	HI F3664
1.48	42.46	19.16	0.25	0.22	2	3.65	7 1.82	4 0.022807	1491.84	1491.42	1491.23	1490.5	62.5	3664 50yr	HLF3664
1.56	48.15	23.24	0.14	0.33	1.44			6 0.025062	1493.46	1492.99	1492.78	1492	81.3	3724 100yr	HLF3724
1.51	45.03	19.48	0.1	0.29		3.54	2.28	1		1	Т	1492	62.5	3724 50yr	HLF3724
											Т				
1.4	40.83	23.8	0.44	0.4						1494.09		1492.5	81.3	3779 100yr	HLF3779
1.38	36.69	19.29	0.37	0.34	2.24	4.2	4 2.13	2 0.017064	1494.42	1493.94	1493.72	1492.5	62.5	3779 50yr	HLF3779
1.59	49.45	24.12	0.44	0.44	3.07	4.11	3.06	3 0.025515	1495.63	1495.21	7	1494.31	81.3	3828 100yr	HLF3828
1.6	46.15	19.69	0.38	0.38	2.87	3.84	2.88	7 0.027033	1495.47		1494.93	1494.31	62.5	3828 50yr	HLF3828
1.31	57.74	28.11	0.35	0.28	2.19	3.24	7 1.89	1 0.017607		1496.46	- 1	1495.62	81.3	3883 100yr	HLF3883
1.25	55.26	23.94	0.3	0.24	1.93				1496.65		1496.27	1495.62	62.5	3883 50yr	HLF3883
1./	41.31	20.73		0.22		4.2	7.17	2 0.030027	1496.22	1497.04	1497.57	1490.5	C.TO	JAOOT OOAL	חברסשיים
1.07	12.70	2C OC		0.10		Ī		-1	Ī	Т	Т	1406 6	01.0	2010 1000	II EDONO
	37 74	16 97		017		۵	1 8	0 030231	1498.07	1497 5	1497 27	1496 5	62.5	3940 50vr	HI 53940
1.78	59.98	23.08	0.21	0.26	2.19	3.89	2.58	4 0.035606	1499.64	1499.16	1498.95	1498.41	81.3	3984 100yr	HLF3984
1.78	57.19	18.98	0.16	0.22				8 0.037621		1499.06	П	1498.41	62.5	3984 50yr	HLF3984
											П				
1.28	76.96	31.25	0.1	0.25	0.96							1500.16	81.3	4038 100yr	HLF4038
1.25	74.26	26.37	0.06	0.21	0.72	2.47	1.63	0.018755	1500.92	1500.69	1500.62	1500.16	62.5	4038 50yr	HLF4038
	0.00	11.10	0.02	0:50			1.0		17000	14004	\neg	1,000,1	00.1	1004	Î
	63.05	21 18	0.03	0.35	0.25	1 86	T	- 1			Т	1458 71	30 1	80 100vr	K) E87
0.98	53.04	17.05		0.35		I	1.85	7 0.012669	1459.57	1459.42	1459.41	1458.71	30.1	82 50vr	KLF82
		100		0.0		١					П			100	i
1.31	45.14	15.8	0.07	0.37	0.84			0.020652		1		1460	39.1	156 100vr	KLF156
1.28	41.08	13.04	0.05	0.34	0.63	2.28	2.35		1460.77	1460.56	1460.5	1460	30.1	156 50yr	KLF156
1.31	44.01	15.8/	0.21	0.39	1.66	2./1	2.52	0.019943	1462.44	1462.2	1462.11	1461.62	39.1	235 100yr	KLF235
1.26	41.43	13.33	0.1/	0.36	1.44		T	_		1462.12		1461.62	30.1	235 50yr	KLF235
						Ì		1							
1.71	36.61	12.4	0.07	0.35	1.07	3.28	3.13	0.035754	1464.01	1463.65	1463.49	1462.98	39.1	293 100yr	KLF293
1.67	34.14	10.31	0.04	0.31	0.75	2.95	5 2.92	0.036336	1463.87	1463.57	1463.43	1462.98	30.1	293 50үг	KLF293
								\neg		П	П				
1.26	37.66	15.28	0.29	0.24	1.9	2.9		=			П	1464.5	39.1	358 100yr	KLF358
1.23	35.7	12.71	0.25	0.19	1.73	2.73	1.46	0.016965	1465.36	1465.12	1465.04	1464.5	30.1	358 50yr	KLF358
	0	ļ.		0.00								F-100:07		100	1
1.4	37.14	14.14		0.08			0.94	0.023393		1466.02	-1	1465 37	39.1	400 100vr	K) E400
1.36	35.06	11.91		0.05		2.54			1466.18		1465.85	1465.37	30.1	400 50yr	KLF400
1.41	36.33	13.89	0.18	0.24	1.6	3.15	1.94	0.022153	1467.14	1	1	1466.08	39.1	435 100yr	KLF435
1.38	34.34	11.6	0.14	0.21	1.36		1.73		1467	1466.73	1466.62	1466.08	30.1	435 50үг	KLF435
									(m)	Ш	- 1				
	100 0010001	1000	היאמו הכלינו י	nyar bepui t	ACI MRITE	AGI CITIE	עפו רפו <i>ר</i>	E.G. Slope	L.G. LIGY	CITC VV.J.	AA.O. LICA	IAILL CLI EL	מוסנטו	ייואכו הנס ו והווכ	14000

Node	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope Vel Left	Vel Left	Vel Chnl	Vel Right	Hydr Depth L	Hydr Depth R	Flow Area	Top Width	Froude # Chl
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m/s)	(m/s)	(m)	(m)	(m2)	(m)	
HLF3604	3604 50yr	50yr	62.5	1489.51	1490.18	1490.28	1490.59	0.017477	2.37	3.09	1.33	0.4	0.17	22.87	50.39	
HLF3604	3604 100yr	100yr	81.3		1490.26	П	П			3.44						
HLF3547	3547 50yr	50yr	62.5		1489.06	1489.17		0.02207	1.75	2.87	1.11		0.11	23.28	63.63	
HLF3547	3547	100уг	81.3	1488.56			1489.6	1_1				0.25				
HLF3484	3484 50yr	50yr	62.5	1487.14	1487.7	1487.81	1488.1	0.020748	2.16	2.94	1.1	0.3	0.11	22.94	57.59	
HLF3484	3484 100yr	100уг	81.3			П			2.37	3.23	1.34					
HLF3430	3430 50yr	50yr	62.5	1485.97	1486.64	1486.76	1487.07	0.017854	2.31	3.22	1.68	0.37	0.23	22.6	50.65	
HLF3430	3430 100yr	100yr	81.3					-	2.48	3.51	1.9					
HLF3380	3380 50yr	50yr	62.5		1485.66	1485.79	1486.12	2 0.020108	1.99		0.89	0.27	0.08	21.58	49.02	
HLF3380	3380 100yr	100yr	81.3	1484.95		П				3.39						
HLF3322	3322 50yr	50yr	62.5	1483	1484.08	1484.32	1484.82	0.023879	0.93			0.08		16.56	27.97	
HLF3322	3322	3322 100yr	81.3	1483	1484.21	1484.48		0.022406	1.32	4.05	0.57	0.14	0.04		33.79	
HLF3254	3254 50yr	50yr	62.5	1482.29	1483.21	1483.29	1483.6	5 0.011993	1.64		1.15	0.3		24.44	49.8	
HLF3254	3254 100yr	100уг	81.3							3.35	1.4		0.22		(8	
HLF3189	3189 50yr	50yr	62.5	1481.54	1482.05	1482.17	1482.48	8 0.027047	2.43	3.07	0.97	0.3	0.07	22.01	61.61	
HLF3189	3189	3189 100yr	81.3		П	Т	Π		П							
HLF3127	3127 50yr	50yr	62.5	1480.5	1481.09	1481.12	1481.36	6 0.012002	1.51		1.14	0.26	0.18	28.29	65.87	
HLF3127	3127	3127 100yr	81.3		П	П	П			2.69						
HLF3074	3074 50yr	50yr	62.5	1480	1480.52	1480.51	1480.73	3 0.009864	1.25		0.16			31.38	69.66	
HLF3074	3074	3074 100yr	81.3		П					2.32		0.27	7 0.05			
HI F3028	3028 50vr	50vr	62 5		1480 03	1480 03		5 0 010428			1 43		3 n 27	18 00		
HLF3028	3028	3028 100vr	81.3	1479.5	П	П	T		1.61	2.43						
		TOO.1.	0.10													
HLF2973	2973 50yr	50yr	62.5	1478.82	1479.48	1479.43	1479.67	7 0.007468	0.76	1.99	1.33	0.14	0.31	32.91	65.18	
HLF2973	2973	2973 100yr	81.3	1478.82	1479.59	1479.53	1479.81	0.006904	0.92	2.14	1.47	0.19	0.39	40	67.68	
HLF2920	2920 50yr	50yr	62.5	1478	1478.95	1478.95	1479.25	5 0.008114	1.11	2.48	1.1	0.22	0.22	27.46	49.3	
HLF2920	2920	2920 100yr	81.3					$\overline{}$	П	2.66					(5)	
HLF2857	2857 50yr	50yr	62.5	1477.4	1478.21	1478.27	1478.6	6 0.012887	0.83		1.2	0.1	0.18		42.02	
HLF2857	2857	2857 100yr	81.3	1477.4	1478.31	1478.4	1478.78		1.09	3.09	1.43)		27.5		
HLF2795	2795 50vr	77.1	2.22	1000				000000								

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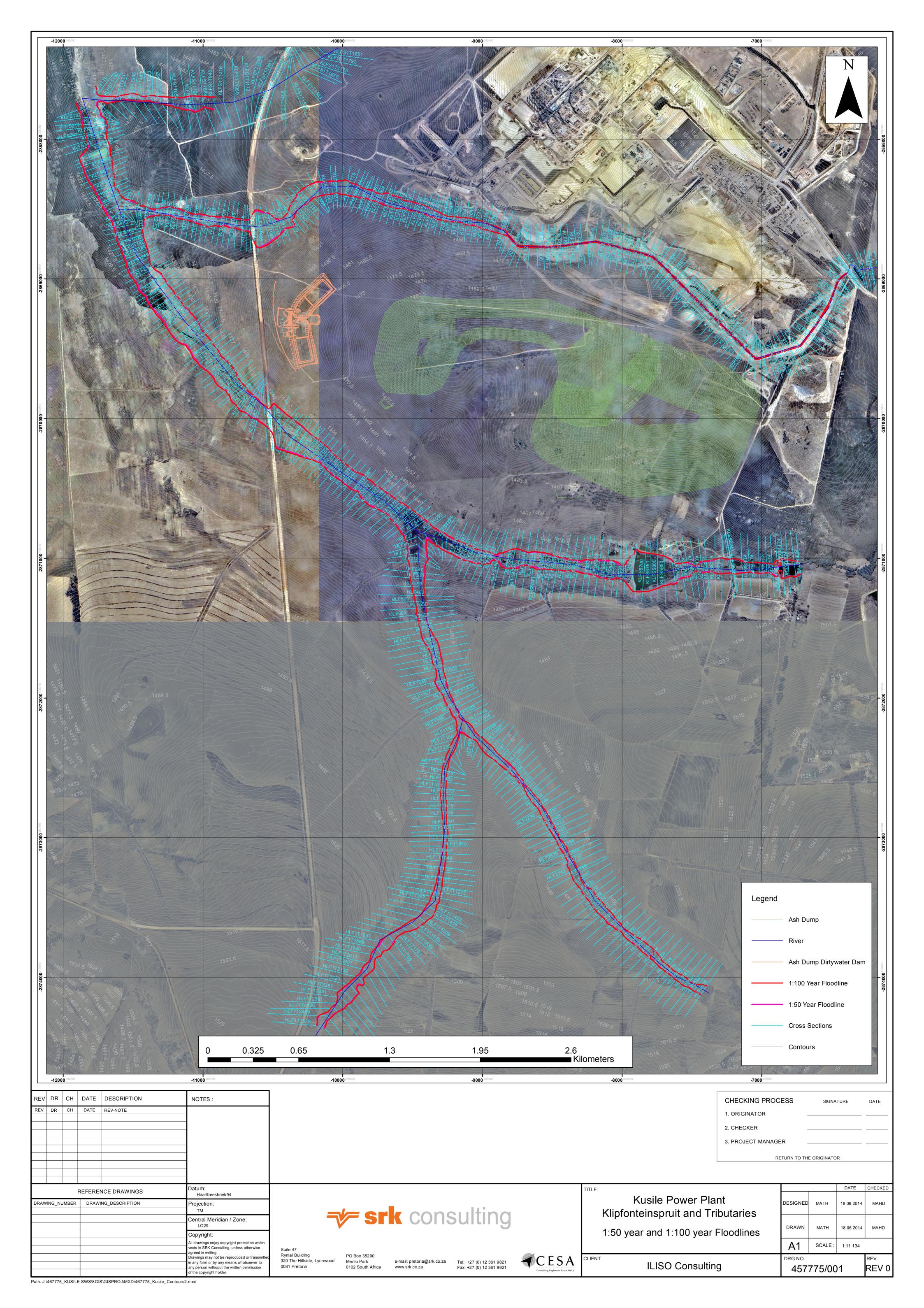
	11 63		0.33	0.2	1.9		2 1.37	2 0.014522	1470.2	1469.8	1469.68	1467.5	81.3	2153 100yr	2153	HLF2153
1.23	41.38	21.36	0.25	0.14	1.66	3.13		Т	L	L	Г		62.5	50yr	2153	HLF 2153
								\top		Т					2	
0.93	48.45	33.06	0.44	0.54	1.72		6 1.98	3 0.00796	1470.73	1470.39	1470.37	1468.5	81.3	2202 100yr	2202	HLF2202
0.89	46.12	28.07	0.37	0.47	1.48	2.77				1470.26	П	1468.5	62.5	2202 50yr	2202	HLF2202
1.39	34.85		0.14	0.29	1.19							1469	81.3	2248 100yr	2248	HLF2248
1.41	31.37	17.73	0.07	0.23	0.81	3.73	3 1.75	7 0.020123	1471.17	1470.69	1470.48	1469	62.5	50yr	2248 50yr	HLF2248
9	10:10		0.00	9	!					П						
0 92	45 18		0.35	0.42	1.45	2.83	İ	6 0.00753	1471.96		ı	1470.51	81.3	2296 100vr	2296	HLF2296
0.93	42.07	26.18	0.27	0.34	1.26		2 1.47			1471.46	1471.46	1470.51	62.5	2296 50yr	2296	HLF2296
								- 1	ĺ	П	\neg					
0.97	45	31.51		0.12		2.6			1472.31		1471.96	1471	81.3	2337 100yr	2337	HLF2337
0.0	42.76	26.85		0.07			1 0.52	3 0.008771	1472.13	1471.82	1471.86	1471	62.5	50yr	2337 50yr	HLF2337
								- 1	1	T	\neg					
0.82	39.81		0.2	0.36	0.86			- 11	1472.67			1470.5	81.3	2388 100yr	2388	HLF2388
0.77	36.92	27.99	0.14	0.29	0.64	2.36	8 1.07	8 0.005338		1472.09	1472.21	1470.5	62.5	50yr	2388 50yr	HLF2388
1.05	37.29		0.15	0.17	0.97					1472.72		1471	81.3	100yr	2432	HLF2432
0.98	34.48	23.17	0.09	0.12	0.66	2.76	9 0.77	2 0.00929	1472.92	1472.55	1472.54	1471	62.5	50yr	2432 50yr	HLF2432
											٦					
0.98	33.59	27.18	0.14	0.23	0.84	3.13	6 1.15	8 0.008506	1473.58			1471.5	81.3	2480 100уг	2480	HLF2480
0.97	29.76		0.07	0.15	0.51		1 0.9			1472.94	1472.94	1471.5	62.5	50уг	2480 50уг	HLF2480
											П					
1.36	32.74		0.07		0.78	3.72	4					1472	81.3	2527 100yr	2527	HLF2527
1.	27.56	17.84	0		0.06	3.5	ы	4 0.019925	1473.94	1473.49	1473.31	1472	62.5	50yr	2527 50yr	HLF2527
								\neg			П					
0.86	44.41	32.24	0.36	0.36	1.36	2.99	3 1.35	7 0.006443	1474.77	1474.37	1474.37	1472	81.3	2584 100yr	2584	HLF2584
0.85	39.55	25.93	0.27	0.29	1.14		2 1.17	7 0.006592	1474.57	1474.22	1474.22	1472	62.5	50yr	2584 50yr	HLF2584
											П					
1.37	28.29	21.09	0.05	0.02	0.62		3 0.34			1474.76	7	1473	81.3	2626 100vr	2626	HLF2626
1.31	24.83	17.94				3.48	7	3 0.017157	1475.03	1474.57	1474.42	1473	62.5	50yr	2626 50yr	HLF2626
1.59	29.28	18.59		0.11		Ī	3 1.22			1475.43	Т	1473.5	81.3	2664 100yr	2664	HLF2664
1.66	19.12	14.05				4.45		6 0.027493	1475.96	1 1	1474.95	1473.5	62.5	50yr	2664 50yr	HLF2664
1.01	56.68	33./1	0.51	0.49	/1.2	2.53	2.07	4 0.010365	14/6.94	14/6.64	14/6.64	14/6	81.3	2/10 100γr	2/10	HLF2/10
	20.00	20.00	0.11	0 10	2 2 2					Т	T	1		Joy-	27.10	12,10
101	55 34	28.06	0 44	0.43	2.03		1 94	8 0 010964	1476.8	1476 54	1476 54	1476	62 5	5Ovr	2710	HI E2710
1.12	55.75	30.7	0.05	0.02	0.5		9 0.27	4 0.013499	1477.44	1477.13	1477.08	1476.34	81.3	2762 100yr	2762	HLF2762
1.14	52.87	25.27				2.47	7	9 0.014737	1477.29	1477.02	1476.98	1476.34	62.5	50yr	2762 50yr	HLF2762
1.17	58.86	30.56		0.27		2.73	7 1.68	9 0.014697	1477.9	1477.6	1477.53	1476.86	81.3	100yr	2795	HLF2795
	(m)		(m)			(m/s)	(m/s)	$\overline{}$	(m)	(m)	(m)		(m3/s)			
					0					917			1	l		

0		10.00				6 55				_		1457	130.8	1385 100vr	1385	HI E139E
2.95	29.67	15.23				6.61		0.096427	1459.89	1458.22	1457.66	1457	100.7	1385 50yr	1385	HLF1385
1.06	92.86	37.81		0.28		2.62		0.011562	1460.2	1459.97		1459	81.3	1449 100yr	1449	HLF1449
1.01	85.96	31.68		0.24		2.39	1.33				1459.85	1459	62.5	1449 50yr	1449	HLF1449
								\neg								
1.01	74.13	37.03		0.45		2.41		0.01075		1460.54		1459.83	81.3	1504 100yr	1504	HLF1504
	71.18	30.84		0.38		2.25	1.84		1460.67		1460.45	1459.83	62.5	1504 50yr	1504	HLF1504
1.24	49./3	26.9	0.08	0.27	0./8	3.31	1./1	0.015041	1461.43	1461.05	1460.91	1460	0L.3	TOOL	1000	חלגדססס
, -	40.72	32.2	0.00	11.0	17.0	2 22	T	_		Т	Ţ	1460	01 0	100	1553	HI E1EE3
1 23	28 77	77	0.03	0 22	0 41	305	153	0.015649	1461.25	1460.97	1460.8	1460	62.5	1553 50vr	1553	HLF1553
1.55	59.93	25.61		0.31		3.53	2.4/	0.026226	1462.4	1462.01	1461.84	1461.19	81.3	1604 100yr	1604	HLF16U4
1.52	57.36	21.37		0.26		3.27		_	Ī.,	Т	1461.77	1461.19	62.5	1604 50yr	1604	HLF1604
								Т		Т						
1.01	68.96	35.83		0.5		2.32	2.22	$\overline{}$		14	1463.09	1462.5	81.3	100yr	1661	HLF1661
	66.58	29.81		0.44		2.14		Т		Г	П	1462.5	62.5	1661 50yr	1661	HLF1661
									Γ							
0.96	59.72	35.28		0.46		2.4	1.93	0.009457	1464.05	1463.76	1463.78	1463	81.3	1731 100yr	1731	HLF1731
0.91	57.47	30.23		0.41		2.15	1.73	0.008892	1463.91	1463.65	1463.69	1463	62.5	1731 50yr	1731	HLF1731
1.17	51.18	28.67	0.21	0.38	1.36	3.21	2.01	0.013381	1464.64	1464.28		1463	81.3	1781 100yr	1781	HLF1781
1.21	47.97	22.94	0.14	0.29	1.1	3.04	1.81	0.014993	1464.49	1464.17	1464.06	1463	62.5	1781 50yr	1781	HLF1781
								\neg								
1.03	50.16	30.96	0.43	0.26	1.87	2.99		\neg	14		1464.77	1463.5	81.3	100yr	1827	HLF1827
0.92	47.92	27.39	0.38	0.21	1.59	2.57	1.08	0.008203	1465	1464.71	1464.7	1463.5	62.5	1827 50yr	1827	HLF1827
1.16	42.56	27.08	0.06	0.4	0.56	3.29					1465.31	1464	81.3	1881 100уг	1881	HLF1881
1.22	37.34	21.27		0.33		3.17	1.95	0.015056	1465.63	1465.27	1465.16	1464	62.5	1881 50yr	1881	HLF1881
1.1	44.17	28.49		0.27		3.01			1466.31	ᅵ	1465.86	1464.5	81.3	1922 100yr	1922	HLF1922
0.97	41.87	25.5		0.24		2.57	1.23	0.009294		1465.8	1465.8	1464.5	62.5	1922 50yr	1922	HLF1922
1.61	25.15	17.81	0.05	0.13	0.68	4.68		\neg			1466.09	1464.5	81.3	1964 100yr	1964	HLF1964
1.75	19.15	13.37		0.09		4.7	1.17	0.03094	1467.01	1466.27	1465.89	1464.5	62.5	1964 50yr	1964	HLF1964
1,01	71.72	2:03	0.50	0.24	1.55	3.55	1.13	0.00000	1407.00	1407.57	1407.10	##.CO#1	0.10	TOOT TOO	2012	ULL ZOT Z
4	24 72	2.10	0.26	0.20	1 55	0 00	Ī		1467.00	1467 27	T	1465 44	01.0	100	2012	E 2012
0.81	34 13	24.3	0.35	0 23	13	س در	0 0	0 005354	1467 59	1467 18	1467 15	1465 44	222	2012 SOvr	7017	HI E2012
1.36	12.94	16.75				4.85			1468.58	1467.86		1465.5	81.3	2060 100yr	2060	HLF2060
1.48	10.54	12.4				5.04		0.020502	1468.3		1467.01	1465.5	62.5	2060 50yr	2060	HLF2060
1.34	40.56	23.44		0.26		3.92	1.8	0.017798	1469.51	1468.99	1468.79	1466.5	81.3	2111 100yr	2111	HLF2111
1.29	37.68	19.08		0.16		3.63	1.3	0.016934	1469.32	1468.88	1468.68	1466.5	62.5	2111 50yr	2111	HLF2111
	(m)					(m/s) ((m/m)	(m)	(m)	(m)	(m)				
	. of a same	11044 71100	The Department	וואמו הבטנוו ב	ACLINBILL	ACI CITIE		ב.ט. טוטסכ שכו בכונ	ר.ט. רוכי	C116 88.0.	44.0. LICA	TALLED CITE	ע וסומו			14000

Node	River Sta Profile	yfile		Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope Vel Left		크	ght	Hydr Depth L	Hydr Depth R	Flow Area	Top Width
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m/s) ((m/s)	(m)	(m)	(m2)	3
HLF1348	1348 50yr	7	100.7	1456	1458.14	1458.3	1458.77		1.32	3.8	1.43	0.33		33.77	7
HLF1348	1348 100yr	ΟVΓ	130.8	1456				0.006097		3.92	1.66	0.46			3
2	220		3	1 100	T					<u>د</u> ن	1 00				
חברבטבט	1310 100		1200.7	1455.05		1450.05		Τ.	1.00	4 5	1.30	0.43	0.2.0	25.05	+
HLF1310	1310 100yr) Vr	130.8	1455.69	1457.76		1458.67	0.01049	1.93	4.54	1.67	0.43			100
HLF1270	1270 50yr	1	100.7	1455.5	1457.43	1457.59	1458	0.006964	1.69	3.84	1.69	0.48	0.48	35.78	<u>س</u>
HLF1270	1270 100yr	Y	130.8	1455.5		П	14		1.84	4.24	1.99	0.51			+
					П	П		-							
HLF1234	1234 50yr	ır	100.7	1455.5	1457.33	1457.34	1457.74	0.005155	1.33	3.29	1.71	0.42	0.61	41.4	4
HLF1234	1234 100yr	УГ	130.8	1455.5	П				1.51	3.49	1.92	0.51			Ψ.
					П										П
HLF1196	1196 50уг	/٢	100.7	1455.5	1456.68	1456.89	1457.4	0.015463	1.11	4.25	2.41	0.14	0.44	1 29.6	ď
HLF1196	1196 100yr	Эγг	130.8	1455.5		1457.06	1457.62		1.5	4.56	2.74	0.22		35.99	9
					П										
HLF1157	1157 50yr	/٢	100.7	1455	1456.24	1456.4	1456.83	0.012118		3.64	1.56		0.28	33.31	1
HLF1157	1157 100yr	γr	130.8	1455	П					3.98	1.97		0.37		8
1 61433	1111	;	100.7	1464	┰					0 1	1 63				4
HI E1122	1177 100		130.0	1/5/15	Т		T	\neg		2 12 1	1 52	0.04			
1101	1004	1	100.0	11011	1.00.10	1100:11	1470:54	0.000700	0.70	10.1	7.0.1	0.21		00.04	1
HLF1086	1086 50yr	, T	100.7	1454.5	1456.08	1455.66	1456.21	0.001715	0.66	1.69	1.01	0.33		8 68.79	٥
HLF1086	1086 100yr	θγr	130.8	1454.5	П	П			0.81	1.84	1.15	0.46	0.76		
					П										T
HLF1050	1050 50yr	1	100./	1454.5	Т	Г	1456.08	-	1.15	2.85	1.54	0.26	0.41		100
HLF1050	1050 100yr	Ογr	130.8	1454.5	1455.86	1455.86		0.006621	1.36	3.06	1.75	0.39		2 49.11	1
HLF1005	1005 50yr	<u></u>	100.7	1454	1455.05	1455.19	1455.62	0.013649	1.68	3.49	1.68	0.28		31.76	S
HLF1005	1005 100yr	Ογr	130.8	1454	1455.18	1455.35		0.013388	1.95	3.8	1.97	0.36	0.37		7
חרגאטי	JANC / CE		TOO./	1455.72				0.012838		19.7	T.U3	U.L			ľ
HLF957	957 100yr	Эyr	130.8	1453.72	1454.62		1455.13	0.014537	1.48	3.23	1.36	0.22	0.2	2 42.26	6
HLF910	910 50yr	7	100.7	1452.5	1453.8	1453.91	1454.28	0.014807		3.23	1.93		0.33	34.13	ω
HLF910	910 100yr	Эүг	130.8	1452.5	[П	1 1	0.47	3.44	2.14	0.04			0
11 E860	860 50		100.7	1 /15	Т	Т			1 04	20 0	1	0			
111 000	1400 000	1	T00./	7C+T	Τ	Т	T	1	1.04	2.60	T.47	0.56			1
HLF860	860 100yr	Оyг	130.8	1452	1453.63	1453.63	1453.98	0.006883	2.04	3.12	1.66	0.63	0.47	54.33	_ ω
HLF807	807 50yr	7	100.7	1451.5	1452.97	1453.06	1453.34	0.012078	2.23	3.44	1.87	0.4	0.37	7 41.46	S
HLF807	807 100yr	ργ	130.8	1451.5	1453.06	1453.16	1453.49		2.49	3.74	2.15	0.54			9
111111111111111111111111111111111111111	77		100.1		Т										
HLF771	771 50vr	į	1007	1451 5	1452 57	1452 62		1452.89 0.012424	2.21	3.09	2 18	0.46	0.45	41 54	-

200				0.29	1 17		1 5/	0 011778	1445 87	1445.62	1445.58	1445	130.8	37 100vr	37	HI F37
0.97	183.29	56.16	0.14	0.25	0.93	2.12	9 1.36	0.010669	1445.73	1445.56	1445.53	1445	100.7	37 50yr	37	HLF37
											П					
0.89			0.29	0.27	1.32	2.23				1446.16		1445.5	130.8	95 100yr	95	HLF95
3.0	160.85	58.46		0.21	1.21		8 1.07	0.008278	1446.27	1446.08	1446.08	1445.5	100.7	95 50yr	95	HLF95
	10101		9					- 1			П					
0.57	162 84		0.46	0.32	1	1.58	0.86	0.003068	1446.66	1446.35	\neg	1445.5	130.8	157 100vr	157	HLF157
0.54	156.52	81.5	0.4	0.26	0.97					1446.27	1446.47	1445.5	100.7	50yr	157	HLF157
1.2	80.80I	1.05	0.31	0.37	1.0		2.00	0.013033	/U./##I	1440.70	1440.04	1440.0	130.0	TOOM.	017	1111 710
	I		0 0 0	75.0	10			т	1447 07	1446 76	T	1445 5	120.0	100,00	218	HI E218
1.16	102.95	41.73	0.25	0.32	1.52		7 1.87	1 0.013267	1446.94	1446.67	1446.56	1445.5	100.7	218 50yr	218	HLF218
0.93	90.33		0.57	0.43	1.51		1./3	0.007		1447.50		1440;	100.0	TOOM	100	10, 657
000		77 05		0.40	1 61	2 7 7			1/17 00	1447 50	П	1446 5	120 0	1000	707	HI E207
0.0	91.77		0.3	0.38	1.33		8 1.54	0.007828		1447.46	1447.46	1446.5	100.7	297 50vr	297	HLF297
1.09	90.19		0.23		1.39	2.58		0.012586	1448.3	1448	1447.94	144/	130.8	339 TOOM	339	ПС1339
		12.07	0.23		1 20	3 6		Т			Т	1447	1000	3	220	17330
1 07	84 29		0.18		1.19	2.46	7	0.012506	1448.15	1447.88	1447.85	1447	100.7	339 50vr	339	HLF339
1.07	87.03	50.85				2.57	51			1448.74	1448.71	1447.57	130.8	399 100yr	399	HLF399
1.05	84.92	42.9				2.35	7	0.012377	1448.9	1448.63	Π	1447.57	100.7	399 50yr	399	HLF399
											П					
1.04	80.33		0.13	0.07	0.91		0.57	0.011083	1449.78	1449.45	1449.43	1448.5	130.8	462 100yr	462	HLF462
1.04	78.5	41.81	0.08	0.02	0.68	2.42	1 0.22	0.01181	1449.62	1449.34	1449.32	1448.5	100.7	462 50yr	462	HLF462
	77.29	51.13				2.56	7		1450.2	1449.87	1449.87	1448.5	130.8	501 100yr	501	HLF501
1.02	75.14	42.23				2.38	J.	0.011136	1450.04	1449.75	1449.75	1448.5	100.7	501 50yr	501	HLF501
	00:0	1.01				0.10	1	- 1	1			1		100		
1 2	78 33	41 01				3 10		٦.	1450 86	1450 46	1450 35	1449 5	130.8	550 100vr	550	HIESSO
1.28	64.98	34.4				2.93		0.01812	1450.68	1450.34	1450.25	1449.5	100.7	550 50yr	550	HLF550
0.99	72.64	49.93	0.39	0.25	1.75		1.27	0.009559	1451.43	1451.07	1451.07	1449.5	130.8	100yr	593	HLF593
0.98		41.81		0.19	1.59	2.49		Т	1451.26	1450.95	1450.95	1449.5	100.7	50yr	593	HLF593
1.22	59.87	40.12	0.33	0.28	1.87		1.7	0.014071	1451.89	1451.45	1451.3	1450	130.8	629 100yr	629	HLF629
1.21	56.54	33.17	0.25	0.23	1.59	3.22	1 1.49	0.014611	1451.69	1451.3	1451.19	1450	100.7	629 50yr	629	HLF629
0.5			0.49	0.32	1.85		1.4	0.008101	1452.47	1452.08	1452.08	1450.5	130.8	682 100yr	682	HLF682
0.94	02.07	40.80	0.41	0.20	1.07	2.00	Ĺ	1	27.7chT	1451.94	1451.94	1450.5	1.00.7	DAY SUYI	780	חרי-1
				0 2	1 67			-	1 150 00	100	1,001	1450	100 4	5	691	17000
0.74	76.07			0.46	1.14	2.32			1452.74		1452.49	1451	130.8	724 100yr	724	HLF724
0.74	71.68	50.31	0.27	0.38	0.98		3 1.25	0.005123	1452.56	1452.22	1452.34	1451	100.7	50yr	724	HLF724
0.93	87.91	57.58	0.6	0.59	2.1	2.85	2.09		1453.04	1452.72	1452.76	1451.5	130.8	100yr	771	HLF771
	(m)	(m2)	(m)	(m)	(m/s)	(m/s)	(m/s)	(m/m)	(m)		(m)	(m)	(m3/s) (
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